

CPS ENERGY TECHNICAL GUIDEBOOK FOR ENERGY EFFICIENCY AND DEMAND RESPONSE

January 2025, Applies to FY 2026



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COMMON ACRONYMS

4CP – The four monthly ERCOT system-wide peaks occurring in June, July, August, and September

ACCA – Air Conditioning Contractors of America

AHRI – Air-Conditioning, Heating, & Refrigeration Institute

ANSI – American National Standards Institute

ASHRAE – American Society of Heating, Refrigerating and Air-Conditioning Engineers

CEE – Consortium for Energy Efficiency

COP – Coefficient of Performance

CP – Coincident Peak

EER – Energy Efficiency Ratio

EFLH – Effective Full Load Hours

ER – Early Retirement

EUL – Estimated Useful Life

HSPF – Heating Seasonal Performance Factor

IEER – Integrated Energy Efficiency Ratio

IPLV – Integrated Part Load Value

NC – New Construction

NCP – Non-coincident Peak

PTAC – Packaged Terminal Air Conditioners

PTHP – Packaged Terminal Heat Pumps

RAC – Room Air Conditioner

ROB – Replace-on-Burnout

RUL – Remaining Useful Life

SEER – Seasonal Energy Efficiency Ratio

1. INTRODUCTION

CPS Energy offers numerous energy efficiency programs to its customers as part of its Sustainable Tomorrow Energy Plan (STEP). These programs reduce annual electric energy use and peak demand and reduce CPS Energy customers' electricity bills. CPS Energy and third parties administer these residential and commercial/industrial programs. Program effectiveness undergoes independent reviews annually.

1.1 OBJECTIVE OF THIS GUIDEBOOK

The purpose of the CPS Energy Technical Guidebook for Energy Efficiency and Demand Response (Guidebook) is to provide a single common reference document for estimating energy and peak demand savings resulting from the installation or implementation of energy efficiency and demand response measures provided through CPS Energy's programs. The Guidebook contains a compilation of deemed savings values for use in savings estimation.

The data and methodologies in this document are to be used by program planners, administrators, implementers, and evaluators for forecasting, reporting, and evaluating energy and demand savings from measures installed through CPS Energy's energy efficiency and demand response programs. The scope of the Guidebook is measure savings; therefore, other resources should be consulted for health and safety considerations related to implementation of measures (i.e., residential air sealing measures).

1.2 HOW TO USE THIS GUIDEBOOK

The Guidebook provides a means for the uniform application of savings methods and the assumptions behind them. This uniformity facilitates consistency among CPS Energy and other Texas utilities in estimating savings across programs and estimating program-level cost-effectiveness. By establishing clear qualification criteria for the development of projected and claimed savings estimates, the Guidebook provides transparency of savings calculations for all interested stakeholders.

The data and algorithms housed in the Guidebook are to be used by program administrators for the following purposes:

- Projecting program savings for the next year
- Reporting program savings from the previous year

2. EVALUATION OVERVIEW

2.1 CPS ENERGY STEP PROGRAM PORTFOLIO STRUCTURE

CPS Energy’s portfolio of energy efficiency and demand response programs addresses all residential and most commercial markets and major end uses for both sectors. For more information on CPS Energy program offerings, please see <https://www.cpsenergy.com/en/my-home/savenow.html>.

CPS Energy evaluates the contribution of each residential and commercial program to the portfolio’s energy, peak demand, and non-coincident peak savings, including avoided transmission charges. Except where noted, coincident peak savings values were calculated by using the weighted-average 20-hour probability method, as described below in Section 2.3.1.

2.2 IMPACT EVALUATION PROCESS

The Guidebook leverages existing evaluation, measurement, and verification (EM&V) work previously conducted for CPS Energy and other electric utilities in Texas. For the past fifteen years, investor-owned utilities, EM&V consultants, and stakeholder groups have collaborated to develop accurate and comprehensive “deemed” savings for hundreds of residential and commercial energy efficiency measures, under the auspices of the Public Utility Commission of Texas (PUCT). This extended effort has culminated in the publication of the Texas Technical Reference Manual (Texas TRM),¹ a compendium of algorithms, baseline efficiency data, efficiency standards, energy savings calculations and data tables. By utilizing the TRM, the Guidebook can provide CPS Energy with energy and demand impact estimates that have been vetted numerous times by independent third parties and are consistent with impact estimates being used by all the investor-owned utilities in Texas. For this Guidebook, the methodologies used are from the current Texas TRM version² except where noted.

Because the Texas TRM does not include expected energy impacts that are specific to San Antonio, additional building energy use model simulations were performed to derive energy savings estimates for weather-sensitive energy efficiency measures. These new estimates are consistent with the TRM but better reflect equipment usage in San Antonio’s climate.

2.3 DEFINITION OF NON-COINCIDENT, COINCIDENT, AND 4CP PEAK DEMAND

¹ Public Utility Commission of Texas (PUCT) Technical Reference Manual (TRM). Available for download at: <http://texasefficiency.com/index.php/regulatory-filings/deemed-savings>.

² Available for download through the Texas Efficiency website. <https://texasefficiency.com/trm-docs/>.

2.3.1 Non-Coincident Peak (NCP)

For each measure and building type, annual kWh savings are allocated to each of the 8,760 hours in a year for the appropriate load shape. Non-coincident peak demand savings are the maximum difference between the pre- and post-retrofit demand, regardless of when that maximum value, or “peak,” occurs. Conceptually, “demand” is instantaneous; in practice, demand savings are frequently estimated using the difference in energy use between pre-and post-retrofit conditions over the course of a one-hour interval.

For measures for which the Guidebook deemed savings estimates are prepared using load shapes and/or engineering algorithms, the maximum estimated reduction in demand over any given hour of the year is reported as the non-coincident peak. In some cases, when deemed savings are estimated using building simulation models, the 99.9th percentile hourly savings estimate is used in lieu of the absolute maximum value.³

2.3.2 Coincident Peak (CP)

The calculation of coincident peak demand savings relies upon a probabilistic analysis of a San Antonio typical meteorological year (TMY), which contains hourly values of solar radiation and meteorological elements for a 1-year period. This analysis used the most recent version of these data, the TMY3 data set, which used data collected from Kelly Field Air Force Base (Kelly AFB) weather station.⁴ This approach relates the TMY3 data set’s actual hourly weather, time-of-day, and day-of-week data to historical CPS Energy peak conditions and calculates a probability-weighted estimate of the average kW savings during the twenty hours with the highest probability of occurring during CPS Energy’s system peak. This approach enjoys broad acceptance in Texas because all investor-owned electric utilities began using it in 2016.

³ This approach is taken with the residential envelope measures, developed with residential building simulation models, to account for some apparent time-displacement in when loads are met in the models. Given that single hour savings in some cases exceed the theoretical maximum hourly savings the measure could deliver according to engineering calculations, it appears that loads occasionally accumulate across hours giving hourly differences that may not realistically reflect the impacts of a measure.

⁴ Data collected at the Kelly Field Air Force Base (Kelly AFB) station were generally used, because the temperature data series collected at the San Antonio International Airport is inexplicably higher than the readings collected at other local weather stations. (See Itron, CPS June 2014 Electricity Forecast, Sept. 2014, pp. 8-9.).

Fundamentally, this approach requires several key steps:

1. Establish the predicted peak hours in summer for CPS Energy.

This estimation approach involves identifying a set of hours during which CPS Energy peaks are likely to happen. Given the variability in when peaks occur, using a wider range of potential peak hours within a logistic model is optimal for estimating the actual, expected impact for a single utility peak hour per year. In other words, a probabilistic approach using 20 hours provides a better chance of estimating the actual peak rather than an approach that relies on a single hour. The 20 most probable hours for this estimate are based on a regression of 2010-2019 June to September 2:00pm-6:00pm historical load data plus CPS Energy estimated hourly demand response load and provide a sufficient range of hours to assign the highest probability of being within the set of actual peak hours.

2. Correlate weather and load data.

A logistic regression model and CPS Energy historical load data are used to estimate a relationship between CPS Energy peak hours and a set of explanatory variables, including a temperature variable and dummy variables representing the time-of-day and month-of-year.

3. Select Peak Hours in TMY Weather Files.

This step applies regression results to San Antonio TMY3 weather data by calculating the probability of an hour coinciding with CPS Energy peak by using marginal probabilities assigned to the explanatory variables. The twenty hours selected are those with the highest probability of occurring during CPS Energy's peak.

Table 2.3-1 shows the selected top 20 hours in order of decreasing relative probability). Additional hours are shown because some hours, such as those occurring on weekends or holidays, are eliminated for some measures.

Kilowatt values for each of the top 20 hours were extracted from the 8,760 hourly load shapes for each specific measure. The coincident peak demand was then calculated as the probability-weighted average kW for the top 20 hours.

Table 2.3-1: [Evaluation Overview] Top Hours in Order of Relative Probability

| Month | Day | Hour (start) | Temp (°F) | Peak Probability (with DR addback) | Month | Day | Hour (start) | Temp (°F) | Peak Probability (with DR addback) |
|-------|-----|--------------|-----------|------------------------------------|-------|-----|--------------|-----------|------------------------------------|
| 6 | 19 | 15 | 104.00 | 0.868682 | 6 | 17 | 16 | 97.88 | 0.056450 |
| 6 | 19 | 16 | 102.92 | 0.846070 | 6 | 18 | 16 | 97.88 | 0.056450 |
| 6 | 20 | 16 | 102.92 | 0.846070 | 7 | 30 | 16 | 98.96 | 0.054889 |
| 6 | 20 | 15 | 101.84 | 0.488014 | 8 | 20 | 14 | 98.96 | 0.035089 |

| Month | Day | Hour (start) | Temp (°F) | Peak Probability (with DR addback) | Month | Day | Hour (start) | Temp (°F) | Peak Probability (with DR addback) |
|-------|-----|--------------|-----------|------------------------------------|-------|-----|--------------|-----------|------------------------------------|
| 6 | 19 | 14 | 102.92 | 0.354302 | 8 | 23 | 14 | 98.96 | 0.035089 |
| 6 | 20 | 14 | 102.92 | 0.354302 | 6 | 10 | 14 | 99.86 | 0.034069 |
| 6 | 19 | 17 | 100.94 | 0.327983 | 6 | 18 | 14 | 99.86 | 0.034069 |
| 6 | 10 | 15 | 100.94 | 0.298350 | 7 | 31 | 14 | 100.94 | 0.033105 |
| 6 | 18 | 15 | 100.94 | 0.298350 | 8 | 18 | 17 | 96.98 | 0.031332 |
| 7 | 31 | 15 | 102.02 | 0.292170 | 8 | 19 | 17 | 96.98 | 0.031332 |
| 8 | 20 | 15 | 99.86 | 0.271695 | 8 | 20 | 17 | 96.98 | 0.031332 |
| 8 | 19 | 16 | 98.96 | 0.267009 | 6 | 17 | 17 | 97.88 | 0.030418 |
| 8 | 20 | 16 | 98.96 | 0.267009 | 6 | 18 | 17 | 97.88 | 0.030418 |
| 6 | 10 | 16 | 99.86 | 0.261069 | 7 | 31 | 17 | 98.96 | 0.029554 |
| 8 | 17 | 15 | 98.96 | 0.142675 | 6 | 13 | 15 | 97.88 | 0.026605 |
| 7 | 31 | 16 | 100.04 | 0.132695 | 6 | 14 | 15 | 97.88 | 0.026605 |
| 8 | 18 | 16 | 97.88 | 0.121478 | 6 | 21 | 15 | 97.88 | 0.026605 |
| 6 | 20 | 17 | 98.96 | 0.076337 | 6 | 5 | 16 | 96.98 | 0.025995 |
| 6 | 17 | 15 | 98.96 | 0.067168 | 6 | 11 | 16 | 96.98 | 0.025995 |
| 8 | 18 | 15 | 97.88 | 0.059418 | 6 | 13 | 16 | 96.98 | 0.025995 |
| 8 | 19 | 15 | 97.88 | 0.059418 | 6 | 21 | 16 | 96.98 | 0.025995 |
| 8 | 17 | 16 | 96.98 | 0.058101 | 8 | 7 | 16 | 95.90 | 0.022879 |
| 8 | 23 | 16 | 96.98 | 0.058101 | 8 | 28 | 16 | 95.90 | 0.022879 |
| 6 | 12 | 16 | 97.88 | 0.056450 | 6 | 17 | 14 | 98.96 | 0.015490 |
| 6 | 16 | 16 | 97.88 | 0.056450 | 7 | 30 | 14 | 100.04 | 0.015044 |

2.3.3 Avoided Transmission Charge (ERCOT 4CP TCOS)

CPS Energy is electrically interconnected to the other electric utilities in the Electric Reliability Council of Texas (ERCOT) region, which encompasses most of Texas. All the users of the ERCOT transmission system share the annual cost of operating the high-voltage transmission system, called the ERCOT transmission cost of service (TCOS). Each user's share of the TCOS is allocated based upon their individual electrical demand during the prior year's monthly ERCOT system peak for the months of June through September, known as the four coincident peaks (4CP).

To reduce their allocated share of the ERCOT 4CP TCOS charge, CPS Energy anticipates likely 4CP events and deploys demand response resources to reduce demand accordingly. Energy efficiency measures also contribute to demand reduction during 4CP events.

To estimate gross demand reduction within each demand response program/subprogram, the estimated load reduction per participant is multiplied by the number of active participants and a "deployment success rate," the rate at which CPS Energy correctly anticipated and deployed each resource during historical 4CP events.

For energy efficiency programs, hourly load shapes for each measure provide the estimate of the impacts during 4CP event hours for each weekday during the months of June through September. Based on historical CPS Energy interval data, the 4CP has occurred in the hour ending 17 for each 4CP month since 2011. Hourly kW values are extracted from measure load shapes for the hour ending 17 for each day during the 4CP months. Finally, the 90th percentile maximum monthly value is averaged across the 4CP months to estimate the 4CP impact for each program. The CPS Energy FY 2016 evaluation saw the addition of ERCOT 4CP demand savings resulting from energy efficiency programs. In previous CPS Energy evaluations, ERCOT 4CP demand savings were calculated only for demand response programs.

3. BENEFIT – COST ANALYSIS

3.1 BENEFIT – COST TESTS OVERVIEW

Five benefit-cost tests are commonly used to assess energy efficiency and demand response programs:

1. Participant Cost Test (PCT)
2. Program Administrator Cost Test (PACT)
3. Ratepayer Impact Measure Test (RIM)
4. Total Resource Cost Test (TRC)
5. Societal Cost Test (SCT)

The outcome of each test is expressed as the ratio of the net present value of program benefits divided by the net present value of program costs. A benefit-cost ratio greater than 1.00 indicates a program's net present value of benefits outweigh the net present value of costs, in accordance with how costs and benefits are tallied within each test. In general, ratios greater than 1.00 are preferred, though ratios must always be considered alongside other motivations and goals in comprehensive program evaluation. Analyzing all five tests together provides a comprehensive view of program performance. To understand how various energy efficiency programs performed collectively, benefit-cost ratios also may be evaluated at various levels of aggregation, including, for example:

- All residential programs
- All commercial programs
- All demand response programs
- Programs under development
- All programs (total portfolio)

3.1.1 Benefit-Cost Test Components

Different benefits and costs apply to each test, as summarized in the table below.

Table 3.1-1: [Benefit-Cost Analysis] Benefit-Cost Test Components

| Test Component | PCT | PACT | RIM | TRC | SCT |
|-------------------------------|-----|------|-----|-----|-----|
| Net Present Value of Benefits | | | | | |
| Customer Rebates Received | ✓ | | | | |
| Customer Bill Savings | ✓ | | | | |
| Avoided Energy Costs | | ✓ | ✓ | ✓ | ✓ |
| Avoided Capacity Costs | | ✓ | ✓ | ✓ | ✓ |
| Avoided Transmission Charges | | ✓ | ✓ | ✓ | ✓ |

| Test Component | PCT | PACT | RIM | TRC | SCT |
|--|-----|------|-----|-----|-----|
| Avoided Price Spikes | | ✓ | ✓ | ✓ | ✓ |
| Net Present Value of Costs | | | | | |
| Incremental Costs | ✓ | | | ✓ | ✓ |
| Utility Administrative Costs | | ✓ | ✓ | ✓ | ✓ |
| Utility Rebate Costs | | ✓ | ✓ | | |
| Lost Revenue because of Reduced Energy Bills | | | ✓ | | |
| Other Externalities | | | | | ✓ |

Evaluated benefits include the following:

Customer Rebates Received are the net present value of rebates received by customers who enrolled in the program each year. In most programs, these are one-time rebate payments made during the program year, and thus are equal to the amount spent by the utility on rebates during that year. However, some programs pay participants over several years. In these cases, the benefit reflects the net present value of the projected stream of customer rebates received and is different from the amount spent during the program year.

Customer Bill Savings are the net present value of participating customers' utility bill savings projected to result from installation of program-induced measures over their expected useful life.

Avoided Energy Costs are the net present value of utility energy cost reductions projected to result from installation of program-induced measures over their expected useful life.

Avoided Capacity Costs are the net present value of utility capacity cost reductions projected to result from installation of program-induced measures over their expected useful life.

Avoided Transmission Charges are the net present value of 4CP transmission cost reductions projected to result from installation of program-induced measures over their expected useful life. The process by which these transmission costs are allocated to CPS Energy is explained in Section 2.3.3.

Avoided Price Spikes are the net present value of wholesale energy price spikes avoided by deployment of demand response resources during wholesale price spike events. This value is only calculated for demand response programs and represents the price spike value less avoided energy costs to prevent double counting avoided energy value.

Other Externalities may include the net present value of avoided environmental impacts or national security costs, induced economic development impacts, and other benefits not directly measurable at the customer's site or on the utility's system.

Evaluated costs include the following:

Incremental Costs are the difference in the cost of a base case energy efficiency measure compared to the cost of a higher efficiency alternative. It represents the incremental cost that participating customers must pay to gain the energy savings benefits from the higher efficiency measure.

Utility Administrative Costs include the net present value of all non-incentive utility costs associated with the program (for example: program overhead costs, traditional administrative costs, marketing and outreach, and similar activities).

Utility Rebate Costs are the net present value of rebates paid to customers who enrolled in the program each year. In most programs, these are one-time payments made during the program year, and thus are equal to the amount spent by the utility on rebates during that year. However, some programs pay participants over several years. In these cases, the cost reflects the net present value of the projected stream of rebate payments and is different from the amount spent during the program year.

Lost Revenue because of Reduced Energy Bills is the net present value of reductions in utility revenue projected to result from installation of program-induced measures over their expected useful life.

3.1.2 Interpreting Benefit-Cost Test Results

3.1.2.1 Participant Cost Test (PCT)

The PCT represents a comparison of the costs and benefits of a utility customer installing or implementing an energy efficiency or demand response measure. Because this test reflects the participant's perspective, it helps inform the utility as to whether a participant will be well off because of their participation.

3.1.2.2 Program Administrator Cost Test (PACT)

The PACT measures each program's potential to reduce CPS Energy's revenue requirements in the form of reduced generation capacity investments, and reduced generation production cost and purchased power requirements. Established to reflect the utility's perspective, the PACT can help a utility evaluate a program's potential contribution to overall resource cost planning objectives.

3.1.2.3 Ratepayer Impact Measure Test (RIM)

The RIM provides an indication of the additional revenues required to keep the utility's rate of return at the same level it would have experienced had it not offered the program. This test attempts to assess the impact on customers who did not participate in the program. It is important to note that, except for certain program types, many standard energy efficiency programs commonly achieve a RIM test result of less than 1.00.

3.1.2.4 Total Resource Cost Test (TRC)

The TRC is a summation of all participant and utility reduced costs (benefits) and all participant and

utility increased costs. Because the TRC only incorporates costs (either avoided or expended) in its calculation, customer inducements are excluded from its calculation. Customer inducements are also transfer payments, so if utility rebates were included, participant costs would be reduced by a corresponding amount. As the TRC combines both customers' and CPS Energy's costs and benefits, it gives an indication of how the program affects both participating and non-participating customers.

3.1.2.5 Societal Cost Test (SCT)

The SCT is a variant of the TRC, with the addition of "externalities" which may include environmental impacts, effects on national security, economic development impacts, and other impacts not directly measurable at the customer's site or on the utility's system. CPS Energy currently includes a projected cost of compliance with potential future carbon emissions regulations in its avoided cost of energy, and thus has already internalized at least a portion of the externalities that would be included in the SCT.

3.2 ADDITIONAL INPUTS & ASSUMPTIONS

3.2.1 Incremental Costs

Customer investment costs (used interchangeably with "incremental costs") are key inputs in three of the five benefit-cost tests: (1) Participant Cost Test, (2) Total Resource Cost Test, and (3) Societal Cost Test. These estimates represent the difference in cost that must be paid between a baseline measure that could have been installed and a higher efficiency measure installed. Because of the nature of most energy efficiency and demand response programs, this type of information can be very hard to estimate precisely. Ideally, invoices showing the exact cost per installation compared to a "standard" cost for a baseline installation would determine the incremental costs. However, this level of detail is not available for all installed measures, so CPS Energy uses the best estimation method for each program. Please see the program sections for additional details.

3.2.2 Estimated Useful Life

The estimated useful life (EUL) of each measure is based on Texas standards used by the state's investor-owned utilities or other knowledge or information specific to CPS Energy. Please see the program sections for more information.

3.2.3 CPS Energy Avoided Cost Periods

CPS Energy annually calculates and provides separate avoided energy cost values for each of five different avoided cost periods for use in benefit-cost modeling. These cost periods are listed in Table 3.2-1. Energy savings associated with each energy efficiency measure are allocated into these avoided cost periods based on the measure's load shape to calculate the value of avoided energy costs.

Table 3.2-1: [Benefit-Cost Analysis] Avoided Cost Periods

| Cost Period | Description | Hours |
|---------------------|--|-------|
| Summer On-Peak | June-September, weekday hours 14-20 | 602 |
| Summer Mid-Peak | June-September, weekday hours 8-13 and 21-22, weekend hours 8-22 | 1,228 |
| Summer Off-Peak | June-September, hours 1-7 and 23-24 | 1,098 |
| Non-Summer Mid-Peak | January-May and October-December, weekday hours 7-22 | 2,736 |
| Non-Summer Off-Peak | January-May and October-December, weekday hours 1-6 and 23-24, all weekend hours | 3,096 |

3.2.4 Net-to-Gross Ratios

The Net-to-Gross (NTG) ratio is a factor that represents the fraction of total purchases caused by the program. The ratio may be made up of a variety of factors that capture differences between gross and net savings, commonly considering the effects of free riders (savings that would have occurred without the program, such as those deriving from customers who would implement measures without rebates but accept them because they are offered) and spillover effects (additional savings induced in customers who implement measures but do not receive rebates as a direct or indirect result of the program). CPS Energy uses NTG ratios based on previous evaluations except for the residential weatherization program, which relies upon a 100% NTG ratio industry standard used in Texas for weatherization programs.

3.2.5 Other Inputs

CPS Energy provides Frontier Energy with current and projected residential and commercial rates, avoided energy costs for each avoided cost period, avoided capacity costs for energy efficiency and demand response measures, and avoided ERCOT Transmission Cost of Service costs, over a 25-year period. CPS Energy also provides Frontier Energy with separate energy and capacity loss factors, a corporate discount rate used in financial analysis, and an estimate of avoided carbon dioxide emissions per kWh.

Frontier estimates the incremental value, over avoided summer peak avoided costs, of avoided price spikes, for use in analyzing the cost-effectiveness of demand response programs. These data are updated annually. They are competitive in nature and are not published in this Guidebook. They do not affect the estimates of kWh, NCP, CP and 4CP savings achieved by each program, but do affect the cost-effectiveness analysis of these savings.

4. RESIDENTIAL: LIGHTING

4.1 GENERAL SERVICE LED LAMPS

4.1.1 Measure Description

This measure provides a method for calculating savings for replacement of a standard-efficiency lamp with an LED general service lamp (GSL) in a residential application.⁵ This measure applies to all lamps not included in the subsequent measure for Specialty LED Lamps.

4.1.1.1 Eligibility Criteria

These savings values rely on usage patterns specific to both indoor and outdoor applications. In lieu of collecting lamp location, a default weighting of 90.5% indoor and 9.5% outdoor may be assumed.⁶

Residential new construction applications are not eligible to claim lighting savings. Current code requires high-efficacy lighting for all permanently-installed fixtures.

Fixtures with integrated LEDs may be eligible under this measure using a modified baseline.

4.1.1.2 Baseline Condition

On May 8, 2022, the Department of Energy (DOE) issued two final rules relating to GSLs:

- Energy Conservation Program: Definitions for GSLs, effective July 8, 2022, which expanded the definition of GSLs.⁷
- Energy Conservation Program: Energy Conservation Standards for GSLs, effective July 25, 2022, which shifted the baseline to 45 lumens per watt efficacy.⁸

These guidelines are reinforced in the current federal standard, effective July 3, 2024.⁹

The baseline is assumed to be the second-tier Energy Independence and Security Act of 2007 (EISA)-mandated efficiency for GSLs. The EISA regulations dictate that GSLs must comply with a 45 lumen per watt efficacy standard at time of sale beginning January 1, 2023.¹⁰

For low income and hard-to-reach direct install programs, utilities may claim additional savings for early retirement of incandescent and halogen lamps with LEDs when documentation requirements are met. It is assumed that the remaining useful life (RUL) of the existing lamps is two years. This is when the

⁵ DOE Final Rule: Definitions for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0012-0022>.

⁶ 2015 U.S. Lighting Market Characterization, Department of Energy. November 2017. Table 4.11. https://www.energy.gov/sites/prod/files/2017/12/f46/lmc2015_nov17.pdf.

⁷ DOE Final Rule: Definitions for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0012-0022>.

⁸ DOE Final Rule: Energy Conservation Standards for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0005-0070>.

⁹ DOE Final Rule: Energy Conservation Standards for General Service Lamps. <https://www.regulations.gov/document/EERE-2022-BT-STD-0022-0205>.

¹⁰ See TRM v9.0 for methodology and baseline.

incandescent or halogen lamp baseline bulbs will be at the end of their useful life and need to be replaced. First year savings are weighted using the dual baseline methodology for the first-tier and second-tier baselines found in Table 4.1-1 and Table 4.1-2. The first-tier baseline may only be used in this scenario.

Residential new construction applications are not eligible to claim lighting savings. Current code requires high-efficacy lighting for all permanently-installed fixtures.

Due to the variability among fixture types compared to screw-in lamps, qualified fixtures with integrated LEDs should use the rated installed wattage and equivalent wattage, or other approved custom methodology, in lieu of the deemed values outlined in the following table. These wattages are available on the ENERGY STAR certificate and can be used in combination with the deemed savings methodologies provided in this measure.

Table 4.1-1: [GSL LEDs] Baseline and Default Wattages for A-Shaped Lamps^{11 12}

| Minimum Lumens | Maximum Lumens | Incandescent Equivalent Wattage Pre-EISA 2007 | First Tier EISA 2007 (W_{base}) ¹³ | 2 nd Tier EISA 2007 (W_{base}) ¹⁴ | Default W_{Post} (if unknown) ¹⁵ |
|----------------|----------------|---|---|---|---|
| 250 | 309 | 25 | Exempt | Exempt | 3.5 |
| 310 | 749 | 40 | 29 | 12 | 5.5 |
| 750 | 1,049 | 60 | 43 | 20 | 9.0 |
| 1,050 | 1,489 | 75 | 53 | 28 | 11.5 |
| 1,490 | 2,600 | 100 | 72 | 45 | 15.0 |
| 2,601 | 3,300 | 150 | Exempt | 66 | 22.5 |

¹¹ Federal standard for General Service Incandescent Lamps (GSILs):

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=20.

¹² If exempt, refer to incandescent equivalent wattage.

¹³ 1st tier baseline is only applicable to low income and hard-to-reach direct install programs. This baseline is only applicable for 2 years, equivalent to the expected life of an incandescent lamp.

¹⁴ Non-exempt baseline wattages are calculated by dividing the midpoint of the specified lumen range by the 45 lumens/watt efficacy standard.

¹⁵ Average rated wattage from ENERGY STAR qualified product listing rounded to nearest half-watt:

<https://www.energystar.gov/productfinder/product/certified-light-bulbs/results>.

Table 4.1-2: [GSL LEDs] Baseline and Default Wattages for Other Lamp Shapes^{16,17}

| Minimum Lumens | Maximum Lumens | Incandescent Equivalent Wattage Pre-EISA 2007 | First Tier EISA 2007 (W_{base}) ¹⁸ | 2 nd Tier EISA 2007 (W_{base}) ¹⁹ | Default W_{Post} (if unknown) ²⁰ |
|----------------|----------------|---|---|---|---|
| 250 | 309 | QPL | Exempt | Exempt | QPL |
| 310 | 749 | - | 29 | 12 | |
| 750 | 1,049 | - | 43 | 20 | |
| 1,050 | 1,489 | - | 53 | 28 | |
| 1,490 | 2,600 | - | 72 | 45 | |
| 2,601 | 3,300 | QPL | Exempt | 66 | |

4.1.1.3 High-Efficiency Condition

The high-efficiency condition is the wattage of the replacement lamp. The ENERGY STAR specification for lamps and luminaires was sunsetted, effective December 31, 2024.²¹ Since the ENERGY STAR light bulbs qualified product listing (QPL) is no longer available, the high-efficiency condition should be determined according to the following guidelines, listed in order of priority.

1. Legacy ENERGY STAR QPL – The evaluation team downloaded a copy of the QPL, which can be shared upon request.
2. Lighting Facts product label – The ENERGY STAR sunset memo indicates that Lighting Facts product labels will continue to convey lamp performance in lieu of the ENERGY STAR specification.
3. For outliers that do not fall under one of the prior two categories, the high-efficiency condition should be set to match the rated wattage on the manufacturer specification sheet.

4.1.2 Energy and Demand Savings Methodology

4.1.2.1 Savings Algorithms and Input Variables

Wattage reduction is defined as the difference between the wattage of a standard baseline lamp

¹⁶ Federal standard for General Service Incandescent Lamps (GSILs):

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=20.

¹⁷ If exempt, refer to incandescent equivalent wattage.

¹⁸ 1st tier baseline is only applicable to low income and hard-to-reach direct install programs. This baseline is only applicable for 2 years, equivalent to the expected life of an incandescent lamp.

¹⁹ Non-exempt baseline wattages are calculated by dividing the midpoint of the specified lumen range by the 45 lumens/watt efficacy standard.

²⁰ Average rated wattage from ENERGY STAR qualified product listing rounded to nearest half-watt:

<https://www.energystar.gov/productfinder/product/certified-light-bulbs/results>.

²¹ ENERGY STAR Lighting Sunset Memo, March 13, 2023.

<https://www.energystar.gov/sites/default/files/asset/document/ENERGY%20STAR%20Lighting%20Sunset%20Memo.pdf>.

according to EISA 2007 (Table 4.1-1 and Table 4.1-2) and the wattage of a comparable GSL LED. An LED is considered comparable to the baseline lamp if they are aligned on the lumen output ranges set out in EISA 2007.

Energy Savings

Annual energy (kWh) savings are calculated as follows.

$$\text{Energy Savings } [\Delta kWh] = \frac{(W_{base} - W_{post})}{1,000} \times HOU \times ISR \times IEF_E$$

Equation 4.1-1

Where:

| | | |
|------------|---|--|
| W_{base} | = | Baseline wattage corresponding with the lumen output of the purchased LED lamp for the year purchased/installed. Reduced baselines are provided for EISA-compliant lamps in Table 4.1-1 and Table 4.1-2. |
| W_{post} | = | Actual wattage of LED purchased/installed (if unknown, use default wattages from Table 4.1-1 and Table 4.1-2). |
| HOU | = | Average hours of use per year = 803 hours (for interior/exterior applications calculated based on an average daily usage of 2.2 hours per day). ²² |
| IEF_E | = | Interactive Effects Factor to account for cooling energy savings and heating energy penalties associated with lighting power reductions; see Table 4.1-3. |
| ISR | = | In-Service Rate, the percentage of incentivized units that are installed and in use (rather than removed, stored, or burnt out) to account for units incentivized but not operating; (see Table 4.1-4) |
| 1,000 | = | Constant to convert from watts to kilowatts. |

Table 4.1-3: [GSL LEDs] Energy Interactive Effects Factors for Cooling Bonus and Heating Penalty²³

| Heating/Cooling Type ²⁴ | IEF_E |
|------------------------------------|---------|
| Gas Heat with AC | 1.17 |
| Gas Heat with no AC | 1.00 |
| Heat Pump | 1.05 |

²² The average daily usage of 2.2 hours per day is a blended value for indoor and outdoor lamps. Source: Evaluation of 2008 Texas 'Make Your Mark' Statewide CFL Program Report. Frontier Associates. June 2009.

²³ Extracted from BEopt energy models used to estimate savings for envelope measures. Referencing the EISA baseline table, the typical lumen output was determined by taking the midpoint for the 60-watt equivalent lamp (900 lm), which was assumed to be the most typical installation. The resulting lumens were divided by the default wattage for incandescents (43 W), CFLs (13 W), and LEDs (10 W) resulting in an assumed efficacy for incandescents (21 lm/W), CFLs (70 lm/W), and LEDs (90 lm/W). IEF values were calculated using the following formula: $1 + \frac{HVAC_{savings}}{Lighting_{savings}}$.

²⁴ IEF values for homes with no AC are most appropriate for customers with room air conditioners.

| Heating/Cooling Type ²⁴ | IEF _E |
|--|------------------|
| Electric Resistance Heat with AC | 0.90 |
| Electric Resistance Heat with no AC | 0.76 |
| No heat with AC | 1.17 |
| Unconditioned Space | 1.00 |
| Heating/Cooling Unknown/Upstream ²⁵ | 1.04 |

Table 4.1-4: [GSL LEDs] In-Service Rates by Program Type

| Program Type | ISR |
|---|------|
| Low-income community kits ²⁶ | 0.88 |
| All other kit programs ²⁷ | 0.60 |
| Retail (time of sale) ²⁸ | 0.76 |
| Midstream/upstream | |
| Direct Install ²⁹ | 0.97 |

Demand Savings

Demand savings are determined by applying a demand factor corresponding to the peak type.

$$\text{Demand Savings } [\Delta kW] = \frac{(W_{base} - W_{post})}{1,000} \times DF \times ISR \times IEF_D$$

Equation 4.1-2

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 4.1-5.

IEF_D = Interactive Effects Factor to account for cooling demand savings or heating demand penalties associated with lighting power reductions; see Table 4.1-6.

²⁵ Calculated using IEFs from Cadmus report, weighted using TMY CDD and HDD for Texas, and adjusted to exclude 16% outdoor lighting except for upstream defaults. Cadmus report: Cadmus. Entergy Energy-Efficiency Portfolio Evaluation Report 2013 Program Year. Prepared for Entergy Arkansas, Inc. March 14, 2014. Docket No. 07-082-TF.

²⁶ Kits targeting low-income qualified communities. From IL TRM v10, based on 2018 Ameren IL income-qualified participant survey. Representative of first-year installations.

²⁷ From IL TRM v10 based on evaluation of ComEd PY9 Elementary Energy Education program. Representative of first-year installations.

²⁸ From IL TRM v10 based on evaluation of ComEd PY9 Elementary Energy Education program. Representative of first-year installations.

²⁹ Dimetrosky, S., Parkinson, K. and Lieb, N. "Residential Lighting Evaluation Protocol – The Uniform Methods Project: Methods for Determining Energy Efficiency Savings for Specific Measures." January 2015. ISR for upstream programs, including storage lamps installed within four years of purchase. <http://energy.gov/sites/prod/files/2015/02/f19/UMPChapter21-residential-lighting-evaluation-protocol.pdf>.

Table 4.1-5: [GSL LEDs] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 0.399 |
| CP | 0.056 |
| 4CP | 0.094 |

Table 4.1-6: [GSL LEDs] Demand Interactive Effects Factors for Cooling Bonus and Heating Penalty³⁰

| Heating/Cooling Type ³¹ | IEF _{D,NCP} | IEF _{D,CP/4CP} |
|--|----------------------|-------------------------|
| Gas Heat with AC | 1.17 | 1.68 |
| Gas Heat with no AC | 1.00 | 1.00 |
| Heat Pump | 1.05 | 1.68 |
| Electric Resistance Heat with AC | 0.90 | 1.68 |
| Electric Resistance Heat with no AC | 0.76 | 1.00 |
| No heat with AC | 1.17 | 1.68 |
| Unconditioned Space | 1.00 | 1.00 |
| Heating/Cooling Unknown/Upstream ³² | 1.04 | 1.58 |

Low Income and Hard-to-Reach Direct Install Programs

Annual energy (kWh) and peak demand (kW) may be calculated separately for two time periods:

- The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
- The remaining time in the EUL period (EUL – RUL)

Annual energy and peak demand savings are calculated by weighting the early retirement and replacement-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in the appendix.

Where:

RUL = Remaining Useful Life = 2 years.

EUL = Estimated Useful Life = 16 or 20 years (see Measure Life and Lifetime Savings section).

³⁰ Refer to Table 4.1-3.

³¹ IEF values for homes with no AC are most appropriate for customers with room air conditioners.

³² Refer to Table 4.1-3.

Upstream/Midstream Program Assumptions

All GSLs with an equivalent wattage of 100 W or lower distributed through upstream or midstream programs should calculate savings using a combination of residential and non-residential savings methodologies with 95 percent of savings allocated to the residential sector and the remaining five percent of savings allocated to the commercial sector. This can be accomplished by multiplying the residential savings by a 0.95 factor and the non-residential savings by a 0.05 factor.

4.1.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

4.1.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

4.1.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is based upon rated lamp life of the LED, assuming an average daily use of 2.2 hours per day based on blended usage for indoor/outdoor applications and applies a 0.85 degradation factor to indoor/outdoor LEDs.

$$EUL = \frac{Rated\ Life \times DF}{HOU \times 365.25}$$

Equation 4.1-3

Where:

Rated Life = 10,000 hours, 12,000 hours, 15,000 hours, or 20,000 hours, as specified by the manufacturer. If unknown, assume a 10,000-hour lifetime.³³

DF = 0.85 degradation factor.³⁴

HOU = 2.2 hours per day.³⁵

³³ Minimum lifetime requirement under ENERGY STAR Lamps Specification V1.1, effective September 30, 2014. <http://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Lamps%20V1%201%20Specification.pdf>.

³⁴ ENERGY STAR CFL Third Party Testing and Verification Off-the-Shelf CFL Performance: Batch 3. Figure 27, p. 47.

³⁵ The average daily usage of 2.2 hours per day is a blended value for indoor and outdoor lamps. Source: Evaluation of 2008 Texas 'Make Your Mark' Statewide CFL Program Report. Frontier Associates. June 2009.

Table 4.1-7: [GSL LEDs] Estimated Useful Life

| Range of Rated Product Lifetime (Hours) | Assumed Rated Product Lifetime (Hours) | EUL (Years) ³⁶ |
|---|--|---------------------------|
| ≤ 17,500 | 15,000 | 16 |
| > 17,500 | 20,000 | 20 |

4.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Program delivery type (low-income targeted kits, non-low-income targeted kits, retail, midstream/upstream, direct install)
- LED ANSI C79. 1-2002 nomenclature/lamp shape (A, C, G, R, PAR, etc.)
- LED manufacturer and model number
- LED quantity
- LED rated wattage
- LED rated lumens
- LED rated lifetime (hours)Home cooling system type (refrigerated, none)
- Home heating system type (gas, electric resistance, heat pump, none)
- Location of replacement lamp (conditioned, unconditioned, outdoor); only required when not assuming default weighting
- Proof of purchase with date of purchase and quantity
 - Alternative: representative photos of replacement lamps or another pre-approved method of installation verification
- ENERGY STAR certificate matching new LED model number
 - Alternative: another pre-approved method of certification (e.g., LM-79, LM-80, TM-21, and ISTMT lab reports)

³⁶ Measure life capped at 20 years. EUL may be deemed at 16 years in lieu of collecting manufacturer rated life or documenting customer baseline.

- For low income and hard-to-reach direct install programs, photo documentation clearly showing the lamp type and approximate quantity replaced or other pre-approved method of verification

4.1.4 Document Revision History

Table 4.1-8: [GSL LEDs] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Added in-service rates by program type. |
| FY 2026 | Clarified federal standard. Updated new construction code high-efficacy lamp requirement. |

4.2 SPECIALTY LED LAMPS

4.2.1 Measure Description

This measure provides a method for calculating savings for replacement of an incandescent or halogen reflector or decorative lamp with an LED specialty lamp in a residential application. These lamps are limited to the following lamp types, defined by the current federal standard³⁷ and further reduced to only include lamps that are common to utility rebate programs.

- G shape lamps that have a first number symbol less than or equal to 12.5 (diameter less than or equal to 1.5625 inches)
- G shape lamps with a diameter of 5 inches or more
- MR shape lamps that have a first symbol equal to 16 (diameter equal to 2 inches) and have a lumen output greater than or equal to 800 lumens
- Reflector lamps that have a first number symbol less than 16 (diameter less than 2 inches) and that do not have E26/E24, E26d, E26/50x39, E26/53x39, E29/28, E29/53x39, E39, E39d, EP39, or EX39 bases

4.2.1.1 Eligibility Criteria

These savings values rely on usage patterns specific to both indoor and outdoor applications. In lieu of collecting lamp location, a default weighting of 90.5% indoor and 9.5% outdoor may be assumed.³⁸

Residential new construction applications are not eligible to claim lighting savings. Current code requires high-efficacy lighting for all permanently-installed fixtures.

Fixtures with integrated LEDs may be eligible under this measure using a modified baseline.

4.2.1.2 Baseline Condition

On May 8, 2022, the Department of Energy (DOE) issued two final rules relating to GSLs:

- Energy Conservation Program: Definitions for General Service Lamps, effective July 8, 2022, which expanded the definition of GSLs.³⁹
- Energy Conservation Program: Energy Conservation Standards for GSLs, effective July 25, 2022, which shifted the baseline to 45 lumens per watt efficacy.⁴⁰

³⁷ DOE Final Rule: Definitions for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0012-0022>.

³⁸ 2015 U.S. Lighting Market Characterization, Department of Energy. November 2017. Table 4.11.

https://www.energy.gov/sites/prod/files/2017/12/f46/lmc2015_nov17.pdf.

³⁹ DOE Final Rule: Definitions for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0012-0022>.

⁴⁰ DOE Final Rule: Energy Conservation Standards for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0005-0070>.

These guidelines are reinforced in the current federal standard, effective July 3, 2024.⁴¹

For all products not defined as GSLs, the baseline is assumed to be the incandescent equivalent wattage. The baseline wattage will be determined based on the bulb shape of the installed lamp as outlined below.

Residential new construction applications are not eligible to claim lighting savings. Current code requires high-efficacy lighting for all permanently-installed fixtures.

Due to the variability among fixture types compared to screw-in lamps, qualified fixtures with integrated LEDs should use the rated installed wattage and equivalent wattage, or other approved custom methodology, in lieu of the deemed values outlined in the following table. These wattages are available on the ENERGY STAR certificate and can be used in combination with the deemed savings methodologies provided in this measure.

Table 4.2-1: [Specialty LEDs] Baseline and Default Wattages⁴²

| Lamp Type ⁴³ | Minimum Lumens | Maximum Lumens | W _{Base} |
|--|----------------|----------------|-------------------|
| G-shape with diameter \geq 5 in. ⁴⁴ | - | - | QPL |
| MR16/MRX16 | 800 | - | 75 |
| R14 | 250 | 299 | 25 |

4.2.1.3 High-Efficiency Condition

The high-efficiency condition is the wattage of the replacement lamp. The ENERGY STAR specification for lamps and luminaires was sunsetted, effective December 31, 2024.⁴⁵ Since the ENERGY STAR light bulbs qualified product listing (QPL) is no longer available, the high-efficiency condition should be determined according to the following guidelines, listed in order of priority.

⁴¹ DOE Final Rule: Energy Conservation Standards for General Service Lamps. <https://www.regulations.gov/document/EERE-2022-BT-STD-0022-0205>.

⁴² Due to large variation in lamp types, use rated value from ENERGY STAR-qualified product listing (QPL) where not specified: <https://www.energystar.gov/productfinder/product/certified-light-bulbs/results>.

⁴³ Lamp types excluded from this table were not included on the ENERGY STAR-qualified product listing. For missing lamp types, refer to the equivalent and rated wattages from the ENERGY STAR® certification.

⁴⁴ G-shape lamps are not included because there were very few ENERGY STAR-qualified products with a diameter of 5 inches or more. For these products, use the equivalent and rated wattages from the ENERGY STAR® certification.

⁴⁵ ENERGY STAR Lighting Sunset Memo, March 13, 2023. <https://www.energystar.gov/sites/default/files/asset/document/ENERGY%20STAR%20Lighting%20Sunset%20Memo.pdf>.

1. Legacy ENERGY STAR QPL – The evaluation team downloaded a copy of the QPL, which can be shared upon request.
2. Lighting Facts product label – The ENERGY STAR sunset memo indicates that Lighting Facts product labels will continue to convey lamp performance in lieu of the ENERGY STAR specification.
3. For outliers that do not fall under one of the prior two categories, the high-efficiency condition should be set to match the rated wattage on the manufacturer specification sheet.

4.2.2 Energy and Demand Savings Methodology

4.2.2.1 Savings Algorithms and Input Variables

Wattage reduction is defined as the difference between the wattage of a specialty baseline lamp and the wattage of a directional or specialty LED.

Energy Savings

Annual energy (kWh) savings are calculated as follows:

$$\text{Energy Savings } [\Delta kWh] = \frac{(W_{base} - W_{post})}{1,000} \times HOU \times ISR \times IEF_E$$

Equation 4.2-1

Where:

| | | |
|------------|---|---|
| W_{base} | = | <i>EISA-exempt specialty lamp or a DOE-ruling-exempt reflector see Table 4.2-1.</i> |
| W_{post} | = | <i>Actual wattage of LED purchased/installed.</i> |
| HOU | = | <i>Average hours of use per year = 803 hours (for interior/exterior applications calculated based on an average daily usage of 2.2 hours per day).⁴⁶</i> |
| IEF_E | = | <i>Interactive Effects Factor to account for cooling energy savings and heating energy penalties associated with lighting power reductions; see Table 4.2-2.</i> |
| ISR | = | <i>In-Service Rate, the percentage of incentivized units that are installed and in use (rather than removed, stored, or burnt out) to account for units incentivized but not operating; see Table 4.2-3</i> |
| 1,000 | = | <i>Constant to convert from watts to kilowatts.</i> |

⁴⁶ The average daily usage of 2.2 hours per day is a blended value for indoor and outdoor lamps. Source: Evaluation of 2008 Texas 'Make Your Mark' Statewide CFL Program Report. Frontier Associates. June 2009.

Table 4.2-2: [Specialty LEDs] Energy Interactive Effects Factors for Cooling Bonus and Heating Penalty⁴⁷

| Heating/Cooling Type ⁴⁸ | IEF _E |
|--|------------------|
| Gas Heat with AC | 1.17 |
| Gas Heat with no AC | 1.00 |
| Heat Pump | 1.05 |
| Electric Resistance Heat with AC | 0.90 |
| Electric Resistance Heat with no AC | 0.76 |
| No heat with AC | 1.17 |
| Unconditioned Space | 1.00 |
| Heating/Cooling Unknown/Upstream ⁴⁹ | 1.04 |

Table 4.2-3: [GSL LEDs] In-Service Rates by Program Type

| Program Type | ISR |
|---|------|
| Low-income community kits ⁵⁰ | 0.88 |
| All other kit programs ⁵¹ | 0.60 |
| Retail (time of sale) ⁵² | 0.76 |
| Midstream/upstream | |
| Direct Install ⁵³ | 0.97 |

⁴⁷ Extracted from BEopt energy models used to estimate savings for envelope measures. Referencing the EISA baseline table, the typical lumen output was determined by taking the midpoint for the 60-watt equivalent lamp (900 lm), which was assumed to be the most typical installation. The resulting lumens were divided by the default wattage for incandescents (43 W), CFLs (13 W), and LEDs (10 W) resulting in an assumed efficacy for incandescents (21 lm/W), CFLs (70 lm/W), and LEDs (90 lm/W). IEF values were calculated using the following formula: $1 + \frac{\text{HVAC}_{\text{savings}}}{\text{Lighting}_{\text{savings}}}$.

⁴⁸ IEF values for homes with no AC are most appropriate for customers with room air conditioners.

⁴⁹ Calculated using IEFs from Cadmus report, weighted using TMY CDD and HDD for Texas, and adjusted to exclude 16% outdoor lighting except for upstream defaults. Cadmus report: Cadmus. Entergy Energy-Efficiency Portfolio Evaluation Report 2013 Program Year. Prepared for Entergy Arkansas, Inc. March 14, 2014. Docket No. 07-082-TF.

⁵⁰ Kits targeting low-income qualified communities. From IL TRM v10, based on 2018 Ameren IL income-qualified participant survey. Representative of first-year installations.

⁵¹ From IL TRM v10 based on evaluation of ComEd PY9 Elementary Energy Education program. Representative of first-year installations.

⁵² From IL TRM v10 based on evaluation of ComEd PY9 Elementary Energy Education program. Representative of first-year installations.

⁵³ Dimetrosky, S., Parkinson, K. and Lieb, N. "Residential Lighting Evaluation Protocol – The Uniform Methods Project: Methods for Determining Energy Efficiency Savings for Specific Measures." January 2015. ISR for upstream programs, including storage lamps installed within four years of purchase. <http://energy.gov/sites/prod/files/2015/02/f19/UMPCChapter21-residential-lighting-evaluation-protocol.pdf>.

Demand Savings

Demand savings are determined by applying a demand factor corresponding to the peak type.

$$\text{Demand Savings } [\Delta kW] = \frac{(W_{base} - W_{post})}{1,000} \times DF \times ISR \times IEF_D$$

Equation 4.2-2

Where:

- DF* = Demand Factor for NCP, CP, or 4CP peak demand; see Table 4.2-4.
- IEF_D* = Interactive Effects Factor to account for cooling demand savings or heating demand penalties associated with lighting power reductions; see Table 4.2-5.

Table 4.2-4: [Specialty LEDs] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 0.399 |
| CP | 0.056 |
| 4CP | 0.094 |

Table 4.2-5: [Specialty LEDs] Demand Interactive Effects Factors for Cooling Bonus and Heating Penalty⁵⁴

| Heating/Cooling Type ⁵⁵ | IEF _{D,NCP} | IEF _{D,CP/4CP} |
|--|----------------------|-------------------------|
| Gas Heat with AC | 1.17 | 1.68 |
| Gas Heat with no AC | 1.00 | 1.00 |
| Heat Pump | 1.05 | 1.68 |
| Electric Resistance Heat with AC | 0.90 | 1.68 |
| Electric Resistance Heat with no AC | 0.76 | 1.00 |
| No heat with AC | 1.17 | 1.68 |
| Unconditioned Space | 1.00 | 1.00 |
| Heating/Cooling Unknown/Upstream ⁵⁶ | 1.04 | 1.58 |

Upstream/Midstream Program Assumptions

All GSLs with an equivalent wattage of 100 W or lower distributed through upstream or midstream programs should calculate savings using a combination of residential and non-residential savings methodologies with 95 percent of savings allocated to the residential sector and the remaining five

⁵⁴ Refer to Table 4.2-2.

⁵⁵ IEF values for homes with no AC are most appropriate for customers with room air conditioners.

⁵⁶ Refer to Table 4.2-2.

percent of savings allocated to the commercial sector. This can be accomplished by multiplying the residential savings by a 0.95 factor and the non-residential savings by a 0.05 factor.

4.2.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

4.2.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

4.2.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is based upon rated lamp life of the LED, assuming an average daily use of 2.2 hours per day based on blended usage for indoor/outdoor applications and applies a 0.85 degradation factor to indoor/outdoor LEDs.

$$EUL = \frac{Rated\ Life \times DF}{HOU \times 365.25}$$

Equation 4.2-3

Where:

Rated Life = 10,000 hours, 12,000 hours, 15,000 hours, or 20,000 hours, as specified by the manufacturer. If unknown, assume a 10,000-hour lifetime.⁵⁷

DF = 0.85 degradation factor.⁵⁸

HOU = 2.2 hours per day.⁵⁹

Table 4.2-6: [Specialty LEDs] Estimated Useful Life

| Range of Rated Product Lifetime (Hours) | Assumed Rated Product Lifetime (Hours) | EUL (Years) ⁶⁰ |
|---|--|---------------------------|
| ≤ 17,500 | 15,000 | 16 |
| > 17,500 | 20,000 | 20 |

⁵⁷ Minimum lifetime requirement under ENERGY STAR Lamps Specification V1.1, effective September 30, 2014.

<http://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Lamps%20V1%201%20Specification.pdf>.

⁵⁸ ENERGY STAR CFL Third Party Testing and Verification Off-the-Shelf CFL Performance: Batch 3. Figure 27, p. 47.

⁵⁹ The average daily usage of 2.2 hours per day is a blended value for indoor and outdoor lamps. Source: Evaluation of 2008 Texas 'Make Your Mark' Statewide CFL Program Report. Frontier Associates. June 2009.

⁶⁰ Measure life capped at 20 years depending on the applicable baseline. EUL may be deemed at 16 years in lieu of collecting manufacturer rated life or documenting customer baseline.

4.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Program delivery type (low-income targeted kits, now-low-income targeted kits, retail, midstream/upstream, direct install)
- LED manufacturer and model number
- LED quantity
- LED ANSI C79. 1-2002 nomenclature/lamp shape (G, MR16, MRX16, R14)
- Baseline calculation methodology (replaced lamp nameplate wattage, EISA-affected non-reflector, EISA-exempt non-reflector, DOE ruling-affected reflector, DOE ruling-exempt reflector, manufacturer-rated equivalent incandescent wattage, or default wattage)
- LED baseline and rated wattage
- LED rated lumens
- LED rated lifetime (hours)
- Home cooling system type (refrigerated, none)
- Home heating system type (gas, electric resistance, heat pump, none)
- Location of replacement lamp (conditioned, unconditioned, outdoor); only required when not assuming default weighting
- Proof of purchase with date of purchase and quantity
 - Alternative: representative photos of replacement lamps or another pre-approved method of installation verification
- ENERGY STAR certificate matching new LED model number
 - Alternative: another pre-approved method of certification (e.g., LM-79, LM-80, TM-21, and ISTMT lab reports)

4.2.4 Document Revision History

Table 4.2-7: [Specialty LEDs] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
|-------------------|-----------------------|

| | |
|---------|---|
| FY 2025 | Added in-service rates by program type. |
| FY 2026 | Clarified federal standard. |

5. RESIDENTIAL: HEATING, VENTILATION, AND AIR CONDITIONING

5.1 AIR CONDITIONER AND HEAT PUMP TUNE-UPS

5.1.1 Measure Description

This measure applies to central air conditioners (AC) and heat pumps (HP) of any configuration where all applicable actions from the checklist below are completed. An AC tune-up involves checking, cleaning, adjusting, and resetting the equipment to factory conditions to restore operating efficiencies closer to as-new performance. This measure applies to all residential applications.

For this measure, the service technician must complete the following tasks according to industry best practices. To properly assess and adjust the refrigerant charge level, the unit must be operating under significant (normal) cooling load conditions. Therefore, this measure may only be performed for energy savings reporting purposes when the outdoor ambient dry bulb temperature is above 75°F, and the indoor return air dry bulb temperature is above 70°F.

HVAC Inspection and Tune-Up Checklist⁶¹

- Check thermostat settings
- Tighten all electrical connections; measure motor voltage and current.
- Lubricate all moving parts, including motor and fan bearings.
- Inspect and clean the condensate drain.
- Inspect controls of the system to ensure proper and safe operation. Check the startup/shutdown cycle of the equipment to ensure the system starts, operates, and shuts off properly.
- Clean evaporator and condenser coils.
- Check refrigerant level and adjust to manufacturer specifications
- Clean indoor blower fan components and adjust to provide proper system airflow.
- Inspect and clean or change air filters; replacement preferred best practice.
- Measure airflow via static pressure across the cooling coil and adjust to manufacturer specifications.

⁶¹ Based on ENERGY STAR HVAC Maintenance Checklist. <https://www.energystar.gov/saveathome/heating-cooling/maintenance-checklist>.

- Check capacitor functionality and capacitance; compare to original equipment manufacturer (OEM) specifications.

5.1.1.1 Eligibility Criteria

HVAC systems must be manufactured before January 1, 2023, to be eligible for for this measure.⁶² All residential customers are eligible for this measure if they have refrigerated air conditioning 65,000 Btu/hr or less in cooling capacity that has not been serviced through a utility program in the last five years.

This measure is also applicable to packaged terminal air conditioners and heat pumps (PTAC/PTHPs).

5.1.1.2 Baseline Condition

The baseline is a system with some or all the following issues:

- Dirty condenser coil
- Dirty evaporator coil
- Dirty blower wheel
- Dirty filter
- Improper airflow
- Incorrect refrigerant charge

The baseline system efficiency should be calculated using the following formulas:

$$EER_{pre} = (1 - EL) \times EER_{post}$$

Equation 5.1-1

$$HSPF_{pre} = (1 - EL) \times HSPF_{post}$$

Equation 5.1-2

Where:

EER_{pre} = Efficiency of the cooling equipment before tune-up.

EL = Efficiency loss because of dirty coils, blower, filter, improper airflow, and/or incorrect refrigerant charge = 0.05.

EER_{post} = Deemed cooling efficiency of the equipment after tune-up = 11.2 EER.

⁶² The current federal standard became effective on January 1, 2023, with full manufacturing compliance of the new SEER2 testing procedure being enforced as of April 24, 2023. This measure will be updated in the future to address the new efficiency ratings.
<https://www.regulations.gov/document/EERE-2021-BT-TP-0030-0027>.

| | | |
|---------------|---|--|
| $HSPF_{pre}$ | = | Heating efficiency of the air source heat pump before tune-up. |
| $HSPF_{post}$ | = | Deemed heating efficiency of air source heat pumps after tune-up = 7.7 HSPF. |

Note: The efficiency loss factor specified above may be replaced with program specific values if an M&V plan and efficiency loss factor derivation are provided to the evaluation team. These factors will be subject to review at the end of each fiscal year and may be revised for the next fiscal year.

5.1.1.3 High-Efficiency Condition

After the tune-up, the equipment must be clean with airflows and refrigerant charges adjusted as appropriate and set forth above, with the added specification that refrigerant charge adjustments must be within +/- 3 degrees of target sub-cooling for units with thermal expansion valves (TXV) and +/- 5 degrees of target super heat for units with fixed orifices or capillary tubes.

The efficiency standard, or efficiency after the tune-up, is deemed to be the manufacturer specified energy efficiency ratio (EER) of the existing central air conditioner or heat pump, which has been determined using the following logic and standards. The useful life of an AC unit is 19 years. The useful life of a heat pump is 16 years. Therefore, it is conservatively thought that the majority of existing, functioning units were installed under the federal standard in place between January 23, 2006 and January 1, 2015, which set a baseline of 13 SEER and 7.7 HSPF.⁶³ A 13 SEER is equivalent to approximately 11.2 EER⁶⁴ using the conversion developed by Lawrence Berkeley Lab and US DOE: $EER = -0.02 \times SEER^2 + 1.12 \times SEER$.

5.1.2 Energy and Demand Savings Methodology

5.1.2.1 Savings Algorithms and Input Variables

Savings are based on an assumed efficiency loss factor of 5% because of dirty coils, dirty filters, improper airflow, and/or incorrect refrigerant charge.⁶⁵

Energy Savings

Heating energy savings are only applicable to heat pumps.

$$\text{Energy Savings [kWh]} = kWh_{Savings,C} + kWh_{Savings,H}$$

Equation 5.1-3

⁶³ Code specified HSPF from federal standard effective January 23, 2006 through January 1, 2015.

⁶⁴ Code specified 13 SEER from federal standard effective January 23, 2006 through January 1, 2015, converted to EER using $EER = -0.02 \times SEER^2 + 1.12 \times SEER$. National Renewable Energy Laboratory (NREL). "Building America House Simulation Protocols." U.S. Department of Energy. Revised October 2010. <http://www.nrel.gov/docs/fy11osti/49246.pdf>.

⁶⁵ Energy Center of Wisconsin, May 2008; "Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research." https://focusonenergy.com/sites/default/files/centralairconditioning_report.pdf.

$$\text{Energy Savings (Cooling)} [kWh_{Savings,C}] = Cap_C \times \left(\frac{1}{EER_{pre}} - \frac{1}{EER_{post}} \right) \times \frac{EFLH_C}{1,000}$$

Equation 5.1-4

$$\text{Energy Savings (Heating)} [kWh_{Savings,H}] = Cap_H \times \left(\frac{1}{HSPF_{pre}} - \frac{1}{HSPF_{post}} \right) \times \frac{EFLH_H}{1,000}$$

Equation 5.1-5

Where:

| | | |
|---------------|---|---|
| Cap_C | = | Rated cooling capacity of the equipment based on model number [Btuh] (1 ton = 12,000 Btuh). |
| Cap_H | = | Rated heating capacity of the equipment based on model number [Btuh] (1 ton = 12,000 Btuh). |
| EER_{pre} | = | Cooling efficiency of the equipment pre-tune-up using Equation 5.1-1 [Btuh/W]. |
| EER_{post} | = | Cooling efficiency of the equipment after the tune-up [Btuh/W]. Assume 11.2. |
| $HSPF_{pre}$ | = | Heating efficiency of the equipment pre-tune-up using Equation 5.1-2 [Btuh/W]. |
| $HSPF_{post}$ | = | Heating efficiency of the equipment after the tune-up [Btuh/W]. Assume 7.7. |
| $EFLH_C$ | = | Cooling equivalent full-load hours [hours] Use 2,237 hours in San Antonio. ⁶⁶ |
| $EFLH_H$ | = | Heating equivalent full-load hours [hours] Use 1,101 hours in San Antonio. ⁶⁷ |
| 1,000 | = | Constant to convert from watts to kilowatts. |

Demand Savings

Summer savings are determined by applying a demand factor.

$$\text{Demand Savings } [\Delta kW] = Cap_C \times \left(\frac{1}{EER_{pre}} - \frac{1}{EER_{post}} \right) \times \frac{DF}{1,000}$$

Equation 5.1-6

Where:

| | | |
|------|---|---|
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 5.1-1. |
|------|---|---|

⁶⁶ ENERGY STAR Central AC/HP Savings Calculator. April 2009 update.

https://www.energystar.gov/sites/default/files/asset/document/ASHP_Sav_Calc.xls.

⁶⁷ Ibid.

1,000 = Constant to convert from watts to kilowatts.

Table 5.1-1: [AC/HP Tune-up] Demand Factors⁶⁸

| Peak Type | DF |
|-----------|------|
| NCP | 1.00 |
| CP | 0.87 |
| 4CP | 0.87 |

5.1.2.2 Deemed Energy Savings Tables

Applying the above algorithms results in the deemed energy savings per ton in Table 5.1-2. Heating savings are only applicable for heat pumps.

Table 5.1-2: [AC/HP Tune-up] Deemed Energy Savings per ton

| Climate Zone | Cooling kWh/ton | Heating kWh/ton |
|--------------|-----------------|-----------------|
| San Antonio | 126.1 | 90.3 |

5.1.2.3 Deemed Demand Savings Tables

Applying the above algorithms results in the deemed demand savings per ton in Table 5.1-3.

Table 5.1-3: [AC/HP Tune-up] Deemed Demand Savings per ton

| Climate Zone | NCP kW/ton | CP kW/ton | 4CP kW/ton |
|--------------|------------|-----------|------------|
| San Antonio | 0.056 | 0.049 | 0.049 |

5.1.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 5 years for AC or HP tune-ups.⁶⁹

5.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Most recent tune-up service date or confirmation that system has not been serviced within

⁶⁸ Demand factors calculated in accordance with the current peak definition are lower than expected for the Texas climate. Residential HVAC measures will temporarily revert to the demand factors used in TX TRM 4.0 before the change to the peak definition. These values will be reevaluated in upcoming TRM cycles to better align with the current peak definition.

⁶⁹ GDS Associates, Inc. (2007). Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures. Prepared for The New England State Program Working Group; Page 1-3, Table 1.
https://library.cee1.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLights&HVACGDS_1Jun2007.pdf.

the previous five years

- Equipment type (split AC, split HP, packaged AC, packaged HP, PTAC, PTHP)
- Manufacturer, model number, and serial number
- Cooling capacity of the serviced HVAC unit (tons)
- Heating capacity of the serviced HVAC unit (algorithm approach only)
- Before and after tune-up pictures of components illustrating condition change due to cleanings (Note: pictures that include well-placed familiar objects like hand tools often provide a sense of scale and a reference for color/shading comparisons. Pictures of equipment name plates are useful)
- Recommended:
 - Serial number
 - Refrigerant type
 - Amount of refrigerant added or removed
 - Target superheat or subcooling
 - Post tune-up superheat or subcooling
 - Static pressures before and after tune-up
 - Return and supply dry bulb and wet bulb temperatures

5.1.4 Document Revision History

Table 5.1-4: [AC/HP Tune-Up] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated demand savings. Clarified eligibility for PTACs and PTHPs. |
| FY 2026 | Updated tune-up checklist to match ENERGY STAR HVAC Maintenance Checklist. |

5.2 CENTRAL AND MINI-SPLIT AIR CONDITIONERS AND HEAT PUMPS WITH SEER2 RATINGS

5.2.1 Measure Description

Residential replacement of existing heating and cooling equipment with a new central or mini-split air-source air conditioner (AC) or heat pump (HP) in an existing building, or the installation of a new central AC or HP in a new residential construction. Downsized systems that are right-sized per heat load calculation are also eligible. A new central system includes an entire packaged unit or a split system consisting of an indoor unit with a matching remote condensing unit. This measure also applies to the installation of dual-fuel HPs and DC inverter systems that meet all existing measure eligibility criteria.

Additional savings may be available for duct removal in combination with the installation of a ductless mini-split. In these cases, refer to the Duct Sealing measure and follow the savings methodology (standard approach) using a value of 0 CFM as the post-improvement duct leakage. Leakage testing must be performed on the existing ductwork to claim savings for duct removal.

5.2.1.1 Eligibility Criteria

The deemed savings apply to units with a capacity of $\leq 65,000$ Btu/hour (5.4 tons).

Equipment shall be properly sized to dwelling based on ASHRAE or ACCA Manual J standards. Manufacturer datasheets for installed equipment or documentation of AHRI or DOE CCMS certification must be provided^{70,71}. Savings should be calculated using rated capacities whenever possible. Reported system capacities and efficiencies should always match those verified by AHRI or DOE as tested under AHRI operating conditions for a specific combination of equipment, including condenser, coil, and furnace (or condenser only for packaged units). Savings should never be calculated using efficiency ratings for individual system components.

Customers should be advised against using the emergency heat (EM HEAT) setting on heat pump thermostats. This setting is meant only for use in emergency situations when the heat pump is damaged or malfunctioning. Supplemental heating automatically kicks on below freezing conditions using the regular HEAT setting. Contractors installing a new heat pump thermostat with equipment install shall advise customer of correct thermostat usage.

For early retirement projects, to receive savings, the unit to be replaced must be functioning at the time of removal with a maximum age of 24 years for ACs and 20 years for HPs. Otherwise, claim savings for a replace-on-burnout project. Additional guidance for systems applying the default age is provided in the Savings Algorithms and Input Variables section.

The replacement of a room AC with a central or mini-split AC or HP is eligible and should be claimed

⁷⁰ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

⁷¹ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

against the new construction baseline. Refer to the Replace-on-burnout or Early Retirement of an Electric Resistance Furnace section for guidance about the appropriate heating baseline for residences with electric resistance heat. Under this scenario, no savings should be awarded for rightsizing.

System rightsizing refers to installing an HVAC system that has been sized in accordance with a load calculation, such as a Manual J, considering specific home characteristics. Rightsizing retrofit projects could include upsizing or downsizing by one-half ton or more from the existing system. New construction projects are not eligible to receive deemed savings for system rightsizing.

For system downsizing, savings may be claimed against the applicable replace-on-burnout or early retirement scenario using the existing higher system pre-capacity with the lower system post-capacity if a Manual J load calculation is completed and included with project documentation.

For system upsizing, savings should generally be claimed against the new construction baseline. However, optional rightsizing savings are available for upsizing up to one ton for the following scenarios. In these cases, savings may be claimed against the applicable replace-on-burnout or early retirement scenario if the specified conditions are met. For these scenarios, savings must be determined using the lower pre tonnage. These exceptions should be applied consistently at the program level for the duration of the program year.

- Replacing a single larger capacity system with multiple smaller capacity systems.⁷² If the multiple installed units do not share the same efficiency value, savings should be determined using the most conservative efficiency value.
- Replacing a single-stage system with a variable-speed system.⁷³ This scenario does not apply to the replacement of a multi-stage unit with another multi-stage unit.
- If a Manual J load calculation (or equivalent) is completed and included with project documentation.⁷⁴

⁷² This exception is allowed to account for efficiency improvements due to zoning that are not reflected in the current savings methodology.

⁷³ This exception is allowed to account for efficiency improvements due to operating at variable speeds that are not reflected in the current savings methodology.

⁷⁴ This exception is allowed to account for efficiency improvements due to replacing a unit that was operating longer than designed to keep up with actual site load conditions.

Additionally, low-income, or hard-to-reach programs may use the electric resistance baseline for the following two scenarios:

- The electric resistance baseline may be used for systems upsized by no more than a half-ton in lieu of the new construction baseline. Under this scenario, cooling savings should be claimed against the new construction baseline using the installed (higher) capacity. Heating savings should be claimed against the electric resistance baseline using the existing (lower) capacity. Documentation should be aligned with the rightsizing and electric resistance baseline requirements outlined in this measure.
- The second scenario is for a major multifamily renovation when a centralized system, such as a boiler, is replaced with individual heat pumps. For this scenario, the electric resistance baseline may be claimed in lieu of new construction only if the building owner can document intent to install electric resistance furnaces without program intervention. The cooling savings should still be claimed against the new construction baseline. Documentation should follow early retirement and electric resistance baseline requirements.

When replacing a single unit with multiple units where the capacity is the same or has been downsized, savings should be calculated using the total system pre- and post-capacity. Again, if the multiple installed units do not share the same efficiency value, savings should be looked up using the most conservative efficiency value.

5.2.1.2 Baseline Condition

New Construction, Replace-on-Burnout, or Early Retirement of an Air-Source AC or HP

New construction baseline efficiency values for ACs or HPs are compliant with the current federal standard,^{75,76} effective January 1, 2023. The baseline is assumed to be a new system with an AHRI-listed SEER2 rating consistent with the values listed in Table 5.2-1 and Table 5.2-2. These baselines are also applicable to central ACs with gas, electric resistance, or unknown heating replacing an HP and room/window ACs with central, space, or no heating.

For replace-on-burnout projects, the cooling baselines are reduced by 4.3%. This value is based on Energy Systems Laboratory (ESL) survey data and incorporates an adjustment to the baseline SEER2/EER2 value to reflect the percentage of current replacements that do not include the installation of an AHRI-matched system.^{77,78} Heating baselines were not included in original ESL survey data and are

⁷⁵ DOE minimum efficiency standard for residential air conditioners/heat pumps.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=48&action=viewlive.

⁷⁶ Walter-Terrinoni, Helen, "New U.S. Energy Efficiency Standards and Refrigerants for Residential ACs and Heat Pumps." Air-Conditioning, Heating, & Refrigeration Institute (AHRI). February 1, 2022.

⁷⁷ Frontier Energy on behalf of the Electric Utility Marketing Managers of Texas (EUMMOT). "Petition to revise Existing Commission-Approved Deemed Savings Values for Central Air Conditioning and Heat Pump Systems: Docket No. 36780." Public Utility Commission of Texas. Approved August 27, 2009. <https://interchange.puc.texas.gov/>. Adapted for new 14 SEER baseline.

⁷⁸ The original petition defines the reduced baseline as 12.44 SEER compared to a 13 SEER federal standard. This deemed value was converted to a percentage reduction to accommodate a transition from SEER to SEER2. No EER adjustment is discussed in the original petition because the

not adjusted.

For early retirement projects, baselines are defined in Table 5.2-1 and Table 5.2-2 based on the applicable federal standard base on manufacture year. These baselines have been converted to SEER2, EER2, and HSPF2 by extrapolating from known values referenced in the current federal standard. Systems manufactured as of January 1, 2023 are not eligible for early retirement.

For early retirement projects involving an HP replacing an AC with gas heat, early retirement cooling baselines should be used in combination with new construction heating baselines.

For all systems with a part-load efficiency rating of 15.2 SEER2 or higher, the full-load efficiency baseline is reduced to 9.8 EER2, consistent with the EER2 federal standard specified for the Southwest region. While this standard does not directly apply to Texas, it is used here to recognize a reduced full-load allowance for systems achieving higher part-load efficiency ratings. This value is not reduced based on ESL survey data. Where applicable, the reduced 9.8 EER2 baseline should be applied in lieu of the EER2 baseline value presented in Table 5.2-1 and Table 5.2-2 except where the specified baseline EER2 value is lower than 9.8 EER2.

Replace-on-Burnout or Early Retirement of an Electric Resistance Furnace

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.⁷⁹ Space heating primarily refers to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.⁸⁰ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters should calculate savings using a HP baseline.

By the nature of the technology, all electric resistance furnaces have the same efficiency with HSPF = 3.412.⁸¹ Projects in which an electric resistance furnace is replaced, either in replace-on-burnout or early retirement scenarios, use this baseline for heating-side savings.

Table 5.2-1: [Central HVAC] AC Baseline Efficiencies

| Project Type | Capacity | Cooling Mode |
|--|----------|-------------------------|
| New Construction, split air conditioners | < 45,000 | 14.3 SEER2 11.7 EER2 |
| | ≥ 45,000 | 13.8 SEER2 11.2 EER2 |

previous deemed savings structure only awarded savings based on SEER ratings. However, supporting documentation of the original filing makes it clear that the adjustment is appropriate for both part- and full-load cooling efficiency values. Therefore, the deemed percentage reduction is applied to both SEER2 and EER2 ROB baselines.

⁷⁹ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

⁸⁰ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

⁸¹ COP = HSPF × 1,055 J/BTU / 3,600 J/W-hr. For Electric Resistance, heating efficiency is 1 COP. Therefore, HSPF = 1 × 3,600 / 1,055 = 3.412.

| Project Type | Capacity | Cooling Mode |
|---|----------|-------------------------|
| New construction, packaged air conditioners | All | 13.4 SEER2 10.9 EER2 |
| Replace-on-burnout, split air conditioners | < 45,000 | 13.7 SEER2 11.2 EER2 |
| | ≥ 45,000 | 13.2 SEER2 10.7 EER2 |
| Replace-on-burnout, packaged air conditioners | All | 12.8 SEER2 10.4 EER2 |
| Early retirement, air conditioners (manufactured 1/1/2015 through 12/31/2022) | All | 12.8 SEER2 10.4 EER2 |
| Early retirement, air conditioners (when applying default age) ⁸² | All | 12.3 SEER2 10.0 EER2 |
| Early retirement, air conditioners (manufactured 1/23/2006 through 12/31/2014) | All | 11.9 SEER2 9.7 EER2 |
| Early retirement, air conditioners (manufactured before 1/23/2006) | All | 9.1 SEER2 7.4 EER2 |
| All systems rated at 15.2 SEER2 or higher ⁸³ | All | 9.8 EER2 |

Table 5.2-2: [Central HVAC] HP Baseline Efficiencies

| Project Type | Cooling Mode | Heating Mode |
|--|-------------------------|--------------|
| New construction, split heat pumps | 14.3 SEER2 11.7 EER2 | 7.5 HSPF2 |
| New construction, packaged heat pumps | 13.4 SEER2 10.9 EER2 | 6.7 HSPF2 |
| Replace-on-burnout, split heat pumps | 13.7 SEER2 11.2 EER2 | 7.5 HSPF2 |
| Replace-on-burnout, packaged heat pumps | 12.8 SEER2 10.4 EER2 | 6.7 HSPF2 |
| Early retirement, split heat pumps (manufactured 1/1/2015 through 12/31/2022) | 12.8 SEER2 10.4 EER2 | 6.9 HSPF2 |

⁸² Baseline efficiencies are calculated by taking the average the early retirement categories for 2006-2014 and 2015-2022.

⁸³ When installing any system with a part-load efficiency rating of 15.2 SEER2 or higher, the reduced 9.8 EER2 full-load efficiency baseline should be applied in lieu of the applicable value presented earlier in the table except where the specified baseline EER2 value is lower than 9.8 EER2.

| Project Type | Cooling Mode | Heating Mode |
|---|-------------------------|--------------|
| Early retirement, packaged heat pumps (manufactured 1/1/2015 through 12/31/2022) | 12.8 SEER2 10.4 EER2 | 6.7 HSPF2 |
| Early retirement, split heat pumps (when applying default age) ⁸⁴ | 12.3 SEER2 10.0 EER2 | 6.7 HSPF2 |
| Early retirement, packaged heat pumps (when applying default age) ⁸⁵ | 12.3 SEER2 10.0 EER2 | 6.6 HSPF2 |
| Early retirement, heat pumps (manufactured 1/23/2006 through 12/31/2014) | 11.9 SEER2 9.7 EER2 | 6.5 HSPF2 |
| Early retirement, heat pumps (manufactured before 1/23/2006) | 9.1 SEER2 7.4 EER2 | 5.7 HSPF2 |
| All systems rated at 15.2 SEER2 or higher ⁸⁶ | 9.8 EER2 | - |
| Early retirement, electric resistance furnace ⁸⁷ | - | 3.412 HSPF2 |

5.2.1.3 High-Efficiency Condition

Rated system cooling (SEER2) and heating (HSPF2) efficiencies must meet or exceed the federal standard specified in Table 5.2-1 and Table 5.2-2. HVAC equipment with SEER2 meeting federal standard minimum requirements is eligible for early retirement cooling savings with verification of age of existing equipment and removal of functional inefficient equipment. HPs with HSPF2 meeting the minimum federal standard replacing electric resistance furnaces should follow the electric resistance documentation requirements.

Since there is no full-load efficiency requirement specified in the current federal standard, systems that comply with SEER2 and HSPF2 requirements but do not comply with the EER2 requirements outlined in Table 5.2-1 and Table 5.2-2 may still be eligible to claim savings. Systems with qualifying SEER2 and HSPF2 energy ratings are permitted to claim cooling energy savings, heating energy savings, and winter demand savings for systems, but not summer demand savings where the EER2 rating does not comply with the minimum requirement.

⁸⁴ Baseline efficiencies are calculated by taking the average the early retirement categories for 2006-2014 and 2015-2022.

⁸⁵ Ibid.

⁸⁶ When installing any system with a part-load efficiency rating of 15.2 SEER2 or higher, the reduced 9.8 EER2 full-load efficiency baseline should be applied in lieu of the applicable value presented earlier in the table except where the specified baseline EER2 value is lower than 9.8 EER2.

⁸⁷ When installing a heat pump replacing a split air conditioner with an electric resistance furnace, the reduced 3.412 HSPF2 heating baseline efficiency should be applied in lieu of the applicable value presented earlier in the table.

Split system efficiencies are driven primarily by the efficiency of the condenser unit. If the paired outdoor and indoor units are not listed on the AHRI certification listing and only provide DOE CCMS testing results, then the capacity and efficiency of the high-efficiency condition shall not exceed the average of the AHRI certification listing pairing for the matching condenser. The DOE CCMS listing provides documentation of the results that are on the AHRI certification listing and can be downloaded and filtered based on listing using a similar condenser and various indoor units.

5.2.2 Energy and Demand Savings Methodology

5.2.2.1 Savings Algorithms and Input Variables

Energy and demand savings algorithms and associated input variables are listed below.

For early retirement or rightsizing projects, attempt to determine the rated capacity of the existing unit. The rated capacity may be found on the manufacturer specification sheet for the existing unit if the new system is not available on the AHRI or DOE CCMS directories. If the model number of the existing unit is unobtainable or if the manufacturer specification sheet cannot be found, use nominal tonnage for both the existing and new unit. Never use nominal tonnage for the existing unit in combination with rated tonnage for the new unit, which can lead to overstated savings. Additionally, never use nominal tonnage to determine savings for projects where no early retirement or rightsizing has occurred.

For early retirement, if age is unknown, assume a default remaining useful life (RUL) 5 years⁸⁸. Default age may be used exclusively if applied consistently for all early retirement projects. This is the only scenario where an early retirement baseline can be applied to systems older than 24 years. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible. Default early retirement baselines are specified in Table 5.2-1 and Table 5.2-2 for use with the default age.

Energy Savings Algorithms

$$\text{Energy Savings } [\Delta kWh] = kWh_{Savings,C} + kWh_{Savings,H}$$

Equation 5.2-1

$$\text{Energy (Cooling)} [kWh_{Savings,C}] = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times EFLH_C \times \frac{1 \text{ kW}}{1,000 \text{ W}}$$

Equation 5.2-2

$$\text{Energy (Heating)} [kWh_{Savings,H}] = \left(\frac{Cap_{H,pre}}{\eta_{baseline,H}} - \frac{Cap_{H,post}}{\eta_{installed,H}} \right) \times EFLH_H \times \frac{1 \text{ kW}}{1,000 \text{ W}} \times DAF$$

Equation 5.2-3

⁸⁸ "Final Evaluation Report for X2001B: Connecticut Measure Life/EUL Update Study-Residential & Commercial". Prepared by Michaels Energy in partnership with Evergreen Economics for the Connecticut Energy Efficiency Board. p. 12-13, Table 3. May 11, 2023. https://energizect.com/sites/default/files/documents/X2001BFINALReport_051523.pdf.

Demand Savings Algorithms

$$\text{Demand Savings } [\Delta kW] = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times DF_C \times \frac{1 \text{ kW}}{1,000 \text{ W}}$$

Equation 5.2-4

Where:

$Cap_{C/H,pre}$ = For early retirement (ER), equipment cooling/heating capacity of the existing equipment; for replace-on-burnout (ROB) & new construction (NC), rated equipment cooling/heating capacity of the new equipment [Btuh]; 1 ton = 12,000 Btuh.

$Cap_{C/H,post}$ = Rated equipment cooling/heating capacity of the newly installed equipment [Btuh]; 1 ton = 12,000 Btuh.

Note: When claiming early retirement or rightsizing savings, pre- and post-capacity should be expressed as a nominal tonnage multiplied by 12,000 Btuh/ton. In all other cases, pre- and post-capacity should be set equal to the rated post-capacity at AHRI standard conditions.

$\eta_{baseline,C}$ = Baseline cooling efficiency of existing equipment (ER) or standard equipment (ROB/NC). [Btuh/W]

$\eta_{installed,C}$ = Rated cooling efficiency of the newly installed equipment (must exceed ROB/NC baseline efficiency standards in Table 5.2-1 and Table 5.2-2). [Btuh/W]

$\eta_{baseline,H}$ = Baseline heating efficiency of existing equipment (ER) or standard equipment (ROB/NC). [Btuh/W]

$\eta_{installed,H}$ = Rated heating efficiency of the newly installed equipment (must exceed baseline efficiency standards in Table 5.2-2). [Btuh/W]

Note: Use SEER2 for cooling kWh, EER2 for kW savings calculations, and HSPF2 for heating kWh savings calculations.

$EFLH_C$ = Equivalent full load hours for cooling; use 2,237 hours for San Antonio.⁸⁹

$EFLH_H$ = Equivalent full load hours for heating; use 1,101 hours for San Antonio.⁹⁰

DAF = Documentation adjustment factor; set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 5.2-3.

⁸⁹ ENERGY STAR Central AC/HP Savings Calculator. April 2009 update.

https://www.energystar.gov/sites/default/files/asset/document/ASHP_Sav_Calc.xls.

⁹⁰ Ibid.

Table 5.2-3: [Central HVAC] Demand Factors^{91,92}

| Peak Type | DF |
|-----------|------|
| NCP | 1.00 |
| CP | 0.87 |
| 4CP | 0.87 |

Early Retirement

Annual energy (kWh) and summer peak demand (kW) savings must be calculated separately for two time periods:

1. The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
2. The remaining time in the EUL period (EUL – RUL)

Annual energy and summer peak demand savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

Where:

RUL = Remaining Useful Life (see Table 5.2-4 and Table 5.2-5). If individual system components were installed at separate times, use the condenser age as a proxy for the entire system. For HPs replacing an AC with an electric resistance furnace, use the AC RUL table.

EUL = Estimated Useful Life = 20 years.

Table 5.2-4: [Central HVAC] Remaining Useful Life of Replaced ACs⁹³

| Age of Replaced Unit (years) | RUL (years) | Age of Replaced Unit (years) | RUL (years) |
|------------------------------|-------------|------------------------------|-------------|
| 1 | 16.8 | 14 | 8.6 |
| 2 | 15.8 | 15 | 8.2 |
| 3 | 14.9 | 16 | 7.9 |
| 4 | 14.1 | 17 | 7.6 |

⁹¹ Demand factors calculated in accordance with the current peak definition are lower than expected for the Texas climate. Residential HVAC measures will temporarily revert to the demand factors used in TX TRM 4.0 before the change to the peak definition. These values will be reevaluated in upcoming TRM cycles to better align with the current peak definition.

⁹² Air Conditioning Contractors of America (ACCA) Manual S recommends that residential heat pumps be sized at 115% of the maximum cooling requirement of the residence (for cooling dominated climates). Assuming that maximum cooling occurs during the peak period, the guideline leads to a demand factor of $1/1.15 = 0.87$.

⁹³ Current federal standard effective date is January 1, 2023. Existing units manufactured as of 2023 are not eligible to use the early retirement baseline and should use the ROB baseline instead.

| Age of Replaced Unit (years) | RUL (years) | Age of Replaced Unit (years) | RUL (years) |
|------------------------------|-------------|------------------------------|-------------|
| 5 | 13.3 | 18 | 7.0 |
| 6 | 12.6 | 19 | 6.0 |
| 7 | 11.9 | 20 | 5.0 |
| 8 | 11.3 | 21 | 4.0 |
| 9 | 10.8 | 22 | 3.0 |
| 10 | 10.3 | 23 | 2.0 |
| 11 | 9.8 | 24 | 1.0 |
| 12 | 9.4 | 25 ^{94,95} | 0.0 |
| 13 | 9.0 | | |

Table 5.2-5: [Central HVAC] Remaining Useful Life of Replaced HPS⁹⁶

| Age of Replaced Unit (years) | RUL (years) | Age of Replaced Unit (years) | RUL (years) |
|------------------------------|-------------|------------------------------|-------------|
| 1 | 13.7 | 12 | 7.9 |
| 2 | 12.7 | 13 | 7.6 |
| 3 | 12.0 | 14 | 7.0 |
| 4 | 11.3 | 15 | 6.0 |
| 5 | 10.7 | 16 | 5.0 |
| 6 | 10.2 | 17 | 4.0 |
| 7 | 9.7 | 18 | 3.0 |
| 8 | 9.3 | 19 | 2.0 |
| 9 | 8.9 | 20 | 1.0 |
| 10 | 8.5 | 21 ^{97,98} | 0.0 |
| 11 | 8.2 | | |

⁹⁴ RULs are capped at the 75th percentile of equipment age as determined based on DOE survival curves. Systems older than this age should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

⁹⁵ Ward, B., Bodington, N., Farah, H., Reeves, S., and Lee, L. "Considerations for early replacement of residential equipment." Prepared by the Evaluation, Measurement, and Verification (EM&V) team for the Electric Utility Marketing Managers of Texas (EUMMOT). January 2015. This document has been made available to Texas investor-owned utilities through the EM&V team's SharePoint and are available for review upon request.

⁹⁶ Current federal standard effective date is January 1, 2023. Existing units manufactured as of 2023 are not eligible to use the early retirement baseline and should use the ROB baseline instead.

⁹⁷ RULs are capped at the 75th percentile of equipment age as determined based on DOE survival curves. Systems older than this age should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

⁹⁸ Ward, B., Bodington, N., Farah, H., Reeves, S., and Lee, L. "Considerations for early replacement of residential equipment." Prepared by the Evaluation, Measurement, and Verification (EM&V) team for the Electric Utility Marketing Managers of Texas (EUMMOT). January 2015. This document has been made available to Texas investor-owned utilities through the EM&V team's SharePoint and are available for review upon request.

Derivation of RUL

ACs have an estimated useful life of 18 years, and HPs have an estimated useful life of 15 years. This estimate is consistent with the age at which approximately 50 percent of ACs and HPs installed in a given year will no longer be in service, as described by the survival functions in Figure 5.2-1 and Figure 5.2-2.

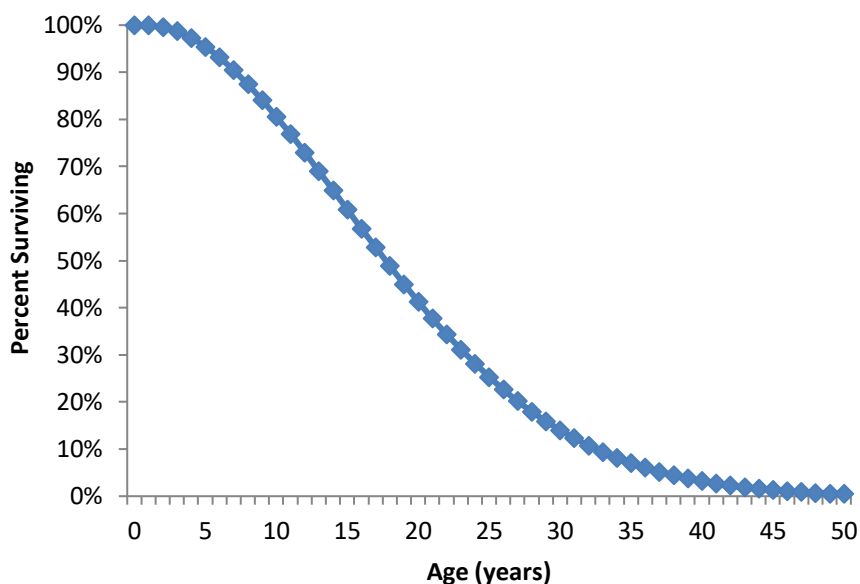


Figure 5.2-1: [Central HVAC] Survival Function for ACs⁹⁹

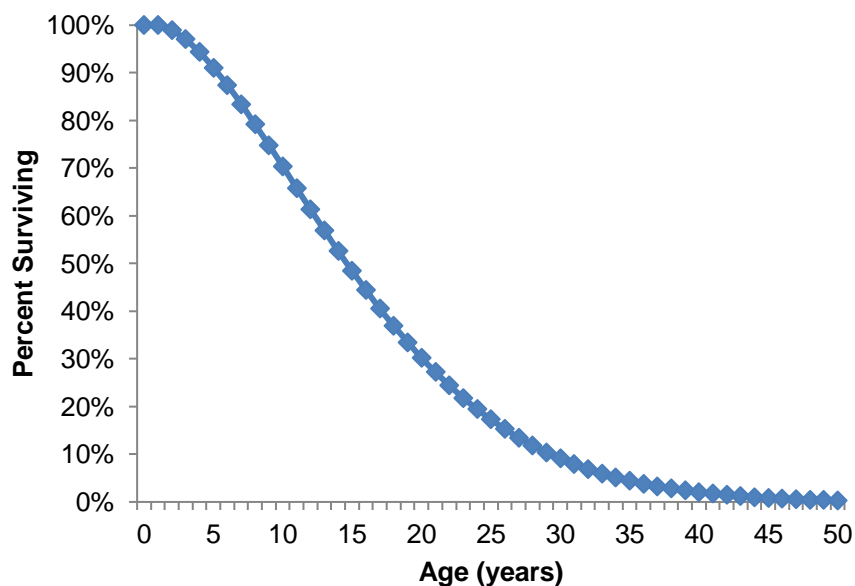


Figure 5.2-2: [Central HVAC] Survival Function for HPs¹⁰⁰

⁹⁹ Department of Energy, Federal Register, 76 FR 37408, Technical Support Document: 8.2.3.5 Lifetime. June 2011.
https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=48&action=viewlive. Download TSD at:
<http://www.regulations.gov/#!documentDetail;D=EERE-2011-BT-STD-0011-0012>.

¹⁰⁰ Ibid.

The method for estimating the remaining useful life (RUL) of a replaced system uses the age of the existing system to re-estimate the projected unit lifetime based on the survival functions shown in Figure 5.2-1 and Figure 5.2-2. The age of the system being replaced is found on the horizontal axis, and the corresponding percentage of surviving systems is determined from the chart. The surviving percentage value is then divided in half, creating a new estimated useful lifetime applicable to the current unit age. The age (year) that corresponds to this new percentage is read from the chart. RUL is estimated as the difference between that age and the current age of the system being replaced.

1.1.1.1 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.2.2.2 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.2.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 20 years for ACs and HPs based on multiple studies supportive of a 20+ year EUL for various space conditioning technologies.^{101,102}

5.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline type: ER, ROB, NC
- Manufacturer, model, and serial number of new unit
 - AHRI/DOE CCMS certificate or reference number matching model number
- Nominal cooling tonnage of retired unit (tons) (early retirement or replace-on-burnout)¹⁰³
- Cooling capacity (btuh) of the new unit
- Heating capacity (btuh) of the new unit (HPs only)

¹⁰¹ "Residential HVAC and DHW Measure Effective Useful Life Study Final Report". Group A, CALMAC ID: CPU0368.02. Prepared by DNV for the California Public Utilities Commission. p. 8, Table 1-3. April 9, 2024.

https://www.calmac.org/publications/CPUC_Group_A_2023_Res_HVAC_and_DHW_EUL_Study_Final_ReportES.pdf.

¹⁰² "Final Evaluation Report for X2001B: Connecticut Measure Life/EUL Update Study-Residential & Commercial". Prepared by Michaels Energy in partnership with Evergreen Economics for the Connecticut Energy Efficiency Board. p. 12-13, Table 3. May 11, 2023.

https://energizect.com/sites/default/files/documents/X2001BFINALReport_051523.pdf.

¹⁰³ Assume nominal baseline heating tonnage is equal to nominal baseline cooling tonnage.

- Seasonal Energy Efficiency Ratio (SEER2) and Energy Efficiency Ratio (EER2) of the new unit
- Heating Seasonal Performance Factor (HSPF2) of the new unit (HPs only)
- Replaced unit type (AC with gas furnace, AC with electric resistance furnace, air source HP)
 - Baseline equipment used for savings (if different from unit replaced)
- New unit type (central AC, central HP, dual-fuel HP, mini-split AC, mini-split HP, DC inverter AC, DC inverter HP)
- Unit type subcategory (split, packaged)
- Compressor type for newly installed unit (single stage, multi-stage)
- Age of the replaced unit (all early retirement unless default EUL is applied consistently across the program)
- Retired cooling unit model number, serial number, manufacturer, and cooling capacity (early retirement unless default EUL is applied consistently across the program; all rightsizing)
- Retired or replaced heating unit model number, serial number, manufacturer, and heating capacity (electric resistance only)
 - Photograph of retired heating unit nameplate, utility inspection, recording nameplate information, or other evaluator-approved approach. Sampling is allowed for multifamily complexes.
- Manual J load calculation or equivalent (rightsizing); see Eligibility Criteria for applicable scenarios
- Photograph of retired cooling unit nameplate (required for all rightsizing projects and early retirement projects unless default age is applied consistently across the program)
 - If a photograph of the retired unit nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (early retirement only)
 - If a photograph of the retired unit nameplate is unavailable or not legible, provide estimated square footage of conditioned area served by the retired unit (rightsizing only)
- Photograph demonstrating functionality of existing equipment and/or customer responses to survey questionnaire documenting the condition of the replaced unit and their motivation for measure replacement for early retirement eligibility determination (early retirement only). This requirement also applies to projects using the default age.

- For installed HVAC systems equal to minimum federal standard SEER2 efficiency:
 - Age of removed equipment
 - Proof of functionality of removed equipment
 - Rated SEER of removed equipment, if available
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

5.2.4 Document Revision History

Table 5.2-6: [Central HVAC] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Defined rightsizing and documentation requirements. Updated early retirement age eligibility. |
| FY 2026 | Clarified documentation requirements and minimum efficiency. Updated early retirement eligibility. |

5.3 ENERGY STAR® ROOM AIR CONDITIONERS

5.3.1 Measure Description

The following deemed savings values are applicable to the installation of a high-efficiency room air conditioner (RAC).

5.3.1.1 Eligibility Criteria

Installed RACs must comply with the current ENERGY STAR specification for RACs.

To claim early retirement savings, the replaced unit must be functioning at the time of removal with a maximum age of 12 years, coinciding with the point at which there is no assumed remaining useful life.

5.3.1.2 Baseline Condition

For new construction (NC) and replace-on-burnout (ROB), the baseline is assumed to be a new room air conditioning unit that is compliant with the current federal standard, effective June 1, 2014.¹⁰⁴ The standard refers to a revised efficiency rating, Combined Energy Efficiency Ratio (CEER), which accounts for standby/off-mode energy usage.

For early retirement (ER), the baseline efficiency is assumed to match the minimum federal standard efficiencies in place prior to June 1, 2014. Since the effective date occurred mid-year, existing systems manufactured as of 2015 are not eligible for early retirement.

A new federal standard went into effect on August 30, 2023. However, this standard does not require manufacturer compliance until May 26, 2026.¹⁰⁵

¹⁰⁴ Legacy DOE minimum efficiency standard for residential RACs effective during current federal standard manufacturer lag period. <https://www.ecfr.gov/current/title-10/chapter-II/subchapter-D/part-430/subpart-C/section-430.32>.

¹⁰⁵ Current DOE minimum efficiency standard for residential room air conditioners. <https://www.regulations.gov/document/EERE-2014-BT-STD-0059-0057>.

Table 5.3-1: [Room ACs] Baseline Efficiencies

| Reverse Cycle (Yes/No) | Louvered Sides (Yes/No) | Capacity (Btu/hr) | Federal Standard prior to June 1, 2014 | Federal Standard as of June 1, 2014 |
|---------------------------|----------------------------|-------------------|---|--|
| | | | ER Baseline EER | NC/ROB Baseline CEER |
| No | Yes | < 6,000 | 9.7 | 11.0 |
| | | 6,000-7,999 | 9.7 | 11.0 |
| | | 8,000-13,999 | 9.8 | 10.9 |
| | | 14,000-19,999 | 9.7 | 10.7 |
| | | 20,000-27,999 | 8.5 | 9.4 |
| | | ≥ 28,000 | 8.5 | 9.0 |
| No | No | < 6,000 | 9.0 | 10.0 |
| | | 6,000-7,999 | 9.0 | 10.0 |
| | | 8,000-10,999 | 8.5 | 9.6 |
| | | 11,000-13,999 | 8.5 | 9.5 |
| | | 14,000-19,999 | 8.5 | 9.3 |
| | | ≥ 20,000 | 8.5 | 9.4 |
| Yes | Yes | < 20,000 | 9.0 | 9.8 |
| | | ≥ 20,000 | 8.5 | 9.3 |
| Yes | No | < 14,000 | 8.5 | 9.3 |
| | | ≥ 14,000 | 8.0 | 8.7 |
| Casement-only | | All capacities | 8.7 | 9.5 |
| Casement-slider | | All capacities | 9.5 | 10.4 |

5.3.1.3 High-Efficiency Condition

The table below displays the ENERGY STAR Final Version 5.0 Requirements for eligible room air conditioners effective October 30, 2023.¹⁰⁶ Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

¹⁰⁶ ENERGY STAR Room Air Conditioners Final Version 5.0 Program Requirements.

<https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%205.0%20Room%20Air%20Conditioners%20Specification%20and%20Partner%20Commitments.pdf>.

Table 5.3-2: [Room ACs] Efficient Condition Specification

| Reverse Cycle (Yes/No) | Louvered Sides (Yes/No) | Capacity (Btu/hr) | Minimum CEER ¹⁰⁷ |
|------------------------|-------------------------|-------------------|-----------------------------|
| No | Yes | < 6,000 | 13.1 |
| | | 6,000-7,999 | 13.7 |
| | | 8,000-13,999 | 14.7 |
| | | 14,000-19,999 | 14.4 |
| | | 20,000-27,999 | 12.7 |
| | | ≥ 28,000 | 12.2 |
| No | No | < 6,000 | 12.8 |
| | | 6,000-7,999 | 12.8 |
| | | 8,000-10,999 | 13.0 |
| | | 11,000-13,999 | 12.8 |
| | | 14,000-19,999 | 12.6 |
| | | ≥ 20,000 | 12.7 |
| Yes | Yes | < 20,000 | 13.2 |
| | | ≥ 20,000 | 12.6 |
| Yes | No | < 14,000 | 12.6 |
| | | ≥ 14,000 | 11.7 |
| Casement-only | | All capacities | 12.8 |
| Casement-slider | | All capacities | 14.0 |

5.3.2 Energy and Demand Savings Methodology

5.3.2.1 Savings Algorithms and Input Variables

Energy Savings

New Construction or Replace-on-Burnout

$$\text{Energy Savings } [\Delta kWh] = \frac{Cap_C}{1,000} \times AOH_C \times \left(\frac{1}{CEER_{Base}} - \frac{1}{CEER_{RAC}} \right)$$

Equation 5.3-1

¹⁰⁷ The updated ENERGY STAR specification discontinues the five percent energy credit for “connected functionality”.

Where:

| | | |
|---------------|---|--|
| Cap_c | = | Rated equipment cooling capacity of the installed RAC [Btu/hr]. |
| AOH_c | = | Annual operating hours for cooling = 1,351 hours. ¹⁰⁸ |
| $CEER_{Base}$ | = | Combined Energy Efficiency Ratio of the baseline cooling equipment; see Table 5.3-1. |
| $CEER_{RAC}$ | = | Combined Energy Efficiency Ratio of the installed RAC. |
| 1,000 | = | Constant to convert from watts to kilowatts. |

Early Retirement

Annual energy (kWh) and peak demand (kW) savings must be calculated separately for two time periods:

1. The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
2. The remaining time in the EUL period (EUL – RUL)

Annual energy (kWh) savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

Where:

| | | |
|-------|---|---|
| RUL | = | Remaining Useful Life (see Table 5.3-3); if unknown, assume the age of the replaced unit is equal to the EUL resulting in a default RUL of 3 years. |
| EUL | = | Estimated Useful Life = 10 years. |

Table 5.3-3: [Room ACs] Remaining Useful Life (RUL)

| Age of Replaced Unit (years) | RUL (years) | Age of Replaced Unit (years) | RUL (years) |
|------------------------------|--------------------|------------------------------|-------------|
| 1 | 8.0 ¹⁰⁹ | 8 | 5.0 |
| 2 | 7.2 | 9 | 4.0 |
| 3 | 6.2 | 10 | 3.0 |
| 4 | 5.2 | 11 | 2.0 |
| 5 | 5.2 | 12 | 1.0 |

¹⁰⁸ Association of Home Appliance Manufacturers (AHAM) Room Air Conditioner Cooling Calculator.

¹⁰⁹ Capped at EUL because RUL cannot exceed EUL.

| Age of Replaced Unit (years) | RUL (years) | Age of Replaced Unit (years) | RUL (years) |
|------------------------------|-------------|------------------------------|-------------|
| 6 | 5.2 | 13 ^{110,111} | 0.0 |
| 7 | 5.2 | | |

For the RUL period:

$$kWh_{savings,ER} = \frac{Cap_C}{1,000} \times AOH_C \times \left(\frac{1}{EER_{ER}} - \frac{1}{CEER_{RAC}} \right)$$

Equation 5.3-2

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

$$kWh_{savings,ROB} = \frac{Cap_C}{1,000} \times AOH_C \times \left(\frac{1}{CEER_{ROB}} - \frac{1}{CEER_{RAC}} \right)$$

Equation 5.3-3

Where:

$CEER_{ROB}$ = Combined Energy Efficiency Ratio of the replace-on-burnout baseline cooling equipment; see Table 5.3-1.

EER_{ER} = Energy Efficiency Ratio of the early retirement baseline cooling equipment; see Table 5.3-1.

Demand Savings

New Construction or Replace-on-Burnout

$$Demand\ Savings\ [\Delta kW] = \frac{Cap_C}{1,000} \times \left(\frac{1}{CEER_{Base}} - \frac{1}{CEER_{RAC}} \right) \times DF$$

Equation 5.3-4

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 5.3-4.

Early Retirement

To calculate demand savings for the early retirement of a RAC, a similar methodology is used as for replace-on-burnout installations, with separate savings calculated for the remaining useful life of the

¹¹⁰ RULs are capped at the 75th percentile of equipment age, 13 years, based on DOE survival curves. Systems older than 13 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

¹¹¹ Ward, B., Bodington, N., Farah, H., Reeves, S., and Lee, L. "Considerations for early replacement of residential equipment." Prepared by the Evaluation, Measurement, and Verification (EM&V) team for the Electric Utility Marketing Managers of Texas (EUMMOT). January 2015.

unit, and the remainder of the EUL as outlined in the section above.

For the RUL period:

$$kW_{Savings,ER} = \frac{Cap_C}{1,000} \times \left(\frac{1}{EER_{ER}} - \frac{1}{EER_{RAC}} \right) \times DF$$

Equation 5.3-5

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

$$kW_{Savings,ROB} = \frac{Cap_C}{1,000} \times \left(\frac{1}{EER_{ROB}} - \frac{1}{EER_{RAC}} \right) \times DF$$

Equation 5.3-6

Table 5.3-4: [Room ACs] Demand Factors^{112,113}

| Peak Type | DF |
|-----------|------|
| NCP | 1.00 |
| CP | 0.87 |
| 4CP | 0.87 |

¹¹² Demand factors calculated in accordance with the current peak definition are lower than expected for the Texas climate. Residential HVAC measures will temporarily revert to the demand factors used in TX TRM 4.0 before the change to the peak definition. These values will be reevaluated in upcoming TRM cycles to better align with the current peak definition.

¹¹³ Air Conditioning Contractors of America (ACCA) Manual S recommends that residential heat pumps be sized at 115% of the maximum cooling requirement of the residence (for cooling dominated climates). Assuming that maximum cooling occurs during the peak period, the guideline leads to a demand factor of $1/1.15 = 0.87$.

Derivation of RULs

RACs have an estimated useful life of 10 years. This estimate is consistent with the age at which approximately 50 percent of the RACs installed in a given year will no longer be in service, as described by the survival function in Figure 5.3-1.

The method for estimating the remaining useful life (RUL) of a replaced system uses the age of the existing system to re-estimate the survival function shown in Figure 5.3-1. The age of the RAC being replaced is found on the horizontal axis, and the corresponding percentage of surviving RACs is determined from the chart. The surviving percentage value is then divided in half, creating a new percentage. Then, the age (year) that corresponds to this new percentage is read from the chart. RUL is estimated as the difference between that age and the current age of the system being replaced.

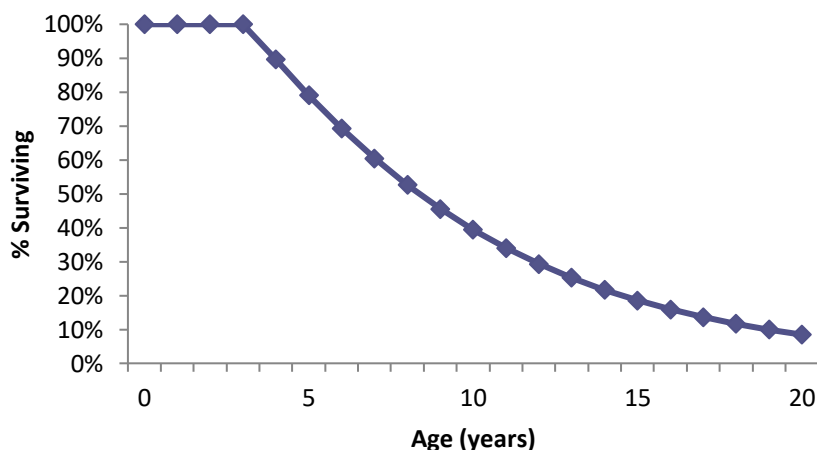


Figure 5.3-1: [Room ACs] Survival Function¹¹⁴

1.1.1.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.3.2.2 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.3.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for RACs based on the Technical Support Document for the

¹¹⁴ Department of Energy, Federal Register, 76 FR 22454, Technical Support Document: 8.2.2.6 Product Lifetime. April 2011.
http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/41. Download TSD at:
<http://www.regulations.gov/#!documentDetail;D=EERE-2007-BT-STD-0010-0053>.

current DOE Final Rule standards for RACs. This value is consistent with the EUL reported in the Department of Energy 76 Final Rule 52852 Technical Support Document for RACs.¹¹⁵

5.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline type: ER, ROB, NC
- Manufacturer, model, and serial number of new unit
 - ENERGY STAR certificate matching model number
- Cooling capacity of the installed unit (Btu/hr)
- Combined Energy Efficiency Ratio (CEER) of the new unit
- Age of the replaced unit (early retirement only)
- Photograph of the retired unit nameplate (early retirement only)
 - If a photograph of the retired unit nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (early retirement only)
- Photograph demonstrating functionality of existing equipment and/or customer responses to survey questionnaire documenting the condition of the replaced unit and their motivation for measure replacement for early retirement eligibility determination (early retirement only)
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

5.3.4 Document Revision History

Table 5.3-5: [Room ACs] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Incorporated updated DOE final rule and ENERGY STAR specification v5.0. Updated early retirement age eligibility. |
| FY 2026 | No revision. |

¹¹⁵ Technical Support Document: Room Air Conditioners, June 2020, p. ES-14. <https://www.regulations.gov/document/EERE-2014-BT-STD-0059-0013>.

5.4 PACKAGED TERMINAL HEAT PUMPS

5.4.1 Measure Description

This section presents the deemed savings methodology for the installation of packaged terminal heat pumps (PTHP) replacing packaged terminal air conditioners (PTAC) with electric resistance heat. This measure covers assumptions made for baseline equipment efficiencies for early retirement (ER) and replace-on-burnout (ROB), based current and previous on efficiency standards. For ER, the actual age of the baseline system should be determined from the equipment nameplate or other physical documentation whenever possible. Default values are provided for when the actual age of the unit is unknown.

Applicable efficient measure types are restricted to packaged terminal heat pumps. Both standard and non-standard size equipment types are covered. Standard size refers to equipment with wall sleeve dimensions having an external wall opening greater than, equal to 16 inches high or greater than, or equal to 42 inches wide and a cross-sectional area greater than 670 in². Non-standard size refers to equipment with existing wall sleeve dimensions having an external wall opening of fewer than 16 inches high or fewer than 42 inches wide and a cross-sectional area less than 670 in².

5.4.1.1 Eligibility Criteria

Existing PTAC and installed PTHP must be the primary cooling source in the residence. Installed PTHPs must be compliant with the current commercial code.

ER projects must involve the replacement of a working system before natural burnout. Additionally, the ER approach cannot be used for projects involving a simultaneous renovation where a major structural change or internal space remodel has occurred. A ROB approach should be used for these scenarios.

Manufacturer datasheets for new equipment or documentation of AHRI or DOE CCMS certification must be provided.^{116,117}

5.4.1.2 Baseline Condition

Early Retirement

Two baseline condition efficiency values are required for an ER scenario, one for the ER (RUL) period and one for the ROB (EUL-RUL) period. For the ROB period, the baseline efficiency is the same as for a ROB scenario. For the ER period, the baseline efficiency should be estimated according to the capacity, system type (PTAC), and age (based on year of manufacture) of the replaced system.¹¹⁸ When the system age can be determined (from a nameplate, building prints, equipment inventory list, etc.), the

¹¹⁶ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

¹¹⁷ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

¹¹⁸ The actual age should be determined from the nameplate, building prints, equipment inventory list, etc. and whenever possible the actual source used should be identified in the project documentation.

baseline efficiency levels provided in Table 5.4-1, reflecting ASHRAE Standard 90.1-2001 through 90.1-2007, should be used. PTHPs replacing PTACs with built-in electric resistance heat should use a baseline heating efficiency of 1.0 COP.

When the system age is unknown, assume 15 years.¹¹⁹ A default RUL may be used exclusively if applied consistently for all eligible early retirement projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible.

Existing systems manufactured as of February 2013 are not eligible for early retirement.

Table 5.4-1: [PTHPs] ER Baseline Efficiency Levels for Standard Size PTACs^{120,121}

| Equipment | Cooling Capacity (Btu/hr) | Baseline Cooling Efficiency (EER) | Baseline Heating Efficiency (COP) – without built-in resistance heat | Baseline Heating Efficiency (COP) – replacing built-in resistance heat |
|-----------|---------------------------|--|--|--|
| PTAC | < 7,000 | 11.0 | - | 1.0 |
| | 7,000-15,000 | $12.5 - (0.213 \times \text{Cap}/1,000)$ | | |
| | > 15,000 | 9.3 | | |

Replace-on-Burnout

Table 5.4-2 provides minimum efficiency standards for PTAC/PTHP units and reflects the federal standard for Packaged Terminal Air Conditioners and Heat Pumps. These values are closely aligned with the federal standards for packaged terminal air-conditioners and heat pumps effective February 2013 and reflected in 10 CFR 431.

¹¹⁹ As noted in Docket 40885, page 14-15: Failure probability weights are established by assuming that systems for which age information will be unavailable are likely to be older, setting a minimum age threshold, and using the survival functions for the relevant system type to estimate the likelihood that an operational system is of a given age beyond that threshold. Baseline efficiency for each year of system age is established relative to program year. Baseline efficiency levels can be estimated for the next ten program years, considering increments in efficiency standards that took place in the historical period.

¹²⁰ ER only applies to standard size units because the minimum efficiency requirements for non-standard systems have never changed, making the ER baseline efficiency the same as for ROB.

¹²¹ Cap refers to the rated cooling capacity in Btuh. If the capacity is less than 7,000 Btuh, use 7,000 Btuh in the calculation. If the capacity is greater than 15,000 Btuh, use 15,000 Btuh in the calculation.

Table 5.4-2: [PTHPs] ROB Baseline Efficiency Levels for PTHPs^{122,123}

| Equipment | Category | Cooling Capacity (Btu/hr) | Baseline Cooling Efficiency (EER) | Baseline Heating Efficiency (COP) | Baseline Heating Efficiency (COP) (replacing built-in resistance heat) |
|-----------|-------------------|---------------------------|--|---|--|
| PTHP | Standard Size | < 7,000 | 11.9 | 3.3 | 1.0 |
| | | 7,000-15,000 | $14.0 - (0.300 \times \text{Cap}/1,000)$ | $3.7 - (0.026 \times \text{Cap}/1,000)$ | |
| | | > 15,000 | 9.5 | 2.9 | |
| | Non-Standard Size | < 7,000 | 9.3 | 2.7 | |
| | | 7,000-15,000 | $10.8 - (0.213 \times \text{Cap}/1,000)$ | $2.9 - (0.026 \times \text{Cap}/1,000)$ | |
| | | > 15,000 | 7.6 | 2.5 | |

5.4.1.3 High-Efficiency Condition

The high-efficiency retrofits must exceed the minimum federal standards found in Table 5.4-2.

The high-efficiency retrofits must also meet the following criteria:¹²⁴

- For ER projects only, the installed equipment cooling capacity must be within 80 percent to 120 percent of the replaced electric cooling capacity.
- No additional measures are being installed that directly affect the operation of the cooling equipment (i.e., control sequences).

¹²² IECC 2018 Table C403.3.2(3).

¹²³ Cap refers to the rated cooling capacity in Btuh. If the capacity is less than 7,000 Btuh, use 7,000 Btuh in the calculation. If the capacity is greater than 15,000 Btuh, use 15,000 Btuh in the calculation.

¹²⁴ Modified from PUCT Docket #41070 for TRMv3 to limit replacement of only smaller-sized units and extend early retirement to cover PTAC/PTHP.

5.4.2 Energy and Demand Savings Methodology

5.4.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{Savings,C} + kWh_{Savings,H}$$

Equation 5.4-1

$$\text{Energy Savings (Cooling)} [kWh_{Savings,C}] = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times \frac{EFLH_C}{1,000}$$

Equation 5.4-2

$$\text{Energy Savings (Heating)} [kWh_{Savings,H}] = \left(\frac{Cap_{H,pre}}{\eta_{baseline,H}} - \frac{Cap_{H,post}}{\eta_{installed,H}} \right) \times \frac{EFLH_H}{3,412}$$

Equation 5.4-3

Where:

| | | |
|----------------------|---|---|
| $Cap_{C/H,pre}$ | = | For ER, rated equipment cooling/heating ¹²⁵ capacity of the existing equipment at AHRI standard conditions; for ROB & NC, rated equipment cooling/heating capacity of the new equipment at AHRI standard conditions [Btuh]; 1 ton = 12,000 Btuh. |
| $Cap_{C/H,post}$ | = | Rated equipment cooling/heating capacity of the newly installed equipment at AHRI standard conditions [Btuh]; 1 ton = 12,000 Btuh. |
| $\eta_{baseline,C}$ | = | Cooling efficiency of existing (ER) or standard (ROB/NC) equipment [EER, Btu/W-h]; see Table 5.4-1 and Table 5.4-2. |
| $\eta_{baseline,H}$ | = | Heating efficiency of existing (ER) or standard (ROB/NC) equipment [COP]; see Table 5.4-1 and Table 5.4-2. |
| $\eta_{installed,C}$ | = | Rated cooling efficiency of the newly installed equipment [EER, Btu/W-h]. Rated cooling efficiency must exceed minimum federal standards found in Table 5.4-2. ¹²⁶ |
| $\eta_{installed,H}$ | = | Rated heating efficiency of the newly installed equipment [COP]. Rated heating efficiency must exceed minimum federal standards found in Table 5.4-2. ¹²⁷ |

¹²⁵ Baseline cooling capacity refers to the rated cooling capacity of the existing PTAC. Assume baseline heating capacity is equal to rated heating capacity for newly installed PTHP.

¹²⁶ Rated efficiency is commonly reported at both 230V and 208V. Savings calculations should reference efficiency at 230V, as AHRI rating conditions specify that voltage.

¹²⁷ Ibid.

| | | |
|----------|---|---|
| $EFLH_c$ | = | Equivalent full load hours for cooling. Use 2,237 hours for San Antonio. ¹²⁸ |
| $EFLH_H$ | = | Equivalent full load hours for heating. Use 1,101 hours for San Antonio. ¹²⁹ |
| 1,000 | = | Constant to convert from watts to kilowatts. |
| 3,412 | = | Constant to convert from Btu to kWh. |

The first-year savings algorithms in the above equations are used for all HVAC projects, across ROB and ER projects. However, ER projects require weighted savings calculated over both the ER and ROB periods taking the EUL and RUL into account. The ER savings are applied over the remaining useful life (RUL) period, and the ROB savings are applied over the remaining period (EUL-RUL). The final reported savings for ER projects are not actually a “first-year” savings, but an “average annual savings over the lifetime (EUL) of the measure.” These savings calculations are explained in in Section 22.1.

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \left(\frac{Cap_{c,pre}}{\eta_{baseline,C}} - \frac{Cap_{c,post}}{\eta_{installed,C}} \right) \times \frac{DF}{1,000}$$

Equation 5.4-4

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 5.4-3.

Table 5.4-3: [PTHPs] Demand Factors^{130,131}

| Peak Type | DF |
|-----------|------|
| NCP | 1.00 |
| CP | 0.87 |
| 4CP | 0.87 |

1.1.1.3 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

¹²⁸ ENERGY STAR Central AC/HP Savings Calculator. April 2009 update.
https://www.energystar.gov/sites/default/files/asset/document/ASHP_Sav_Calc.xls.

¹²⁹ Ibid.

¹³⁰ Demand factors calculated in accordance with the current peak definition are lower than expected for the Texas climate. Residential HVAC measures will temporarily revert to the demand factors used in TX TRM 4.0 before the change to the peak definition. These values will be reevaluated in upcoming TRM cycles to better align with the current peak definition.

¹³¹ Air Conditioning Contractors of America (ACCA) Manual S recommends that residential heat pumps be sized at 115% of the maximum cooling requirement of the residence (for cooling dominated climates). Assuming that maximum cooling occurs during the peak period, the guideline leads to a demand factor of $1/1.15 = 0.87$.

5.4.2.2 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.4.2.3 Measure Life and Lifetime Savings

Estimated Useful Life (EUL)

The EUL is 15 years for PTHPs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID HVAC-PTHP.¹³²

Remaining Useful Life (RUL) for PTAC/PTHP Systems

Annual energy (kWh) and peak demand (kW) savings must be calculated separately for two time periods:

1. The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
2. The remaining time in the EUL period (EUL – RUL)

Annual energy (kWh) savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

Where:

RUL = Remaining Useful Life (see Table 5.4-4); if unknown, assume the age of the replaced unit is equal to the EUL resulting in a default RUL of 2.8 years.

EUL = Estimated Useful Life = 15 years.

Table 5.4-4: [PTHPs] Remaining Useful Life or Replaced Unit¹³³

| Age of Replaced System (Years) | RUL (Years) | Age of Replaced System (Years) | RUL (Years) |
|--------------------------------|-------------|--------------------------------|-------------|
| 1 | 14.0 | 10 | 5.7 |
| 2 | 13.0 | 11 | 5.0 |
| 3 | 12.0 | 12 | 4.4 |
| 4 | 11.0 | 13 | 3.8 |
| 5 | 10.0 | 14 | 3.3 |

¹³² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

¹³³ Current NC baseline matches the baseline for existing systems manufactured in 2018. Existing systems manufactured after 1/1/2018 are not eligible to use the early retirement baseline.

| Age of Replaced System (Years) | RUL (Years) | Age of Replaced System (Years) | RUL (Years) |
|--------------------------------|-------------|--------------------------------|-------------|
| 6 | 9.1 | 15 | 2.8 |
| 7 | 8.2 | 16 | 2.0 |
| 8 | 7.3 | 17 | 1.0 |
| 9 | 6.5 | 18 ¹³⁴ | 0.0 |

5.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline type: ER, ROB
- Baseline unit equipment type (PTAC with electric resistance heat)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
- Baseline unit quantity
- Baseline rated cooling capacity
- For ER ONLY:
 - Baseline Age and Method of Determination (e.g., nameplate, blueprints, customer reported, not available)
 - Photograph of retired unit nameplate demonstrating model number, serial number, and manufacturer; if photograph of nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (alternate forms of documentation can be approved at the evaluator's discretion)
 - Documentation demonstrating the functionality of existing equipment, including but not limited to photograph demonstrating the functionality of existing equipment or customer responses to survey questionnaire documenting the condition of the replaced unit and their motivation for measure replacement for early retirement eligibility determination

¹³⁴ RULs are capped at the 75th percentile of equipment age, 18 years, as determined based on DOE survival curves. Systems older than 18 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

- Manufacturer, model, and serial number of new unit
 - AHRI/DOE CCMS certificate or reference number matching model number
- New unit equipment type (PTHP)
- New unit equipment configuration category: standard/non-standard (PTAC/PTHP only)
- New unit quantity
- New unit rated cooling and heating capacities
- New unit cooling and heating efficiency ratings
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

5.4.4 Document Revision History

Table 5.4-5: [PTHPs] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Updated early retirement age eligibility. |
| FY 2026 | No revision. |

5.5 ENERGY STAR® GROUND SOURCE HEAT PUMPS

5.5.1 Measure Description

This measure requires the installation of a ground-source heat pump (GSHP) meeting the minimum requirements of ENERGY STAR geothermal heat pump key product criteria. Savings calculations are presented for systems with and without desuperheaters.

5.5.1.1 Eligibility Criteria

The deemed savings apply to units with a capacity of $\leq 65,000$ Btu/hour.

Energy savings for desuperheaters only apply if the desuperheater is attached to an electric storage water heater. The electric storage water heating cannot replace a gas water heater in a retrofit installation.

5.5.1.2 Baseline Condition

The baseline unit is assumed to be an air-source heat pump (ASHP) for new construction, and either an ASHP or an air conditioner with an electric resistance furnace for replace-on-burnout projects. New construction baseline efficiency values for ASHPs comply with the current federal minimum standard, effective January 1, 2023.¹³⁵

For replace-on-burnout (ROB) projects, the cooling baseline is reduced to 13.7 SEER2. This value incorporates an adjustment to the baseline SEER2 value to reflect the percentage of current replacements that do not include the installation of an AHRI-matched system.¹³⁶ The heating baseline for replace-on-burnout projects is dependent on the heating type of the baseline equipment.

Table 5.5-1: [GSHPs] Baseline Efficiencies

| Project Type | Cooling Mode ¹³⁷ | Heating Mode ¹³⁸ |
|------------------|-----------------------------|-----------------------------|
| New Construction | 9.8 EER2 14.3 SEER2 | 2.2 COP 7.5 HSPF2 |

¹³⁵ DOE minimum efficiency standard for residential air conditioners/heat pumps.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=48&action=viewlive.

¹³⁶ Frontier Energy on behalf of the Electric Utility Marketing Managers of Texas (EUMMOT). "Petition to revise Existing Commission-Approved Deemed Savings Values for Central Air Conditioning and Heat Pump Systems: Docket No. 36780." Public Utility Commission of Texas. Approved August 27, 2009. <https://interchange.puc.texas.gov/>. Adapted for new 14 SEER baseline.

¹³⁷ The Central HP EER2 baseline is reduced to 9.8 EER2 for systems rated at 15.2 SEER2 or higher. While GSHPs do not have a SEER2 rating, all full-load EER minimum efficiency requirements exceed that threshold. Therefore, the reduced EER2 baseline is extended to all GSHP installations.

¹³⁸ Code specified HSPF value converted to COP using $\text{COP} = \text{HSPF} \times 1,055 \text{ J/Btu} \div 3,600 \text{ J/W-h} = \text{HSPF} \div 3.412$.

| Project Type | Cooling Mode ¹³⁷ | Heating Mode ¹³⁸ |
|---|-----------------------------|-----------------------------|
| ROB – Air Source Heat Pump Baseline | 9.8 EER2 13.7 SEER2 | 2.2 COP 7.5 HSPF2 |
| ROB – Air Conditioner with Electric Resistance Furnace Baseline | | 1.0 COP 3.412 HSPF2 |

5.5.1.3 High-Efficiency Condition

Table 5.5-2 displays the ENERGY STAR Final Version 3.2 requirements for eligible geothermal heat pumps, effective January 1, 2012.¹³⁹ Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

Table 5.5-2: [GSHPs] ENERGY STAR Efficiency Requirements

| Project Type | Cooling Mode (EER) | Heating Mode (COP) |
|----------------------------|--------------------|--------------------|
| Closed Loop Water-to-Air | 17.1 | 3.6 |
| Open Loop Water-to-Air | 21.1 | 4.1 |
| Closed Loop Water-to-Water | 16.1 | 3.1 |
| Open Loop Water-to-Water | 20.1 | 3.5 |
| Direct Geoexchange (DGX) | 16.0 | 3.6 |

The specifications in the charts above apply to single-stage models. Multi-stage models may be qualified based on:¹⁴⁰

$$EER = (\text{highest rated capacity EER} + \text{lowest rated capacity EER}) \div 2$$

Equation 5.5-1

$$COP = (\text{highest rated capacity COP} + \text{lowest rated capacity COP}) \div 2$$

Equation 5.5-2

5.5.2 Energy and Demand Savings Methodology

5.5.2.1 Savings Algorithms and Input Variables

Peak demand and annual energy savings for GSHP systems should be calculated as shown below. Where a desuperheater is also installed, an additional factor is included in the calculations to account for estimated additional energy and demand savings.

¹³⁹ ENERGY STAR Program Requirements Product Specification for Geothermal Heat Pumps, v3.2.

<https://www.energystar.gov/sites/default/files/Geothermal%20Heat%20Pump%20Version%203.2%20Final%20Specification.pdf>.

¹⁴⁰ Geothermal Heat Pumps Key Product Criteria,

https://www.energystar.gov/products/heating_cooling/heat_pumps_geothermal/key_product_criteria.

Energy and demand savings for desuperheaters were adapted from a 2001 study conducted by Oak Ridge National Laboratory (ORNL) on ground source heat pumps in Texas.¹⁴¹ Desuperheater savings were calculated by taking the difference in savings between GSHPs with and without desuperheaters and averaging the savings between low and high efficiency units. Savings for GSHP systems with desuperheaters should be calculated using the algorithms below with an additional energy credit based on the system capacity and efficiency.

The ORNL study draws from a 1998 analysis based on a study conducted at the Fort Polk Joint Readiness Training Center in Leesville, Louisiana. The Fort Polk study used calibrated simulations of 200 multifamily residences in the complex to estimate energy savings attributable to replacement of air source heat pumps with ground source heat pumps. These estimates were found to be within 5% of actual post-retrofit savings. Building models were developed using TRNSYS.¹⁴²

Using the Fort Polk models, the ORNL study assumed a baseline of a 1.5-ton, 10 SEER air source heat pump. Simulations of low-, medium-, and high-efficiency ground source heat pumps with and without desuperheaters were compared against the baseline unit. The models were run using TMY-2 weather profiles for the San Antonio climate zone. Energy and demand differences between the pre- and post-retrofit models were used to estimate average savings per ton of cooling capacity.

In the 1998 analysis, low-efficiency GSHPs were assumed to be units with an EER of 12.4 and capacity of 19 kBtuh, while medium-efficiency units had an EER of 16.8 and capacity of 21 kBtuh. High-efficiency units had an EER of 18.3, with a capacity of 22 kBtuh.

These models were used to derive the energy and demand savings associated with installation of a desuperheater along with a ground source heat pump.

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{Savings,C} + kWh_{Savings,H} + kWh_{DS}$$

Equation 5.5-3

$$\text{Energy Savings (Cooling)} [kWh_{Savings,C}] = Cap_C \times \frac{EFLH_C}{1,000} \times \left(\frac{1}{EER_{Base}} - \frac{1}{EER_{GSHP}} \right)$$

Equation 5.5-4

$$\text{Energy Savings (Heating)} [kWh_{Savings,H}] = Cap_H \times \frac{1 \text{ kWh}}{3,412 \text{ Btu}} \times EFLH_H \times \left(\frac{1}{COP_{Base}} - \frac{1}{COP_{GSHP}} \right)$$

Equation 5.5-5

¹⁴¹ Shonder, J. A., Hughes, P., and Thornton, J. Development of Deemed Energy and Demand Savings for Residential Ground Source Heat Pump Retrofits in the State of Texas. Transactions-American Society of Heating, Refrigerating, and Air Conditioning Engineers. 108, no. 1: 953-961, 2001. <http://web.ornl.gov/~webworks/cpr/v2001/pres/112677.pdf>.

¹⁴² Klein, S. A. TRNSYS Manual: A Transient Simulation Program. Solar Engineering Laboratory, University of Wisconsin-Madison, Version 14.2 for Windows, September 1996.

Where:

| | | |
|--------------|---|--|
| kWh_{DS} | = | Annual energy savings [kWh] associated with installation of a desuperheater = 802 kWh. These savings should only be added if a desuperheater is installed. |
| Cap_c | = | Rated equipment cooling capacity of the installed GSHP [Btu/hr]. |
| Cap_H | = | Rated equipment heating capacity of the installed GSHP [Btu/hr]. |
| $EFLH_C$ | = | Equivalent full load hours for cooling. Use 2,237 hours for San Antonio. ¹⁴³ |
| $EFLH_H$ | = | Equivalent full load hours for heating. Use 1,101 hours for San Antonio. ¹⁴⁴ |
| EER_{Base} | = | Energy Efficiency Ratio of the baseline cooling equipment; see Table 5.5-1. |
| EER_{GSHP} | = | Energy Efficiency Ratio of the installed GSHP. |
| COP_{Base} | = | Coefficient of Performance of the baseline heating equipment; see Table 5.5-1. |
| COP_{GSHP} | = | Coefficient of Performance of the installed GSHP. |
| 1,000 | = | Constant to convert from watts to kilowatts. |
| 3,412 | = | Constant to convert from Btu to kWh. |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{Cap_c}{1,000} \times \left(\frac{1}{EER_{Base}} - \frac{1}{EER_{GSHP}} \right) \times DF + kW_{DS}$$

Equation 5.5-6

Where:

| | | |
|-----------|---|---|
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 5.5-3. |
| kW_{DS} | = | Demand savings [kW] associated with installation of a desuperheater = 0.405 kW. These savings should only be added if a desuperheater is installed. |

¹⁴³ ENERGY STAR Central AC/HP Savings Calculator. April 2009 update.
https://www.energystar.gov/sites/default/files/asset/document/ASHP_Sav_Calc.xls.

¹⁴⁴ Ibid.

Table 5.5-3: [GSHPs] Demand Factors^{145,146}

| Peak Type | DF |
|-----------|------|
| NCP | 1.00 |
| CP | 0.87 |
| 4CP | 0.87 |

5.5.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.5.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.5.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 24 years for GSHPs. This value is consistent with the life expectancy of the heat pump components reported in multiple Department of Energy GSHP guides. Underground ground-loop infrastructure is expected to last 25-50 years.^{147,148}

5.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline type: ROB, NC
- Replaced unit heating type (heat pump, electric resistance furnace)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes

¹⁴⁵ Demand factors calculated in accordance with the current peak definition are lower than expected for the Texas climate. Residential HVAC measures will temporarily revert to the demand factors used in TX TRM 4.0 before the change to the peak definition. These values will be reevaluated in upcoming TRM cycles to better align with the current peak definition.

¹⁴⁶ Air Conditioning Contractors of America (ACCA) Manual S recommends that residential heat pumps be sized at 115% of the maximum cooling requirement of the residence (for cooling dominated climates). Assuming that maximum cooling occurs during the peak period, the guideline leads to a demand factor of $1/1.15 = 0.87$.

¹⁴⁷ Department of Energy. Geothermal Heat Pump Energy Saver article. <https://www.energy.gov/energysaver/geothermal-heat-pumps>.

¹⁴⁸ Department of Energy. "Guide to Geothermal Heat Pumps. February 2011. http://www.energy.gov/sites/prod/files/guide_to_geothermal_heat_pumps.pdf.

- Manufacturer, model, and serial number of the new unit
- ENERGY STAR certificate matching installed model number
- GSHP type (closed loop water-to-air, open loop water-to-air, closed loop water-to-water, open loop water-to-water, direct geoexchange)
- Energy Efficiency Ratio (EER) of the new unit
- Coefficient of Performance (COP) of the new unit
- Product specification sheet
- Rated cooling and heating capacity of the new unit (Btu/hr)¹⁴⁹
- Whether a desuperheater was installed or present
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

5.5.4 Document Revision History

Table 5.5-4: [GSHPs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Integrated federal standard change and SEER2 test procedure. |
| FY 2026 | No revision. |

¹⁴⁹ Rated capacities are not specified on the ENERGY STAR certificate and should be taken from the product specification sheet.

5.6 LARGE CAPACITY SPLIT AND PACKAGED AIR CONDITIONERS AND HEAT PUMPS

5.6.1 Measure Description

This measure applies to the installation of a split/package air conditioner (AC) or heat pump (HP) with a capacity exceeding that of a typical residential system (greater than or equal to 65,000 Btu/hr) in a retrofit or new construction application. This measure also applies to the installation of ground-source heat pumps (GSHP) with a capacity exceeding 65,000 Btu/hr.

5.6.1.1 Eligibility Criteria

- The deemed savings apply to central AC/HPs with a capacity of 65,000-240,000 Btu/hr (5.4-20 tons) and GSHPs with a capacity of 65,000-135,000 Btu/hr (5.4-11.3 tons).
- Equipment shall be properly sized to dwelling based on ASHRAE or ACCA Manual J standards.
- Manufacturer datasheets for new equipment or documentation of AHRI or DOE CCMS certification must be provided.^{150,151}

5.6.1.2 Baseline Condition

New construction and replace-on-burnout baseline efficiency levels are provided in Table 5.6-1 and Table 5.6-2. These baseline efficiency levels reflect the latest minimum efficiency requirements from the current federal manufacturing standard, IECC 2015, and ASHRAE 90.1-2013.

Table 5.6-1: [Large Capacity AC/HPs] NC/ROB Baseline Efficiencies for AC/HPs¹⁵²

| System Type | Capacity (tons) | Baseline Efficiencies |
|------------------|-----------------|-----------------------|
| Air conditioners | > 5.4 to < 11.3 | 11.0 EER 14.6 IEER |
| | ≥ 11.3 to < 20 | 10.8 EER 14.0 IEER |

¹⁵⁰ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

¹⁵¹ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

¹⁵² IECC 2018 Table C403.3.2(1) and C403.3.2(2).

| System Type | Capacity (tons) | Baseline Efficiencies |
|-------------------------------------|-----------------|-----------------------|
| Heat pumps (cooling) ¹⁵³ | > 5.4 to < 11.3 | 11.0 EER 14.1 IEER |
| | ≥ 11.3 to ≤ 20 | 10.6 EER 13.5 IEER |
| Heat pumps (heating) ¹⁵⁴ | > 5.4 to < 11.3 | 3.4 COP |
| | ≥ 11.3 to < 20 | 3.3 COP |

Table 5.6-2: [Large Capacity AC/HPs] NC/ROB Baseline Efficiencies for GSHPs¹⁵⁵

| System Type | Capacity (Btuh) | Cooling EWT Rating Condition | Minimum Cooling EER | Heating EWT Rating Condition | Minimum Heating COP |
|------------------------------|------------------------|------------------------------|---------------------|------------------------------|---------------------|
| Water-to-air (water loop) | ≥ 65,000 and < 135,000 | 86°F | 13.0 | 68°F | 4.3 |
| Water-to-air (groundwater) | | 59°F | 18.0 | 50°F | 3.7 |
| Brine-to-air (ground loop) | | 77°F | 14.1 | 32°F | 3.2 |
| Water-to-water (water loop) | | 86°F | 10.6 | 68°F | 3.7 |
| Water-to-water (groundwater) | | 59°F | 16.3 | 50°F | 3.1 |
| Brine-to-water (ground loop) | | 77°F | 12.1 | 32°F | 2.5 |

5.6.1.3 High-Efficiency Condition

Split and packaged systems must exceed the minimum efficiencies specified in Table 5.6-1 and Table 5.6-2.

For reference, both ENERGY STAR and the Consortium for Energy Efficiency (CEE) offer suggested guidelines for high-efficiency equipment.

¹⁵³ ASHRAE 90.1-2010 Table 6.8.1B. For systems larger than 5.4 tons, the minimum efficiency levels provided in this table are based on systems with heating type “No Heating or Electric Resistance Heating”, excluding systems with “All Other Types of Heating”.

¹⁵⁴ Heat pump retrofits must also exceed the baseline efficiency levels for heating efficiencies.

¹⁵⁵ IECC 2018 Table C403.3.2(2).

5.6.2 Energy and Demand Savings Methodology

5.6.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{\text{Savings,C}} + kWh_{\text{Savings,H}}$$

Equation 5.6-1

$$\text{Energy Savings (Cooling)} [kWh_{\text{Savings,C}}] = Cap_C \times \left(\frac{1}{\eta_{\text{baseline,C}}} - \frac{1}{\eta_{\text{installed,C}}} \right) \times EFLH_C \times \frac{1 \text{ kW}}{1,000 \text{ W}}$$

Equation 5.6-2

$$\text{Energy Savings (Heating)} [kWh_{\text{Savings,H}}] = Cap_H \times \left(\frac{1}{\eta_{\text{baseline,H}}} - \frac{1}{\eta_{\text{installed,H}}} \right) \times EFLH_H \times \frac{1 \text{ kWh}}{3,412 \text{ Btu}}$$

Equation 5.6-3

Where:

| | | |
|-----------------------------|---|--|
| $Cap_{C/H}$ | = | Rated equipment cooling/heating capacity of the installed equipment at AHRI standard conditions [Btu/hr]; 1 ton = 12,000 Btu/hr. |
| $\eta_{\text{baseline,C}}$ | = | Cooling efficiency of standard equipment (Btuh/W). |
| $\eta_{\text{installed,C}}$ | = | Rated cooling efficiency of the newly installed equipment (Btuh/W). |
| $\eta_{\text{baseline,H}}$ | = | Heating efficiency of standard equipment (Btuh/W or COP). |
| $\eta_{\text{installed,H}}$ | = | Rated heating efficiency of the newly installed equipment (Btuh/W or COP). |

Note: Use EER for cooling kW and COP for heating kW and kWh savings calculations. SEER/IEER should be used to calculate cooling kWh for central ACs and HPs. EER should be used to calculate cooling kWh for GSHPs. Heating efficiencies expressed as HSPF will be approximated as a seasonal COP and should be converted using the following equation:

$$COP = \frac{HSPF}{3.412}$$

Equation 5.6-4

| | | |
|----------|---|---|
| $EFLH_C$ | = | Equivalent full load hours for cooling. Use 2,237 hours for San Antonio. ¹⁵⁶ |
| $EFLH_H$ | = | Equivalent full load hours for heating. Use 1,101 hours for San Antonio. ¹⁵⁷ |
| 1,000 | = | Constant to convert from watts to kilowatts. |

¹⁵⁶ ENERGY STAR Central AC/HP Savings Calculator. April 2009 update.
https://www.energystar.gov/sites/default/files/asset/document/ASHP_Sav_Calc.xls.

¹⁵⁷ Ibid.

3,412 = Constant to convert from Btu to kWh.

Demand Savings

$$kW_{Savings} = CAP_C \times \left(\frac{1}{\eta_{baseline,C}} - \frac{1}{\eta_{installed,C}} \right) \times DF_C \times \frac{1 \text{ kW}}{1,000 \text{ W}}$$

Equation 5.6-5

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 5.6-3.

Table 5.6-3: [Large Capacity AC/HPs] Demand Factors^{158,159}

| Peak Type | DF |
|-----------|------|
| NCP | 1.00 |
| CP | 0.87 |
| 4CP | 0.87 |

1.1.1.4 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.6.2.2 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

5.6.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 18 years for large-capacity ACs and 15 years for large capacity HPs based on the current DOE Final Rule standards for central HPs.¹⁶⁰ The EUL 24 years for GSHPs, consistent with the EUL reported in the DOE GSHP guide.¹⁶¹

These values are consistent with the life expectancy of the heat pump components reported in multiple

¹⁵⁸ Demand factors calculated in accordance with the current peak definition are lower than expected for the Texas climate. Residential HVAC measures will temporarily revert to the demand factors used in TX TRM 4.0 before the change to the peak definition. These values will be reevaluated in upcoming TRM cycles to better align with the current peak definition.

¹⁵⁹ Air Conditioning Contractors of America (ACCA) Manual S recommends that residential heat pumps be sized at 115% of the maximum cooling requirement of the residence (for cooling dominated climates). Assuming that maximum cooling occurs during the peak period, the guideline leads to a demand factor of $1/1.15 = 0.87$.

¹⁶⁰ Final Rule: Standards, Federal Register, 76 FR 37408 (June 27, 2011) and associated Technical Support Document.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=75.

¹⁶¹ Department of Energy. "Guide to Geothermal Heat Pumps. February 2011.

http://www.energy.gov/sites/prod/files/guide_to_geothermal_heat_pumps.pdf.

DOE GSHP guides. Underground ground-loop infrastructure is expected to last 25-50 years.^{162,163}

5.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline type: ROB, NC
- Manufacturer, model, and serial number of new unit
 - AHRI/DOE CCMS certificate or reference number matching model number
- Cooling and heating capacities of the installed unit (Btu/hr)
- Full-load efficiency rating (EER) of the new unit
- Part-load efficiency rating (SEER/IEER) of the new unit (if applicable)
- Coefficient of performance (COP) of the new unit (heat pumps and GSHPs only)
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

5.6.4 Document Revision History

Table 5.6-4: [Large Capacity AC/HPs] Revision History

| Guidebook version | Description of change |
|-------------------|------------------------------------|
| FY 2025 | Updated GSHP EUL. |
| FY 2026 | Updated baseline efficiency table. |

¹⁶² Department of Energy. Geothermal Heat Pump Energy Saver article. <https://www.energy.gov/energysaver/geothermal-heat-pumps>.

¹⁶³ Department of Energy. "Guide to Geothermal Heat Pumps. February 2011. http://www.energy.gov/sites/prod/files/guide_to_geothermal_heat_pumps.pdf.

5.7 ENERGY STAR® CONNECTED THERMOSTATS

5.7.1 Measure Description

Deemed savings are provided for the replacement of a standard or programmable thermostat with an ENERGY STAR Connected Thermostat.

5.7.1.1 Eligibility Criteria

All residential customers with refrigerated air conditioning are eligible to claim cooling savings for this measure. Customers must have electric central heating (either an electric resistance furnace or a heat pump) to claim heating savings.

The Connected Thermostats measure is primarily a residential retrofit measure; savings are presented for the average efficiency ratings of installed HVAC systems. Deemed savings are also presented for new construction for efficiency ratings (minimum efficiency set by federal standards).

Customers should be advised against using the emergency heat (EM HEAT) setting on heat pump thermostats. This setting is meant only for use in emergency situations when the heat pump is damaged or malfunctioning. Supplemental heating automatically engages in below-freezing conditions using the regular HEAT setting. Contractors installing a new heat pump thermostat with equipment install shall advise customer of correct thermostat usage.

Customers that receive incentives for purchasing a thermostat device through an energy efficiency program, may be able to enroll in the load management program offered by the utility at the point of purchase. Deemed demand savings can only be claimed for those customers if they participate in the peak demand events. Otherwise, these devices are only eligible for the deemed energy efficiency savings.

5.7.1.2 Baseline Condition

The baseline condition is a residential central HVAC system controlled by a thermostat that does not meet the criteria for a connected thermostat (see High Efficiency Condition). For connected thermostats installed in conjunction with an existing HVAC unit, the baseline condition is an HVAC unit controlled by a manual or programmable thermostat with an average efficiency for existing HVAC units in Texas estimated as shown in Table 5.7-1.

Table 5.7-1: [Smart Tstats] Baseline Efficiency of Existing ACs

| Project Type | Capacity (Btu/hr) | Cooling mode |
|---|-------------------|--------------|
| Split air conditioners (manufactured as of 1/1/2023) | < 45,000 | 14.3 SEER2 |
| | ≥ 45,000 | 13.8 SEER2 |
| Packaged air conditioners (manufactured as of 1/1/2023) | All | 13.4 SEER2 |
| Split/package air conditioners (manufactured 1/1/2015 through 12/31/2023) | All | 12.8 SEER2 |
| Split/package air conditioners (when age is unknown) ¹⁶⁴ | All | 12.3 SEER2 |
| Split/package air conditioners (manufactured 1/23/2006 through 12/31/2014) | All | 11.9 SEER2 |
| Split/package air conditioners (manufactured before 1/23/2006) | All | 9.1 SEER2 |

Table 5.7-2: [Smart Tstats] Baseline Efficiency of Existing HPs

| Project Type | Cooling mode | Heating mode |
|---|--------------|--------------|
| Split heat pumps (manufactured as of 1/1/2023) | 14.3 SEER2 | 7.5 HSPF2 |
| Packaged heat pumps (manufactured as of 1/1/2023) | 13.4 SEER2 | 6.7 HSPF2 |
| Split heat pumps (manufactured 1/1/2015 through 12/31/2022) | 12.8 SEER2 | 6.9 HSPF2 |
| Packaged heat pumps (manufactured 1/1/2015 through 12/31/2022) | 12.8 SEER2 | 6.7 HSPF2 |
| Split Heat Pumps (when age is unknown) ¹⁶⁵ | 12.3 SEER2 | 6.7 HSPF2 |
| Packaged heat pumps (when age is unknown) ¹⁶⁶ | 12.3 SEER2 | 6.6 HSPF2 |
| Split/package heat pumps (manufactured 1/23/2006 through 12/31/2014) | 11.9 SEER2 | 6.5 HSPF2 |
| Split/package heat pumps (manufactured before 1/12/2006) | 9.1 SEER2 | 5.7 HSPF2 |
| Electric resistance furnace | — | 3.412 HSPF2 |

¹⁶⁴ Baseline efficiencies are calculated by taking the average the early retirement categories for 2006– 2014 and 2015–2022.

¹⁶⁵ Baseline efficiencies are calculated by taking the average the early retirement categories for 2006– 2014 and 2015–2022.

¹⁶⁶ Ibid.

For connected thermostats installed in conjunction with a new HVAC unit (for both retrofit and new construction applications), the baseline condition is an HVAC unit controlled by a manual or programmable thermostat with the baseline HVAC unit efficiency being equal to the efficiency of the installed system. The efficiency ratings of newly installed HVAC units should meet or exceed minimum values set by the federal manufacturing standards in effect at the time of the installation.

5.7.1.3 High-Efficiency Condition

The high-efficiency condition is an HVAC unit being controlled by a connected thermostat compliant with the ENERGY STAR Final Version 1.0 requirements for eligible connected thermostats effective December 3, 2016.¹⁶⁷ A list of eligible thermostats is available on the ENERGY STAR website.¹⁶⁸ Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

5.7.2 Energy and Demand Savings Methodology

Energy savings are estimated according to the program requirements established by the ENERGY STAR program for thermostat service providers seeking certification. In addition to a series of other technical and programmatic requirements, providers must demonstrate that their thermostat services result in significant run-time reductions for the controlled cooling and heating equipment. Specifically, ENERGY STAR provides the runtime reduction criteria reproduced in Table 5.7-3.

The ENERGY STAR runtime reductions are translated to energy savings estimates using the methodologies defined in the Central and Mini-Split Air Conditioners and Heat Pumps measure.

Demand (kW) savings are not estimated for the Connected Thermostats measure.

¹⁶⁷ ENERGY STAR Program Requirements Product Specification for Connected Thermostats, v1.0.

<https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Program%20Requirements%20for%20Connected%20Thermostats%20Version%201.0.pdf>.

¹⁶⁸ ENERGY STAR qualified product listing. <https://www.energystar.gov/productfinder/product/certified-connected-thermostats/results>.

Table 5.7-3: [Smart Tstats] ENERGY STAR Runtime Reduction Criteria

| Metric | Statistical Measure | Performance Requirement |
|--|--|-------------------------|
| Annual % Run Time Reduction, Cooling (CS) | Lower 95% Confidence Limit of Weighted National Average | $\geq 10\%$ |
| | Weighted National Average of 20th Percentiles | $\geq 5\%$ |
| Annual % Run Time Reduction, Heating (HS) | Lower 95% Confidence Limit of Weighted National Average | $\geq 8\%$ |
| | Weighted National Average of 20th Percentiles | $\geq 4\%$ |
| Average Resistance Heat Utilization for Heat Pump Installations (RU) | National Mean in 5°F Outdoor Temperature Bins from 0 to 60°F | Reporting Requirement |

5.7.2.1 Savings Algorithms and Input Variables

Energy and demand savings algorithms and associated input variables are listed below. Total Energy Savings $[\Delta kWh] = kWh_c + kWh_H$

Equation 5.7-1

$$\text{Energy Savings (Cooling)} [kWh_c] = \frac{Cap_c}{\eta_c} \times EFLH_c \times \frac{1 kW}{1,000 W} \times CRF$$

Equation 5.7-2

$$\text{Energy Savings (Heating)} [kWh_H] = \frac{Cap_H}{\eta_H} \times EFLH_H \times \frac{1 kW}{1,000 W} \times HRF \times DAF$$

Equation 5.7-3

Where:

| | | |
|-------------|---|---|
| $Cap_{C/H}$ | = | HVAC equipment cooling/heating capacity. For thermostats installed on existing equipment, use the nominal tonnage converted to nominal capacity. For thermostats installed with a new HVAC system use the AHRI rated capacity of the new equipment. For thermostats installed with a new or existing electric furnace, use the applicable nominal or rated cooling capacity as a proxy for heating capacity. [Btuh]; 1 ton = 12,000 Btuh. |
| η_c | = | HVAC equipment cooling efficiency. For thermostats installed on existing equipment, default to the code SEER2 rating from Table 5.7-1 for ACs and Table 5.7-2 for HPs. For thermostats installed with a new HVAC system, use the AHRI SEER2 rating of the new equipment. (Btuh/W). |
| η_H | = | HVAC equipment heating efficiency. For thermostats installed on existing equipment, default to the code HSPF2 rating from Table 5.7-2. For thermostats installed with a new HVAC system, use the AHRI HSPF2 rating |

of the new equipment. For thermostats installed with a new or existing electric resistance furnace, use 3.412 HSPF. (Btuh/W).

| | | |
|-------------------------|---|--|
| <i>EFLH_C</i> | = | Equivalent full load hours for cooling. Use 2,237 hours for San Antonio. ¹⁶⁹ |
| <i>EFLH_H</i> | = | Equivalent full load hours for heating. Use 1,101 hours for San Antonio. ¹⁷⁰ |
| <i>CRF</i> | = | Cooling hours reduction factor = 10% (Table 5.7-3). |
| <i>HRF</i> | = | Heating hours reduction factor = 8% (Table 5.7-3) |
| <i>DAF</i> | = | Documentation adjustment factor; set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases |

5.7.2.2 Deemed Energy Savings Tables

Deemed savings tables are only provided for connected thermostats installations where the cooling and heating equipment is unspecified. Savings are presented in kWh per thermostat, assuming a default of 3.7 tons.¹⁷¹

The following table describes various equipment replacement scenarios that may be encountered and specifies which baseline should be used in each case.

Table 5.7-4: [Smart Tstats] Baseline for Various Equipment Replacement Scenarios

| Equipment Replacement Scenario | Baseline | |
|--|----------|-------------------------|
| | Cooling | Heating |
| No HVAC equipment replacement | Existing | Existing |
| Coil replacements | Existing | Existing |
| Gas furnace replacements | Existing | No savings |
| | Existing | Existing |
| Air conditioner condenser replacement w/ gas furnace | New | No savings |
| Air conditioner condenser replacement w/ electric heat | New | Existing ¹⁷² |
| Heat pump condenser replacement | New | New |

For upstream and midstream programs where the existing HVAC system is unknown, assume a heating

¹⁶⁹ ENERGY STAR Central AC/HP Savings Calculator. April 2009 update.
https://www.energystar.gov/sites/default/files/asset/document/ASHP_Sav_Calc.xls.

¹⁷⁰ Ibid.

¹⁷¹ Based on review of average reported cooling capacity for central air conditioners and heat pumps installed in Texas utility programs in previous program years.

¹⁷² In this scenario, utilize the existing cooling capacity as the existing heating capacity as a proxy due the fact that the existing heating capacity is not provided.

type weighting of 41.7% gas, 30.0% electric resistance, and 28.3% heat pump heat.¹⁷³

Table 5.7-5: [Smart Tstats] Energy Savings for Thermostats Installed on Unspecified Existing HVAC (kWh/thermostat)¹⁷⁴

| Total Energy Savings |
|-------------------------|
| 1,317 |

5.7.2.3 Deemed Demand Savings Tables

Demand savings shall not be claimed for the connected thermostats measure.

5.7.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 11 years for connected thermostats, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID HV-ProgTstat.¹⁷⁵

5.7.3 Program Tracking Data and Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

All program types:

- Thermostat quantity purchased/installed
- Thermostat manufacturer and model number
- ENERGY STAR certificate matching model number

Additional requirements for all program types other than upstream/midstream:

- HVAC system type (split AC, packaged AC, split HP, packaged HP)
- Determine whether HVAC condenser was replaced in conjunction with thermostat
- If installed with existing HVAC equipment:
 - HVAC capacity (Btuh): Nominal tons converted to capacity
 - Manufacture year
- If installed with a new HVAC system:

¹⁷³ Residential Energy Consumption Survey (RECS) 2020: Space heating in homes in the South and West Regions (HC6.8), <https://www.eia.gov/consumption/residential/data/2020/>.

¹⁷⁴ Assuming smart thermostat is installed in conjunction with an existing 3.7-ton HVAC unit.

¹⁷⁵ DEER READI (Remote Ex-Ante Database Interface). <http://www.deerresources.com/index.php/readi>.

- HVAC capacity (Btuh): AHRI rated capacity
- Part-load cooling efficiency (SEER2)
- Heating efficiency (HSPF2) – HPs only
- Heating type (gas, electric resistance, heat pump, none)
- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification
- Retired or replaced heating unit model number, serial number, manufacturer, and heating capacity (electric resistance only)
 - Photograph of retired heating unit nameplate, utility inspection, recording nameplate information, or other evaluator-approved approach. Sampling is allowed for multifamily complexes.
 - If documentation is not provided, an adjustment factor of 0.75 will be applied to the heating energy

5.7.4 Document Revision History

Table 5.7-6: [Smart Tstats] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Incorporated algorithm approach. Incorporated new SEER2 test procedure. |
| FY 2026 | Updated heating type weighting and unspecified equipment deemed savings. Added electric resistance baseline and documentation requirement. |

5.8 DUCT SEALING

5.8.1 Measure Description

This measure involves sealing leaks in supply and return ducts of the HVAC distribution systems of homes or converted residences with central air conditioning. The standard approach for estimating savings in this measure is based on the results obtained via pre- and post-measure implementation leakage testing as defined in this measure (the “standard approach”). In lieu of leakage testing, savings for eligible duct sealing projects may be claimed using the deemed savings tables for implementations in which testing is not performed (subheadings “absent leakage testing”).

5.8.1.1 Eligibility Criteria

All residential customers with ducted central refrigerated air cooling are eligible for this measure. Customers must have ducted central heating with either a furnace (gas or electric resistance) or a heat pump to claim heating savings. The specified deemed savings are not applicable to residences with space (non-central or ducted) air conditioning or heating. New construction is not eligible.

For the standard approach with leakage testing, duct leakage should be assessed following Building Performance Institute (BPI) standards. Duct leakage testing should not be conducted in homes where evidence of asbestos or mold is present or suspected.¹⁷⁶ Installers should be mindful of health and safety considerations related to implementation of duct efficiency measures and/or testing procedures.

5.8.1.2 Baseline Condition

The savings calculation methods for this measure (when implemented with duct leakage testing) are valid up to a maximum pre-installation leakage rate of 35 percent of total fan flow.¹⁷⁷ For homes with an initial leakage rate greater than 35 percent of total fan flow, savings will be awarded with respect to this cap rather than the initial leakage. Data from nearly 28,000 single-family and mobile home duct blaster tests conducted for duct efficiency improvements in Texas between 2003 and 2006 show that more than 70 percent of all pre-retrofit leakage rates fall below 38 percent total leakage.¹⁷⁸

Engineering calculations show that the interior temperature in those settings that exceed 38 percent total leakage would be above the thermally acceptable comfort levels published by ASHRAE in its 2009 Fundamentals publication. The proposed pre-installation leakage limits will help ensure that the deemed savings are an accurate reflection of the program’s impacts, and that the program focuses its efforts on scenarios where leakage conditions are likely to persist if unaddressed for several years.

¹⁷⁶ “Technical Standards for the Building Analyst Professional,” Building Performance Institute (BPI), v1/4/12mda, Page 1 of 17, states: “Health and Safety: Where the presence of asbestos, lead, mold and/or other potentially hazardous material is known or suspected, all relevant state and federal (EPA) guidelines must be followed to ensure technician and occupant safety. Blower door depressurization tests may not be performed in homes where there is a risk of asbestos becoming airborne and being drawn into the dwelling.”

<http://www.bpi.org/sites/default/files/Technical%20Standards%20for%20the%20Building%20Analyst%20Professional.pdf>.

¹⁷⁷ $Total\ Fan\ Flow = Cooling\ Capacity\ (tons) \times 400\ cfm/ton$.

¹⁷⁸ Based on data collected by Frontier Energy for investor-owned utilities in Texas.

CPS Energy may waive the cap limiting the maximum pre-installation leakage rate to 35 percent of total fan flow for low-income qualified customers.

While these baseline criteria were applied in deriving the deemed savings for the alternate approach (absent leakage testing), it is not necessary to determine pre-installation leakage rate for projects in which implementers choose to apply those (absent leakage testing) savings.

5.8.1.3 High-Efficiency Condition

Materials used should be long-lasting materials, such as mastics, UL 181A or UL 181B approved foil tape, or aerosol-based sealants. Fabric-based duct tape is not allowed.

The selected methodology for estimating duct sealing deemed savings, according to the standard approach, requires duct leakage-to-outside testing using a combination duct pressurization and house pressurization.

5.8.1.4 Duct Leakage Testing (Standard Approach)

Measurements to determine pre-installation and post-installation leakage rates must be performed in accordance with CPS-approved procedures. For this measure, leakage-to-outside must be directly measured. The Project Sponsor shall use the Combination Duct Blaster™ (or equivalent) and Blower Door method. Prior to beginning any installations, the Project Sponsor must submit the intended method(s) and may be required to provide the utility with evidence of competency, such as Home Energy Rating System (HERS) or North American Technician Excellence (NATE) certification. Leakage rates must be measured and reported at the average air distribution system operating pressure (25 Pa).¹⁷⁹

5.8.1.5 Categorizing Achieved Duct Leakage Reduction (absent leakage testing)

Participating project sponsors electing not to perform leakage testing should nevertheless provide an estimate of the expected outcome of the leakage reduction work performed: projects should be characterized according to the project sponsor's estimation of whether the work required should result in **low**, **average**, or **high** reduction in duct system leakage. Sponsors should take the following considerations into account in assessing the likely leakage reduction achieved in each project:

- The number and size of repaired leaks.
- Leak location: a leak in an attic joint will cause more energy loss than a joint that leaks to conditioned space.
- Supply/Return: Supply-side leaks, particularly in the return air plenum and near the air

¹⁷⁹ See RESNET Technical Committee, Proposed Amendment: Chapter 8 RESNET Standards, 800 RESNET Standard for Performance Testing and Work Scope: Enclosure and Air Distribution Leakage Testing; Section 803.2 and Table 803.1. <https://www.resnet.us/wp-content/uploads/Chapter-Eight-22RESNET-Standard-for-Performance-Testing-and-Work-Scope-Enclosure-and-Air-Distribution-Leakage-Testing22.pdf>.

handling unit can be especially problematic, as they tend to draw additional unconditioned air into the system.

Systems that were not initially very leaky and in which few joints and supply vents were sealed should be characterized as low reduction. Jobs with a typical number of supply vents and joints sealed, and in which the supply air return or the return air plenum were sealed, should be characterized as average reduction. Jobs requiring significant interventions to eliminate large or numerous leaks should be considered high reduction.

The following table provides a guideline for selecting an appropriate leakage category. How the category is determined may fluctuate on a per home basis.

Table 5.8-1: [Duct Sealing] Leakage Categorization Guide¹⁸⁰

| Category | Duct Location | Duct Insulation | Leakage Characteristics ¹⁸¹ |
|----------|--------------------|-----------------|--|
| Low | > 90% Conditioned | > R7 | Some observable leaks |
| | | | Substantial leaks |
| | | R4 - R7 | Some observable leaks |
| | | | Substantial leaks |
| | | < R4 | Some observable leaks |
| | | | Substantial leaks |
| | 50-90% Conditioned | > R7 | Some observable leaks |
| | | R4 - R7 | Some observable leaks |
| | | < R4 | Some observable leaks |
| Average | > 90% Conditioned | > R7 | Catastrophic leaks |
| | | R4 - R7 | Catastrophic leaks |
| | | < R4 | Catastrophic leaks |
| | 50-90% Conditioned | > R7 | Substantial leaks |
| | | | Catastrophic leaks |
| | | R4 - R7 | Substantial leaks |
| | | < R4 | Substantial leaks |
| | < 50% Conditioned | > R7 | Some observable leaks |
| | | R4 - R7 | Some observable leaks |
| | | < R4 | Some observable leaks |

¹⁸⁰ Based on typical distribution efficiency assumptions from the Building Performance Institute (BPI) Technical Standards for the Heating Professional, November 20, 2007, page 7.

<http://www.bpi.org/sites/default/files/Technical%20Standards%20for%20the%20Heating%20Professional.pdf>

¹⁸¹ Catastrophic leaks are defined by BPI as disconnected ducts, missing endcaps, and other catastrophic holes.

| Category | Duct Location | Duct Insulation | Leakage Characteristics ¹⁸¹ |
|----------|--------------------|-----------------|--|
| High | 50-90% Conditioned | R4 - R7 | Catastrophic leaks |
| | | < R4 | Catastrophic leaks |
| | < 50% Conditioned | > R7 | Substantial leaks |
| | | | Catastrophic leaks |
| | | R4 - R7 | Substantial leaks |
| | | | Catastrophic leaks |
| | | < R4 | Substantial leaks |
| | | | Catastrophic leaks |

5.8.2 Energy and Demand Savings Methodology

Savings may be claimed according to either the standard approach (with duct leakage testing) or the alternate approach, according to the following sections.

5.8.2.1 Savings Algorithms and Input Variables

Calibrated simulation modeling was used to develop these deemed savings, which are expressed as linear functions of the reduction in duct leakage achieved (in CFM₂₅). Specifically, these deemed savings estimates were developed using BEopt 2.6, running EnergyPlus 8.4 as the underlying simulation engine. To model this measure, the prototype home models for San Antonio were modified as follows: the base case duct leakage rate was set to 8 CFM₂₅ per 100 square feet. Results from running the base case model provide estimated hourly energy use for the prototypical home prior to treatment. Post-treatment conditions were simulated by setting the leakage rate to 6 CFM₂₅ per 100 square feet. Results from running the change case model provide estimated hourly energy use for the prototypical home after treatment. Comparison of these two runs provides the deemed savings estimates.

Deemed savings are presented as a function of the CFM₂₅ reduction achieved, as demonstrated by leakage to outside testing using the Combination Duct Blaster™ (or equivalent) and Blower Door method. The kWh and kW per CFM₂₅ values represented by the V_E and V_D coefficients are derived by taking the difference between annual energy use and peak demand as estimated by the two model runs and normalizing to the CFM₂₅ reduction achieved.

5.8.2.2 Standard Approach (with leakage testing)

The annual energy and peak demand savings to be claimed for this measure, according to the standard approach, shall be calculated as a function of the reduction in duct leakage achieved, using the energy and demand savings coefficients from Table 5.8-2 through Table 5.8-3 for the type of heating equipment in the project home.

Energy Savings

In the standard approach, energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models.

The following formula shall be used to calculate annual energy savings for duct leakage reduction:

$$\text{Energy Savings } [\Delta kWh] = (DL_{pre} - DL_{post}) \times (V_{E,C} + V_{E,H} \times DAF)$$

Equation 5.8-1

Where:

| | | |
|-------------|---|---|
| DL_{pre} | = | Pre-improvement duct leakage at 25 Pa (cu. ft./min). |
| DL_{post} | = | Post-improvement duct leakage at 25 Pa (cu. ft./min). |
| $V_{E,C}$ | = | Cooling Energy Savings Coefficient in Table 5.8-2. |
| $V_{E,H}$ | = | Heating Energy Savings Coefficient in Table 5.8-2. |
| DAF | = | Documentation adjustment factor; set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases. |

Estimated savings per unit of leakage rate reduction (measured in CFM₂₅) are presented in the deemed energy savings tables below.

Demand Savings

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4CP) demand savings are estimated in accordance with the definitions provided in Section 2.3 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per unit of leakage rate reduction (measured in CFM₂₅) are presented in the deemed demand savings tables below.

The following formula shall be used to calculate deemed demand savings for duct leakage reduction:

$$\text{Demand Savings } [\Delta kW] = (DL_{pre} - DL_{post}) \times V_D$$

Equation 5.8-2

Where:

| | | |
|-------|---|--|
| V_D | = | Demand Savings Coefficient in Table 5.8-3. |
|-------|---|--|

Estimated savings per unit of leakage rate reduction (measured in CFM₂₅) are presented in the deemed demand savings tables below.

5.8.2.3 Deemed Energy Savings Tables (with leakage testing)

The following table presents the annual energy savings per CFM₂₅ reduction for a residential duct sealing project.

Table 5.8-2: [Duct Sealing] V_E, Standard Approach Energy Savings per CFM₂₅ Reduction

| V _{E,C} : Cooling Savings | V _{E,H} : Heating Savings | | |
|------------------------------------|------------------------------------|---------------------|-----------|
| | Gas | Electric Resistance | Heat Pump |
| 1.43 | 0.02 | 0.79 | 0.19 |

5.8.2.4 Deemed Demand Savings Tables (with leakage testing)

Table 5.8-3: [Duct Sealing] Standard Approach Peak Demand Savings V_D per CFM₂₅ Reduction

| V _D | Primary Heat Source | Demand Savings (kW/CFM ₂₅) |
|----------------|---------------------|--|
| NCP | Gas Furnace | 1.29 x 10 ⁻³ |
| | Electric Resistance | 1.75 x 10 ⁻³ |
| | Heat Pump | 2.60 x 10 ⁻³ |
| CP | All | 9.43 x 10 ⁻⁴ |
| 4CP | All | 1.07 x 10 ⁻³ |

5.8.2.5 Alternate Approach (absent leakage testing)

Savings tables are provided for projects implemented without performance of duct leakage testing, accounting for the application of pre-retrofit leakage caps to non-hard-to-reach (HTR) projects. The annual energy and peak demand savings to be claimed according to this alternate approach for this measure shall be taken from Table 5.8-4 and Table 5.8-5 according to the type of heating equipment in the project home.

While savings for multiple duct systems are additive for the standard approach, the following savings are specified per home when using the alternate approach and should not be multiplied by the number of treated duct systems.

NOTE: This approach is only available to programs with an incentive structure that does not vary by leakage category. Additionally, energy efficiency service providers (EESPs) should not alternate between the standard and alternate approaches during the same program year. The utility should either restrict all participants within an individual program to one approach or the other or they should restrict individual EESPs to one approach or the other across all program types.

5.8.2.6 Deemed Energy Savings Tables (absent leakage testing)

Table 5.8-4 presents the annual energy savings for a residential duct sealing project.

Table 5.8-4: [Duct Sealing] Alternate Approach Energy Savings

| Assessed Leakiness | Cooling Savings | Heating Savings | | |
|--------------------|-----------------|-----------------|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| Low | 327 | 4 | 180 | 44 |
| Average | 524 | 6 | 288 | 71 |
| High | 749 | 8 | 412 | 101 |

5.8.2.7 Deemed Demand Savings Tables (absent leakage testing)

Table 5.8-5 presents the peak demand savings for a residential duct sealing project.

Table 5.8-5: [Duct Sealing] Alternate Approach Peak Demand Savings

| V _D | Primary Heat Source | Low | Average | High |
|----------------|---------------------|------|---------|------|
| NCP | Gas Furnace | 0.30 | 0.47 | 0.68 |
| | Electric Resistance | 0.40 | 0.64 | 0.91 |
| | Heat Pump | 0.59 | 0.95 | 1.36 |
| CP | All | 0.22 | 0.34 | 0.49 |
| 4CP | All | 0.24 | 0.39 | 0.56 |

5.8.2.8 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 18 years for duct sealing, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID HV-DuctSeal-BW.¹⁸²

5.8.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

All projects:

- Cooling type (central refrigerated cooling, none)

¹⁸² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

- Heating type (central gas furnace, central electric resistance furnace, heat pump, none)
 - Additional documentation is required to validate resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach)
- Cooling capacity of home HVAC unit(s) (tons)

Sponsors claiming savings according to duct leakage testing:

- Pre-improvement duct leakage at 25 Pa (cu. ft./min)
- Post-improvement duct leakage at 25 Pa (cu. ft./min)
- Pre and post photos of leakage test readings

Sponsors claiming savings without performing leakage testing should provide:

- Description of the leakage severity in the home (low, average, or high)
- Description and condition of ducts:
 - Duct location (> 90% conditioned, 50-90% conditioned, < 50% conditioned)
 - Existing duct insulation value (> R7, R4-R7, < R4)
- Leakage characteristics (some observable leaks, substantial leaks, catastrophic leaks)
- Other relevant details that may assist with validating claimed leakage category
- Description and photos of interventions taken (both pre and post condition), such as newly sealed joints, supply vents, and other relevant leaks sealed
- Incentive rate structure: incentive should be paid per home and should not vary by leakage category to protect against overstating existing leakage category

5.8.4 Document Revision History

Table 5.8-6: [Duct Sealing] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | No revision. |
| FY 2026 | Incorporated electric resistance documentation adjustment factor. |

6. RESIDENTIAL: BUILDING ENVELOPE

6.1 AIR INFILTRATION

6.1.1 Measure Description

This measure involves the implementation of interventions to reduce the rate of air infiltration into residences. Pre- and post-treatment blower door air pressure readings are required to confirm air leakage reduction. The standard approach for estimating savings in this measure is based on the results obtained via pre- and post-leakage testing as defined in this measure.

6.1.1.1 Eligibility Criteria

Cooling savings in this measure only apply to residential customers with central or mini-split electric refrigerated air HVAC systems in their residences. Residences must be centrally heated with either a furnace (gas or electric resistance) or a heat pump to claim heating savings. Customers are eligible to claim reduced heating savings for homes heated with gas or electric resistance space heaters by applying an adjustment to deemed savings specified by heating type. Customers are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that are specified for homes with refrigerated air.

While all homes are eligible for treatment, the savings that can be claimed for any individual home are limited by a maximum pre-retrofit infiltration rate of 5.2 CFM₅₀ per square foot of house floor area.

Air leakage should be assessed through testing that follows Building Performance Institute (BPI) standards. In some limited cases, where testing is not possible or unsafe (e.g., because of potential presence of asbestos), visual assessment may be satisfactory. The air leakage testing should not be conducted in homes where evidence of asbestos or mold is present or suspected because of the age of the home.¹⁸³ CPS Energy may require certification or competency testing of personnel who will perform the blower door tests.

Utilities may require certification or competency testing of personnel who will perform the blower door tests. Air leakage should be assessed through testing following Building Performance Institute (BPI) standards. In some limited cases, where testing is not possible or unsafe (e.g., due to the potential presence of asbestos), a visual assessment may be satisfactory. The air leakage testing should not be conducted in homes where either evidence of asbestos or mold is present or suspected due to the age of the home.¹⁸⁴ Utilities' program manuals should be consulted for health and safety considerations

¹⁸³ "Technical Standards for the Building Analyst Professional," Building Performance Institute (BPI), v1/4/125mda, Page 1 of 17, states: "Health and Safety: Where the presence of asbestos, lead, mold and/or other potentially hazardous material is known or suspected, all relevant state and federal (EPA) guidelines must be followed to ensure technician and occupant safety. Blower door depressurization tests may not be performed in homes where there is a risk of asbestos becoming airborne and being drawn into the dwelling."
<http://www.bpi.org/sites/default/files/Technical%20Standards%20for%20the%20Building%20Analyst%20Professional.pdf>.

¹⁸⁴ The Building Performance Institute, Inc. (BPI) Standard Reference: Building Performance Institute Technical Standards for the Building Analyst Professional, v2/28/05mda, Page 1 of 17, states: "Health and Safety: Where the presence of asbestos, lead, mold and/or other

related to the implementation of air sealing measures.

Only structures with electric refrigerated air conditioning systems are eligible.

6.1.1.2 Baseline Condition

The baseline for this measure is defined by the leakage rate of the participating residence prior to treatment, capped at 5.2 CFM₅₀/ft² to account for the fact that the linear relationship described by the deemed savings values per CFM₅₀ leakage reduction are only applicable up to the point where the existing HVAC equipment would run continuously. Beyond that point, energy use will no longer increase linearly with an increase in leakage.^{185,186}

The baseline for this measure is the existing leakage rate of the treated residence. The existing leakage rate should be capped to account for the fact that the deemed savings values per CFM₅₀ leakage reduction are only applicable up to a point where the existing HVAC equipment would run continuously. Beyond that point, energy use will no longer increase linearly with an increase in leakage.

Baseline assumptions used in the development of these deemed savings are based on a conversion from ACH_{Natural}. ASHRAE Handbook: Fundamentals specifies that more than 80% of sampled low-income housing had a pre-leakage rate at or below 1.75 ACH_{Natural}.¹⁸⁷ ACH_{Natural} was converted to CFM₅₀/sqft using the following equation.

$$NL = 1,000 \times \frac{ELA_4}{A \times 0.3048^2} \times \left(\frac{H \times 0.3048}{2.5 \text{ m}} \right)^{0.3}$$

Equation 6.1-1

$$Q_{50} = \frac{ELA_4}{\left(\sqrt{\frac{\rho}{2(4 \text{ Pa})}} \times \left(\frac{4 \text{ Pa}}{50 \text{ Pa}} \right)^{0.65} \right)}$$

Equation 6.1-2

$$CFM_{50,pre}/ft^2 = \frac{Q_{50} \times 60 \times 35.3147}{A}$$

Equation 6.1-3

Where:

$$NL = \text{Normalized Leakage} = 2.0 \text{ from LBNL study.}$$

potentially hazardous material is known or suspected, all relevant state and federal (EPA) guidelines must be followed to ensure technician and occupant safety. Blower door depressurization tests may not be performed in homes where there is a risk of asbestos becoming airborne and being drawn into the dwelling.”

¹⁸⁵ Baseline assumptions used in the development of these deemed savings are based on a 2013 Lawrence Berkeley National Laboratory (LBNL) analysis of air leakage measurements of US houses. The LBNL study showed that approximately 95 percent of the home infiltration rates were below a normalized leakage rate of 2.0. Conversion of a normalized leakage rate of 2.0 to CFM₅₀/ft² through a series of equations results in the provided 5.2 CFM₅₀/ft² cap. TX TRM 8.0 updated this value to 4.6 based on 2017 ASHRAE Handbook: Fundamentals, Chapter 16, p. 16.19, Fig. 12. However, the reduction to the pre-leakage cap was not applied here based on a review of CPS Energy consumption data.

¹⁸⁶ Chan, W.R., Joh, J., and Sherman, M. H. Analysis of air leakage measurements of US houses. Environmental Energy Technologies Division, Lawrence Berkeley National Laboratory (LBNL), p. 616-625.

¹⁸⁷ 2017 ASHRAE Handbook: Fundamentals, Chapter 16, p. 16.19, Fig. 12.

| | | |
|---------------------|---|--|
| ELA_4 | = | Area of an orifice that would result in the same airflow through the building envelope at a pressure difference of 4 Pa [m^2]. |
| A | = | Average area of a home in Texas from RECS 2009 [ft^2] = 1,757 ft^2 . |
| H | = | Ceiling height [ft] = 8.5 (default). ¹⁸⁸ |
| 0.3048 | = | Constant to convert from feet to meters. |
| Q_{50} | = | Leakage rate at 50 Pa [m^3/s]. |
| ρ | = | 1.2 kg/m^3 from LBNL study. |
| $CFM_{50,pre}/ft^2$ | = | Maximum per-square-foot pre-installation infiltration rate. |
| 60 | = | Constant to convert from minutes to seconds. |
| 35.3147 | = | Constant to convert from cubic meters to cubic feet. |

Using the above approach, the maximum per-square-foot pre-installation infiltration rate is 5.2. Therefore, to avoid incentivizing homes with envelope problems not easily remedied through typical weatherization procedures, or where blower door tests were improperly conducted, these savings should only be applied starting at a baseline CFM_{50}/ft^2 of 5.2 or lower.

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.¹⁸⁹ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.¹⁹⁰ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Demand Savings Tables sections.

6.1.1.3 High-Efficiency Condition

Blower door air pressure measurements must also be used to ensure that post-treatment air infiltration rates are not less than those set forth by the standard in Equation 6.1-4, based on floor area and number of bedrooms.¹⁹¹ These calculated minimum CFM_{50} values assume two occupants for a one-bedroom dwelling unit and an additional person for each additional bedroom. At the utility's discretion, this minimum CFM_{50} requirement may be enforced as an eligibility requirement. Otherwise, savings may be claimed for projects where the measured final infiltration rate is less than the minimum allowable ventilation rate if the following conditions are met:

- Mechanical ventilation is present or introduced in compliance with ASHRAE 62.2-2013.

¹⁸⁸ Typical ceiling height of 8 feet adjusted to account for greater ceiling heights in some areas of a typical residence.

¹⁸⁹ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

¹⁹⁰ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

¹⁹¹ ASHRAE 62.2-2013. CFM_{Nat} values converted to CFM_{50} values by multiplying by appropriate N factor.

- Post-treatment infiltration rate is reported as the actual measured CFM50 result.
- Savings are calculated using the minimum allowable ventilation rate with no additional savings claimed for CFM reduction below this amount.

Where higher occupant densities are known, the minimum rate shall be increased by 7.5 CFM_{Nat} for each additional person. A CFM_{Nat} value can be converted to CFM₅₀ by multiplying by the appropriate N factor provided in Table 6.1-1.

$$\text{Min CFM}_{50} = [0.03 \times A_{\text{Floor}} + 7.5 \times \text{OCC}] \times N$$

Equation 6.1-4

Where:

| | | |
|-----------------------------|---|---|
| <i>Min CFM₅₀</i> | = | <i>Minimum final ventilation rate [CFM₅₀].</i> |
| <i>A_{Floor}</i> | = | <i>Floor area [ft²].</i> |
| <i>OCC</i> | = | <i>the number of home occupants, or 1+ the number of bedrooms (1 + BR), whichever is greater.</i> |
| <i>N</i> | = | <i>N factor; see Table 6.1-1.</i> |

Table 6.1-1: [Air Infiltration] N Factors¹⁹²

| Shielding | Number of Stories | | |
|---------------|-------------------|-----------|-------------------|
| | Single Story | Two Story | 3 or More Stories |
| Well shielded | 22.2 | 17.8 | 15.5 |
| Normal | 18.5 | 14.8 | 13.0 |
| Exposed | 16.7 | 13.3 | 11.7 |

The maximum CFM reduction percentage¹⁹³ is capped at 30 percent. It is important to note that the minimum ventilation rate specified earlier in this measure still applies for cases where the maximum 30 percent CFM reduction cannot be achieved due to the post CFM value being limited by the minimum allowable post CFM value provisioned for safety reasons.

An upper limit of 5.2 CFM₅₀ per square foot of conditioned floor area is applied to the pre-retrofit infiltration rate. For homes where the pre-retrofit leakage exceeds this limit, energy and demand savings must be calculated using the pre-measure installation leakage cap. Therefore, when the pre-retrofit leakage is capped, energy and demand savings can only be claimed for a 30 percent reduction in CFM compared to the capped pre-CFM value. When the pre-retrofit leakage is not capped, energy and demand savings can only be claimed for a 30 percent reduction compared to the tested, actual pre-

¹⁹² Krigger, J. and Dorsi, C., "Residential Energy: Cost Savings and Comfort for Existing Buildings." A-11 Building Tightness Limits, p. 284. Use Zone 2 for Texas climate.

¹⁹³ CFM reduction percentage is calculated as: (pre-CFM value – post-CFM value) / pre-CFM value.

retrofit infiltration rate of the home.

Contractors shall provide documentary evidence—such as pictures capturing the scope/type of retrofit implemented and blower door test readings—for all projects claiming savings for all homes.

6.1.2 Energy and Demand Savings Methodology

Calibrated simulation modeling was used to develop these deemed savings, which are expressed as linear functions of the leakage reduction achieved (in CFM₅₀).¹⁹⁴ Specifically, these deemed savings estimates were developed using BEopt 2.6 software, running EnergyPlus 8.4 as the underlying simulation engine. To model this measure, the prototype home model was modified as follows: the base case air infiltration rate was set to 20 ACH₅₀. Results from running the base case model provide estimated hourly energy used for the prototypical home prior to treatment. Post-treatment conditions were simulated by setting the leakage rate to 3 ACH₅₀.

6.1.2.1 Savings Algorithms and Input Variables

Deemed savings are presented as a function of the CFM₅₀ reduction achieved, as demonstrated by blower door testing. The kWh and kW per CFM₅₀ values represented by the V_E , V_S , and V_W coefficients are derived by taking the difference between annual energy use and peak demand as estimated by the two model runs and normalizing to the CFM₅₀ reduction achieved. The pre- and post-treatment ACH₅₀ values (20 and 3, respectively) are converted to CFM₅₀ by multiplying the pressurized air-change rate by the volume of the model home and dividing by 60 (minutes/hour).

Energy Savings

Energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per unit of leakage rate reduction (measured in CFM₅₀) are presented in the deemed energy savings tables below.

Demand Savings

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4CP) demand savings are estimated in accordance with the definitions provided in Section 2.3 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per unit of leakage rate reduction (measured in CFM₅₀) are presented in the deemed demand savings tables below.

¹⁹⁴ Model testing indicates a straight-line relationship between demand and energy savings achieved and CFM₅₀ reductions is appropriate with beginning and ending leakage rates within the ranges permitted by the measure.

6.1.2.2 Deemed Energy Savings Tables

Table 6.1-2 presents the energy savings per CFM₅₀ reduction for a residential air sealing project. The following formula shall be used to calculate deemed energy savings for infiltration efficiency improvements.

$$\text{Energy Savings } [\Delta kWh] = \Delta CFM_{50} \times (V_{E,C} \times CAF + V_{E,H} \times HAF \times DAF)$$

Equation 6.1-5

Where:

ΔCFM_{50} = Air infiltration reduction in cubic feet per minute at 50 Pascal.

$V_{E,C}$ = Corresponding cooling savings value in

Table 6.1-2.

CAF = Cooling adjustment factor for homes with room air conditioners; set to 1.0 for homes with refrigerated air or set to 0.6 for homes with one or more room air conditioners.

$V_{E,H}$ = Corresponding heating savings value in Table 6.1-2.

HAF = Heating adjustment factor for homes with electric resistance space heaters; set to 1.0 for homes with central heating with supplemental space heating or set to 0.24 for homes with primary electric resistance space heating.

DAF = Documentation adjustment factor; set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases.

For customers who participate in hard-to-reach (HTR) or low-income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying appropriate cooling values in

Table 6.1-2 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by multiplying appropriate heating values in

Table 6.1-2 by a factor of 0.24.¹⁹⁵

¹⁹⁵ This factor was derived based on expected capacity reduction assuming 1200 sq. ft. (historical analysis of HTR participants) x 0.35 BTU/sq. ft. = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields 10,200 ÷ 42,000 = 0.24.

Table 6.1-2: [Air Infiltration] VE, Energy Savings per CFM50 Reduction

| V _{E,C} : Cooling Savings | V _{E,H} : Heating Savings | | |
|------------------------------------|------------------------------------|---------------------|-----------|
| | Gas | Electric Resistance | Heat Pump |
| 0.27 | 0.02 | 0.67 | 0.28 |

Table 6.1-3: [Air Infiltration] CAF/HAF, Cooling & Heating Adjustment Factors

| HVAC System Type | CAF | HAF |
|----------------------------------|------|------|
| Central AC | 1.00 | - |
| Window or room AC | 0.60 | - |
| Central furnace or HP | - | 1.00 |
| Electric resistance space heater | - | 0.24 |
| None | - | - |

6.1.2.3 Deemed Demand Savings Tables

Table 6.1-4 presents the peak demand savings per CFM₅₀ reduction for a residential air sealing project. The following formula shall be used to calculate deemed demand savings for air infiltration improvements. For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying V_D in Table 6.1-4 by a factor of 0.6.

$$\text{Demand Savings } [\Delta kW] = \Delta CFM_{50} \times V_D \times AF$$

Equation 6.1-6

Where:

V_D = Corresponding demand savings value in Table 6.1-4.

AF = Adjustment factor based on HVAC system type in Table 6.1-5.

Table 6.1-4: [Air Infiltration] Peak Demand Savings V_D per CFM₅₀ Reduction

| V _D | Primary Heat Source | Demand Savings (kW/CFM ₅₀) |
|----------------|---------------------|--|
| NCP | Gas Furnace | 4.91 x 10 ⁻⁴ |
| | Electric Resistance | 1.68 x 10 ⁻³ |
| | Heat Pump | 6.46 x 10 ⁻⁴ |
| CP | All | 2.18 x 10 ⁻⁴ |
| 4CP | All | 1.96 x 10 ⁻⁴ |

Table 6.1-5: [Air Infiltration] AF, Adjustment Factors

| Cooling System Type | NCP Adjustment Factor by Primary Heat Source | | | | CP and 4CP Adjustment Factor by Primary Heat Source | | | |
|---------------------|--|-----|-----|------|---|-----|-----|------|
| | Gas | ER | HP | None | Gas | ER | HP | None |
| Central AC | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Window or Room AC | 0.6 | 1.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| None | - | 1.0 | - | - | - | - | - | - |

6.1.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) for is 11 years for air infiltration reduction, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID BS-Wthr.¹⁹⁶

6.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Pre-retrofit air infiltration in cubic feet per minute at 50 Pascal
- Post-retrofit air infiltration in cubic feet per minute at 50 Pascal
- Cooling type (central refrigerated cooling, room air conditioner, none)
- Heating type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
- Square footage of the residence conditioned space
- Shielding level (well shielded, normal, exposed)
- Number of bedrooms
- Number of stories
- Number of occupants
- Pre- and post-photos of blower door test readings

¹⁹⁶ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

- Representative photos of leak repairs

Document Revision History

Table 6.1-6: [Air Infiltration] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Added electric resistance documentation adjustment factor. |
| FY 2026 | Clarified application of electric resistance documentation adjustment factor. Updated eligibility to all residential customers, as applicable. |

6.2 CEILING INSULATION

6.2.1 Measure Description

Savings are estimated for insulation improvements made to the ceiling area above a conditioned space in a residence.

6.2.1.1 Eligibility Criteria

Cooling savings in this measure apply to customers with central or mini-split electric refrigerated air conditioning in their homes. Homes must be centrally heated with either a furnace (gas or electric resistance) or a heat pump to claim heating savings. Customers who participate in hard-to-reach (HTR) or low-income (LI) programs are eligible to claim reduced heating savings for homes heated with gas or electric resistance space heaters by applying an adjustment to deemed savings that is specified for that heat type. Customers participating in HTR or LI programs are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that is specified for homes with central refrigerated air.

6.2.1.2 Baseline Condition

Ceiling insulation levels encountered in existing homes can vary significantly, depending on factors such as the age of the home, type of insulation installed, and level of attic use (equipment, storage, etc.). Deemed savings have been developed based on different levels of encountered (existing) ceiling insulation in participating homes, ranging from sparsely insulated ($< R-5$) to the equivalent of about 6 inches of fiberglass batt insulation ($R-22$). The current average ceiling insulation level at participating homes is to be determined and documented by the insulation installer. Degradation due to age and density of the existing insulation should be taken into account.

If existing insulation is or has been removed during measure implementation, the existing R-value for claiming savings shall be based upon the R-value of the existing insulation prior to removal.

If there are varying levels of existing insulation, an area-weighted U-factor should be used to find the effective R-value across the treated area. The U-factor should be taken from the existing insulation only. This approach should be used in single attic spaces and savings should be estimated separately for independent spaces where there is a separate heating or cooling method (i.e., additions).

6.2.1.3 Area-weighted U-factor Calculation Method:

$$U_A = [U_1 \times Area_1 + U_2 \times Area_2 + \dots] / [Area_1 + Area_2 + \dots]$$

$$Effective\ Rvalue = \frac{1}{U_A}$$

Equation 6.2-1

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.¹⁹⁷ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.¹⁹⁸ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Demand Savings Tables sections.

6.2.1.4 High-Efficiency Condition

A minimum ceiling insulation level of R-30 is recommended throughout Texas as prescribed by the Department of Energy. Accordingly, deemed savings are provided for insulating to R-30. Accordingly, deemed savings are provided for insulating to R-30. Adjustment factors are provided to allow contractors to estimate savings for installation of higher or lower levels of post-retrofit insulation. Contractors should estimate achieved post-retrofit R-value according to the average insulation depth across the treated area and the R-per-inch of the insulation material installed.

6.2.2 Energy and Demand Savings Methodology

6.2.2.1 Savings Algorithms and Input Variables

Calibrated simulation modeling was used to develop these deemed savings values. Specifically, these deemed savings estimates were developed by using BEopt 2.6 software, running EnergyPlus 8.4 as the underlying simulation engine. To model this measure, the prototype home models were modified as follows: the default R-value of ceiling insulation (R-15) was set at different levels, ranging from R-0 (no ceiling insulation) to R-22. These modifications are shown in Table 6.2-1.

The model runs produced estimated peak demand and energy use for the modeled home at each of the base case ceiling insulation levels. The change-case models were run with the ceiling insulated to R-30.

¹⁹⁷ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

¹⁹⁸ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

Table 6.2-1: [Ceiling Insulation] Prototypical Home Characteristics

| Shell Characteristic | Value | Source |
|---------------------------|-------------------------------------|--------------------------------|
| Base Ceiling Insulation | R0-R4 R5-R8 R9-R14 R15-R22 | Existing insulation level |
| Change Ceiling Insulation | R-30 | R-30 retrofit insulation level |

Energy Savings

Energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of ceiling insulation installed (ceiling area net of framing materials) are presented in the deemed energy savings tables below.

Demand Savings

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4CP) demand savings are estimated in accordance with the definitions provided in Section 2.3 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of ceiling insulation installed are presented in the deemed demand savings tables below.

6.2.2.2 Deemed Energy Savings Tables

Table 6.2-2 presents the cooling and heating energy savings (kWh) achieved for every square foot of R-30 ceiling insulation installed in attics in CPS Energy's service territory. Annual energy savings are the sum of the cooling savings and the heating savings for the appropriate heating equipment type.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.2-2 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by multiplying heating savings in Table 6.2-2 by a factor of 0.24.¹⁹⁹

$$\text{Energy Savings } [\Delta kWh] = (R30 \text{ Savings}/ft^2_c \times CAF + R30 \text{ Savings}/ft^2_h \times HAF \times DAF) \times A$$

Equation 6.2-2

¹⁹⁹ This factor was derived based on expected capacity reduction assuming 1200 sqft (historical analysis of HTR participants) x 0.35 BTU/sqft = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields 10,200 ÷ 42,000 = 0.24.

Where:

| | | |
|------------------------------|---|---|
| $R30 \text{ Savings/ft}^2_c$ | = | Deemed cooling energy savings per square foot; see Table 6.2-2. |
| CAF | = | Cooling adjustment factor in Table 6.2-3. |
| $R30 \text{ Savings/ft}^2_H$ | = | Deemed heating energy savings per square foot; see Table 6.2-2. |
| HAF | = | Heating adjustment factor in Table 6.2-3. |
| DAF | = | Documentation adjustment factor; set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases. |
| A | = | Treated area [ft^2]. |

Table 6.2-2: [Ceiling Insulation] Energy Savings for R-30 Insulation (kWh/sq. ft.)

| Ceiling Insulation Base R Value | Cooling Savings | Heating Savings | | |
|------------------------------------|-----------------|-----------------|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| R-0 to R-4 | 1.29 | 0.07 | 1.86 | 0.78 |
| R-5 to R-8 | 0.58 | 0.03 | 0.87 | 0.37 |
| R-9 to R-14 | 0.30 | 0.02 | 0.47 | 0.20 |
| R-15 to R-22 | 0.13 | 0.01 | 0.20 | 0.09 |

Table 6.2-3: [Ceiling Insulation] CAF/HAF, Cooling & Heating Adjustment Factors

| HVAC System Type | CAF | HAF |
|----------------------------------|------|------|
| Central AC | 1.00 | - |
| Window or Room AC | 0.60 | - |
| Central Furnace or HP | - | 1.00 |
| Electric Resistance Space Heater | - | 0.24 |
| None | - | - |

Scale Down/Up Factors: Insulation to above or below R-30

The factors presented in this section are to be used when the average post-retrofit insulation depth provides less or more than R-30 insulation. Scale down factors are provided for the case when average post-retrofit insulation depth is not sufficient to achieve R-30; scale up factors are provided for the case when a contractor chooses to insulate to a level greater than R-30. In either case, the following equation should be applied to scale down or scale up the energy savings.

$$\begin{aligned} \text{Deemed Energy Savings (kWh)} &= \{ [R30 \text{ Savings}/ft^2_c + [S_{D/U,C} \times (R_{Achieved} - 30)] \times CAF] \\ &+ [R30 \text{ Savings}/ft^2_H + [S_{D/U,H} \times (R_{Achieved} - 30)] \times HAF \times DAF] \} \times A \end{aligned}$$

Equation 6.2-3

Where:

$S_{D/U,C}$ = Project-appropriate Scale-down or Scale-up Cooling Factor from either of Table 6.2-4 or Table 6.2-5.

$S_{D/U,H}$ = Project-appropriate Scale-down or Scale-up Heating Factor from either of Table 6.2-4 or Table 6.2-5.

$R_{Achieved}$ = Achieved R-value of installed insulation (e.g., for R-28, $R_{Achieved} = 28$).

If the ceiling is insulated to a level less than R-30, the following factors shall be applied to scale down the achieved energy savings per square foot of treated ceiling area.

Table 6.2-4: [Ceiling Insulation] Energy Savings Scale Down Factors for less than R-30 (kWh/sq. ft./ΔR)

| Cooling Factor | Heating Factors by Primary Heat Source | | |
|-----------------------|--|-----------------------|-----------------------|
| | Gas | Electric Resistance | Heat Pump |
| 8.20×10^{-3} | 4.88×10^{-4} | 1.29×10^{-2} | 5.44×10^{-3} |

If the ceiling is insulated to a level greater than R-30, the following factors shall be applied to scale up the achieved energy savings per square foot of treated ceiling area.

Table 6.2-5: [Ceiling Insulation] Energy Savings Scale Up Factors for greater than R-30 (kWh/sq. ft./ΔR)

| Cooling Factor | Heating Factors by Primary Heat Source | | |
|-----------------------|--|-----------------------|-----------------------|
| | Gas | Electric Resistance | Heat Pump |
| 5.44×10^{-3} | 3.11×10^{-4} | 8.58×10^{-3} | 3.63×10^{-3} |

6.2.2.3 Deemed Demand Savings Tables

Table 6.2-6 presents the non-coincident peak (NCP), coincident peak (CP), and ERCOT 4CP demand savings (kW) per sq. ft. associated with ceiling insulation for San Antonio.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.2-6 by a factor of 0.6.

$$\text{Demand Savings } [\Delta kW] = R30\text{Savings}/ft^2 \times AF \times A$$

Equation 6.2-4

Where:

$R30 \text{ Savings}/ft^2 =$ Deemed NCP, CP, or 4CP demand savings per square foot; see Table 6.2-6.

$AF =$ Adjustment factor based on HVAC system type in Table 6.2-7.

Table 6.2-6: [Ceiling Insulation] Deemed Demand Savings for R-30 Insulation (kW/sq. ft.)

| Ceiling Insulation Base R-value | NCP by Primary Heat Source | | | CP | 4CP |
|---------------------------------|----------------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| | Gas | Electric Resistance | Heat Pump | | |
| R-0 to R-4 | 1.81×10^{-3} | 2.00×10^{-3} | 1.14×10^{-3} | 1.23×10^{-3} | 1.08×10^{-3} |
| R-5 to R-8 | 8.32×10^{-4} | 9.37×10^{-4} | 5.73×10^{-4} | 5.49×10^{-4} | 5.05×10^{-4} |
| R-9 to R-14 | 4.94×10^{-4} | 5.20×10^{-4} | 3.24×10^{-4} | 2.90×10^{-4} | 2.71×10^{-4} |
| R-15 to R-22 | 2.50×10^{-4} | 2.58×10^{-4} | 2.36×10^{-4} | 1.28×10^{-4} | 1.19×10^{-4} |

Table 6.2-7: [Ceiling Insulation] AF, Adjustment Factors

| Cooling System Type | NCP Adjustment Factor by Primary Heat Source | | | | CP and 4CP Adjustment Factor by Primary Heat Source | | | |
|---------------------|--|-----|-----|------|---|-----|-----|------|
| | Gas | ER | HP | None | Gas | ER | HP | None |
| Central AC | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Window or Room AC | 0.6 | 1.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| None | - | 1.0 | - | - | - | - | - | - |

Scale Down/Up Factors: Insulation to Above or Below R-30

The factors presented in this section are to be used when the average post-retrofit insulation depth is providing more or less than R-30 insulation. Scale down factors are provided for the case when average post-retrofit insulation depth is not sufficient to achieve R-30; scale up factors are provided for the case when a contractor chooses to insulate to a level greater than R-30. In either case, the following equation should be applied to scale down or scale up the NCP, CP, or 4CP deemed demand savings.

$$\text{Deemed Demand Savings (kW)} = \{R30 \text{ Savings}/ft^2 + [S_{D/U} * (R_{Achieved} - 30)]\} \times AF \times A$$

Equation 6.2-5

Where:

$S_{D/U} =$ Project-appropriate Scale-down or Scale-up factor from Table 6.2-8.

If the ceiling is insulated to a level less than or greater than R-30, use the appropriate factor from Table 6.2-8 to scale down or scale up the achieved demand savings per square foot of treated ceiling area.

Table 6.2-8: [Ceiling Insulation] Demand Savings Scale Down/Up Factors (kW/sq. ft./ΔR)

| $S_{D/U}$ | Scale Factor (kW/sq. ft./ΔR) |
|--|---------------------------------|
| Scale Down Factor, S_D , if final insulation is less than R-30 | 8.04×10^{-6} |
| Scale Up Factor, S_U if final insulation is greater than R-30 | 5.44×10^{-6} |

Example Deemed Savings Calculation

Example 1 (Scale Up). A contractor installs 550 square feet of R-38 insulation in the attic of a home with central air conditioning and an electric resistance furnace that had existing insulation estimated at R-5.

$$\text{Cooling energy savings per sq. ft.} = 0.58 + 5.44 \times 10^{-3} \times (38 - 30) = 0.62 \text{ kWh/sq. ft.}$$

$$\text{Heating energy savings per sq. ft.} = 0.87 + 8.58 \times 10^{-3} \times (38 - 30) = 0.94 \text{ kWh/sq. ft.}$$

$$\text{Energy savings} = (0.62 + 0.94) \times 550 = 858 \text{ kWh}$$

$$\text{NCP demand savings per sq. ft.} = 9.37 \times 10^{-4} + 5.44 \times 10^{-6} \times (38 - 30) = 9.81 \times 10^{-4} \text{ kW/sq. ft.}$$

$$\text{NCP demand savings} = 9.81 \times 10^{-4} \times 550 = 0.54 \text{ kW}$$

$$\text{CP demand savings per sq. ft.} = 5.49 \times 10^{-4} + 5.44 \times 10^{-6} \times (38 - 30) = 5.93 \times 10^{-4} \text{ kW/sq. ft.}$$

$$\text{CP demand savings} = 5.93 \times 10^{-4} \times 550 = 0.33 \text{ kW}$$

$$\text{4CP demand savings per sq. ft.} = 5.05 \times 10^{-4} + 5.44 \times 10^{-6} \times (38 - 30) = 5.49 \times 10^{-4} \text{ kW/sq. ft.}$$

$$\text{4CP demand savings} = 5.49 \times 10^{-4} \times 550 = 0.30 \text{ kW}$$

Example 2 (Scale Down). A contractor installs 550 square feet of R-26 insulation in the attic of a home with central air conditioning and a gas furnace that had no existing ceiling insulation.

$$\text{Cooling energy savings per sq. ft.} = 1.58 + 8.20 \times 10^{-3} \times (26 - 30) = 1.55 \text{ kWh/sq. ft.}$$

$$\text{Heating energy savings per sq. ft.} = 0.09 + 4.88 \times 10^{-4} \times (26 - 30) = 0.09 \text{ kWh/sq. ft.}$$

$$\text{energy savings} = (1.55 + 0.09) \times 550 = 902 \text{ kWh}$$

$$\text{NCP demand savings per sq. ft.} = 2.09 \times 10^{-3} + 8.04 \times 10^{-6} \times (26 - 30) = 2.06 \times 10^{-3} \text{ kW/sq. ft.}$$

$$\text{NCP demand savings} = (2.06 \times 10^{-3}) \times 550 = 1.13 \text{ kW}$$

$$\text{CP demand savings per sq. ft.} = 1.45 \times 10^{-3} + 8.04 \times 10^{-6} \times (26 - 30) = 1.42 \times 10^{-3} \text{ kW/sq. ft.}$$

$$\text{CP demand savings} = (1.42 \times 10^{-3}) \times 550 = 0.78 \text{ kW}$$

$$\text{4CP demand savings per sq. ft.} = 1.30 \times 10^{-3} + 8.04 \times 10^{-6} \times (26 - 30) = 1.27 \times 10^{-3} \text{ kW/sq. ft.}$$

$$\text{4CP demand savings} = (1.27 \times 10^{-3}) \times 550 = 0.70 \text{ kW}$$

6.2.2.4 Measure Life and Lifetime Savings

According to the GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007),²⁰⁰ the estimated useful life is 25 years for ceiling insulation.

6.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Base R-value of original insulation
- R-value of installed insulation
- Cooling system type (central refrigerated cooling, room air conditioner, none)
- Heating system type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
- Square footage of ceiling insulation installed above a conditioned space
- For homes with a reported baseline R-value that is less than R-5:
 - Two pictures: (1) a picture showing the entire attic floor, and (2) a close-up picture of a ruler that shows the measurement of the depth of the insulation.
 - Note: The second photo type is required for each area of insulation where there are varying R-values less than R-5. Additionally, both photo types are required for all separate attic/ceiling areas, even when the installed R-value is the same.

Document Revision History

Table 6.2-9: [Ceiling Insulation] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Added electric resistance documentation adjustment factor. |
| FY 2026 | Clarified application of electric resistance documentation adjustment factor. |

²⁰⁰ GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007).
http://library.cee1.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLightsandHVACGDS_1Jun2007.pdf.

6.3 ATTIC ENCAPSULATION

6.3.1 Measure Description

Savings are estimated for bringing the attic into conditioned space by insulating and sealing the attic walls and roofs, eliminating leakage (to outside) and removing ceiling insulation, if present, to enhance airflow between the attic and the conditioned space directly below. Savings are presented according to Insulation Improvement and Infiltration Reduction components. Participants are expected to claim the sum of component savings.

6.3.1.1 Eligibility Criteria

Cooling savings in this measure apply to customers with central or mini-split electric refrigerated air conditioning in their homes. Residences must be centrally heated with either a furnace (gas or electric resistance) or a heat pump to claim heating savings. Customers participating in hard-to-reach (HTR) or low income (LI) programs are eligible to claim reduced heating savings for homes heated with gas or electric resistance space heaters by applying an adjustment to deemed savings that is specified for that heat type. Customers participating in HTR or LI programs are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that are specified for homes with central refrigerated air.

6.3.1.2 Baseline Condition

The baseline condition is a vented, unfinished attic with some level of ceiling insulation. Ceiling insulation levels in existing construction can vary significantly, depending on the age of the home, type of insulation installed, and activity in the attic (such as using the attic for storage and HVAC equipment). Deemed savings have been developed based on different levels of encountered (existing) ceiling insulation in participating homes, ranging from sparsely insulated (< R-5) to the equivalent of about 6 inches of fiberglass batt insulation (R-22). The average ceiling insulation level prior to the retrofit at participating homes is to be determined and documented by the contractor. Degradation due to age and density of the existing insulation should be considered.

Because existing ceiling insulation must be removed during measure implementation, the existing R-value will be based upon the R-value of the existing insulation prior to removal.

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.²⁰¹ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.²⁰² Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Summer

²⁰¹ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

²⁰² Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

Demand Savings Tables sections.

6.3.1.3 High-Efficiency Condition

A minimum ceiling insulation level of R-30 is recommended throughout Texas as prescribed by the Department of Energy.²⁰³ Accordingly, deemed savings are provided for insulating to R-30. Adjustment factors are provided to allow contractors to estimate savings for installation of higher or lower levels of post-retrofit insulation. Contractors should estimate post-retrofit R-value according to the average insulation depth achieved across the area treated and the R-per-inch of the insulation material installed.

Vents are sealed, as are obvious leaks. Ceiling insulation between the attic and the conditioned space is removed.

6.3.2 Energy and Demand Savings Methodology

The energy and demand savings produced by the attic encapsulation measures have two components: 1) reduced heat transfer into the attic from the insulation improvement; and 2) reduced leakage of conditioned air to outside by closing off vents and sealing of leaks. Accordingly, deemed energy and demand savings are presented by their insulation and air infiltration components. Both Insulation Improvement component and Infiltration Reduction component savings should be claimed for all projects. Insulation Improvement component savings shall be claimed using deemed savings derived for the ceiling insulation measure, as explained below. There are two paths for claiming Infiltration Reduction component savings depending on whether pre- and post-retrofit blower door testing is undertaken when implementing the attic encapsulation measure. If blower door testing is performed, savings for the Infiltration Reduction component can be estimated according to the Residential Air Infiltration Measure. If blower door testing is not undertaken, savings for the Infiltration Reduction component shall be claimed as presented in the Air Infiltration Reduction Component savings presented in this measure (below).

In previous versions of the Guidebook, energy and demand savings for the attic encapsulation measure have been presented according to the results achieved by directly modeling the attic encapsulation measure according to a best interpretation of how the measure should be represented. The expectation is that this measure should, at minimum, provide savings commensurate with those obtained from the installation of ceiling insulation. In general, the measure is expected to out-perform ceiling insulation. However, the modeling results have not reflected this expectation due to complications with sufficiently accounting for infiltration reduction, resulting in lower deemed savings for the attic encapsulation measure than those estimated for ceiling insulation. To encourage implementation of the measure and begin to develop information about the outcomes, the savings presented in this measure for the Insulation Improvement component of the Attic Encapsulation Measure are equivalent to the ceiling insulation measure savings. After adding Air Infiltration Reduction component savings to the Insulation Improvement component savings, attic encapsulation measure savings will exceed those of the ceiling

²⁰³ Department of Energy Insulation R-value recommendations for zone 2/3, <https://www.energy.gov/energysaver/weatherize/insulation>.

insulation measure.

6.3.2.1 Savings Algorithms and Input Variables (Insulation Component)

Calibrated simulation modeling was used to develop these deemed savings values. Specifically, these deemed savings estimates were developed by modeling *the ceiling insulation measure* using BEopt 2.6, running EnergyPlus 8.4 as the underlying simulation engine. For details on the derivation of these savings, refer to the Residential Ceiling Insulation Measure.

Energy Savings (Insulation Component)

Energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of ceiling insulation installed (ceiling area net of framing materials) are presented in the deemed energy savings tables below.

Demand Savings (Insulation Component)

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4CP) demand savings are estimated in accordance with the definitions provided in Section 2.3 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of ceiling insulation installed are presented in the deemed demand savings tables below.

6.3.2.2 Deemed Energy Savings Tables (Insulation Component)

Table 6.3-1 presents the cooling and heating energy savings (kWh) achieved for every square foot of R-30 ceiling insulation installed in attics in CPS Energy's service territory. Annual energy savings are the sum of the cooling savings and the heating savings for the appropriate heating equipment type.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.3-1 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by multiplying heating savings in Table 6.3-1 by a factor of 0.24.²⁰⁴

²⁰⁴ This factor was derived based on expected capacity reduction assuming 1200 sqft (historical analysis of HTR participants) x 0.35 BTU/sqft = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields $10,200 \div 42,000 = 0.24$.

$$\text{Energy Savings } [\Delta kWh] = (R30 \text{ Savings}/ft^2_c \times CAF + R30 \text{ Savings}/ft^2_H \times HAF \times DAF) \times A$$

Equation 6.3-1

Where:

| | | |
|------------------------------|---|---|
| $R30 \text{ Savings}/ft^2_c$ | = | Deemed cooling energy savings per square foot; see Table 6.3-1. |
| CAF | = | Cooling adjustment factor in Table 6.3-2. |
| $R30 \text{ Savings}/ft^2_H$ | = | Deemed heating energy savings per square foot; see Table 6.3-1. |
| HAF | = | Heating adjustment factor in Table 6.3-2. |
| DAF | = | Documentation adjustment factor, set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases. |
| A | = | Treated area $[ft^2]$. |

Table 6.3-1: [Attic Encapsulation] Energy Savings for R-30 Insulation (kWh/sq. ft.)

| Ceiling Insulation Base R Value | Cooling Savings | Heating Savings | | |
|------------------------------------|-----------------|-----------------|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| R-0 to R-4 | 1.29 | 0.07 | 1.86 | 0.78 |
| R-5 to R-8 | 0.58 | 0.03 | 0.87 | 0.37 |
| R-9 to R-14 | 0.30 | 0.02 | 0.47 | 0.20 |
| R-15 to R-22 | 0.13 | 0.01 | 0.20 | 0.09 |

Table 6.3-2: [Attic Encapsulation] CAF/HAF, Cooling & Heating Adjustment Factors

| HVAC System Type | CAF | HAF |
|----------------------------------|------|------|
| Central AC | 1.00 | - |
| Window or Room AC | 0.60 | - |
| Central Furnace or HP | - | 1.00 |
| Electric Resistance Space Heater | - | 0.24 |
| None | - | - |

Scale Down/Up Factors: Insulation to above or below R-30

The factors presented in this section are to be used when the average post-retrofit insulation depth provides less or more than R-30 insulation. Scale down factors are provided for the case when average post-retrofit insulation depth is not sufficient to achieve R-30; scale up factors are provided for the case when a contractor chooses to insulate to a level greater than R-30. In either case, the following equation should be applied to scale down or scale up the energy savings.

$$\begin{aligned}
\text{Energy Savings } [\Delta kWh] &= \{ [R30 \text{ Savings}/ft^2_c + [S_{D/U,C} \times (R_{Achieved} - 30)] \times CAF] \\
&+ [R30 \text{ Savings}/ft^2_H + [S_{D/U,H} \times (R_{Achieved} - 30)] \times HAF \times DAF] \} \times A
\end{aligned}$$

Equation 6.3-2

Where:

$S_{D/U,C}$ = Project-appropriate Scale-down or Scale-up Cooling Factor from either of Table 6.3-3 or Table 6.3-4.

$S_{D/U,H}$ = Project-appropriate Scale-down or Scale-up Heating Factor from either of Table 6.3-3 or Table 6.3-4.

$R_{Achieved}$ = Achieved R-value of installed insulation (e.g., for R-28, $R_{Achieved} = 28$).

If the ceiling is insulated to a level less than R-30, the following factors shall be applied to scale down the achieved energy savings per square foot of treated ceiling area.

Table 6.3-3: [Attic Encapsulation] Energy Savings Scale Down Factors for less than R-30 (kWh/sq. ft./ΔR)

| Cooling Factor | Heating Factors by Primary Heat Source | | |
|-----------------------|--|-----------------------|-----------------------|
| | Gas | Electric Resistance | Heat Pump |
| 8.20×10^{-3} | 4.88×10^{-4} | 1.29×10^{-2} | 5.44×10^{-3} |

If the ceiling is insulated to a level greater than R-30, the following factors shall be applied to scale up the achieved energy savings per square foot of treated ceiling area.

Table 6.3-4: [Attic Encapsulation] Energy Savings Scale Up Factors for greater than R-30 (kWh/sq. ft./ΔR)

| Cooling Factor | Heating Factors by Primary Heat Source | | |
|-----------------------|--|-----------------------|-----------------------|
| | Gas | Electric Resistance | Heat Pump |
| 5.44×10^{-3} | 3.11×10^{-4} | 8.58×10^{-3} | 3.63×10^{-3} |

6.3.2.3 Deemed Demand Savings Tables (Insulation Component)

Table 6.3-5 presents the non-coincident peak (NCP), coincident peak (CP), and ERCOT 4CP demand savings (kW) per sq. ft. associated with ceiling insulation for San Antonio.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.3-5 by a factor of 0.6.

$$\text{Demand Savings } [\Delta kW] = R30 \text{ Savings}/ft^2 \times AF \times A$$

Equation 6.3-3

Where:

$R30 \text{ Savings}/ft^2 =$ Deemed NCP, CP, or 4CP demand savings per square foot; see Table 6.3-5.

$AF =$ Adjustment factor based on HVAC system type in Table 6.3-6.

Table 6.3-5: [Attic Encapsulation] Deemed Demand Savings for R-30 Insulation (kW/sq. ft.)

| Ceiling Insulation Base R-value | NCP by Primary Heat Source | | | CP | 4CP |
|------------------------------------|----------------------------|------------------------|-----------------------|-----------------------|-----------------------|
| | Gas | Electric Resistance | Heat Pump | | |
| R-0 to R-4 | 1.81×10^{-3} | 2.00×10^{-3} | 1.14×10^{-3} | 1.23×10^{-3} | 1.08×10^{-3} |
| R-5 to R-8 | 8.32×10^{-4} | 9.37×10^{-4} | 5.73×10^{-4} | 5.49×10^{-4} | 5.05×10^{-4} |
| R-9 to R-14 | 4.94×10^{-4} | 5.20×10^{-4} | 3.24×10^{-4} | 2.90×10^{-4} | 2.71×10^{-4} |
| R-15 to R-22 | 2.50×10^{-4} | 2.58×10^{-4} | 2.36×10^{-4} | 1.28×10^{-4} | 1.19×10^{-4} |

Table 6.3-6: [Attic Encapsulation] AF, Adjustment Factors

| Cooling System Type | NCP Adjustment Factor by Primary Heat Source | | | | CP and 4CP Adjustment Factor by Primary Heat Source | | | |
|---------------------|---|-----|-----|------|--|-----|-----|------|
| | Gas | ER | HP | None | Gas | ER | HP | None |
| Central AC | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Window or Room AC | 0.6 | 1.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| None | - | 1.0 | - | - | - | - | - | - |

Scale Down/Up Factors: Insulation to Above or Below R-30

The factors presented in this section are to be used when the average post-retrofit insulation depth is providing more or less than R-30 insulation. Scale down factors are provided for the case when average post-retrofit insulation depth is not sufficient to achieve R-30; scale up factors are provided for the case when a contractor chooses to insulate to a level greater than R-30. In either case, the following equation should be applied to scale down or scale up the NCP, CP, or 4CP deemed demand savings.

$$\text{Deemed Demand Savings (kW)} = \{R30 \text{ Savings}/ft^2 + [S_{D/U} * (R_{Achieved} - 30)]\} \times AF \times A \times DAF$$

Equation 6.3-4

Where:

$S_{D/U} =$ Project-appropriate Scale-down or Scale-up factor from Table 6.3-7.

If the ceiling is insulated to a level less than or greater than R-30, use the appropriate factor from Table 6.3-7 to scale down or scale up the achieved demand savings per square foot of treated ceiling area.

Table 6.3-7: [Attic Encapsulation] Demand Savings Scale Down/Up Factors (kW/sq. ft./ΔR)

| $S_{D/U}$ | Scale Factor (kW/sq. ft./ΔR) |
|--|---------------------------------|
| Scale Down Factor, S_D , if final insulation is less than R-30 | 8.04×10^{-6} |
| Scale Up Factor, S_U if final insulation is greater than R-30 | 5.44×10^{-6} |

6.3.2.4 Savings Algorithms and Input Variables (Infiltration Component)

Energy and Demand savings for the Air Infiltration Reduction component of the attic encapsulation measure are calculated either using the results of pre- and post-retrofit blower door testing or using an average percent infiltration reduction. Regardless of how Air Infiltration Reduction component savings are calculated, they should be added to the Insulation Improvement component savings to arrive at the total energy and demand savings for implementing the Attic Encapsulation Measure.

Homes without refrigerated cooling should not claim Air Infiltration Reduction component savings for attic encapsulation.

With Blower Door Testing

Implementers choosing to perform pre- and post-measure blower door testing should claim Air Infiltration Reduction component deemed energy and demand savings for the Attic Encapsulation Measure using the estimated CFM₅₀ reduction from the blower door tests with the equations and coefficients in the Residential Infiltration Measure (Section 6.1 Air Infiltration).

Without Blower Door Testing

Implementers electing not to perform blower door testing when performing this measure shall claim Air Infiltration Reduction component deemed energy and demand savings for the Attic Encapsulation Measure using this section, which presents the annual energy (kWh) and demand savings (kW) associated with attic encapsulation in San Antonio, considering a mean leakage reduction of 18 percent.²⁰⁵ Savings are presented per home.

Calibrated simulation modeling was used to develop air infiltration reduction deemed savings, which are expressed in the Residential Air Infiltration measure as linear functions of the leakage reduction achieved (in CFM₅₀).²⁰⁶ For details on the derivation of the air infiltration measure savings, refer to the Residential Air Infiltration measure.

ACCA Manual J provides an average leakage reduction attributable to attic encapsulation projects of 18

²⁰⁵ Section 21-14 of ACCA Manual J states that, "...a foam encapsulated attic eliminates ceiling leakage to the outdoors (i.e., to a vented attic), which means that the reduction in infiltration CFM may range from 3 to 30 percent, with an 18 percent mean, as noted above." See Air Conditioning Contractors of America. Manual J, 8th Edition Version 2.10. Nov. 2011, p. 188.

²⁰⁶ Model testing indicates a straight-line relationship between demand and energy savings achieved and CFM₅₀ reductions is appropriate with beginning and ending leakage rates within the ranges permitted by the measure.

percent.²⁰⁷ Accordingly, deemed savings attributable to the Air Infiltration Reduction component of an attic encapsulation project implemented without pre- and post-implementation blower door testing are estimated by applying an 18 percent leakage reduction to the infiltration rates embedded in the deemed savings prototype model homes used in the derivation of residential envelope measure deemed savings for the Guidebook. This 18 percent leakage reduction provides the CFM₅₀ reduction input required to estimate air infiltration measure deemed savings with the equations in the Residential Air Infiltration measure.

Table 6.3-8: [Attic Encapsulation] Prototypical Home Characteristics

| Shell Characteristics | CFM ₅₀ Reduction | Source |
|---|-----------------------------|---|
| Air Infiltration Reduction from Attic Encapsulation (without Blower Door Testing) | 18% reduction | Mean reduction achieved via attic encapsulation according to ACCA Manual J, 8 th Edition, Section 21-14 ²⁰⁸ |

6.3.2.5 Deemed Energy Savings Tables (Infiltration Component)

Annual energy savings are provided by space heating equipment type combined with refrigerated cooling. Savings are specified per home based on a deemed 18 percent infiltration reduction. Homes without refrigerated cooling are not eligible to claim these savings.

Table 6.3-9: [Attic Encapsulation] Infiltration Reduction Deemed Energy Savings (kWh/home)

| Heating Type | | | |
|--------------|---------------------|-----------|------|
| Gas | Electric Resistance | Heat Pump | None |
| 178 | 577 | 337 | 178 |

6.3.2.6 Deemed Demand Savings Tables (Infiltration Component)

Demand savings are specified per home based on a deemed 18 percent infiltration reduction. Homes without refrigerated cooling are not eligible to claim these savings.

²⁰⁷ Air Conditioning Contractors of America. Manual J, 8th Edition Version 2.10. Nov. 2011, p. 188.

²⁰⁸ Section 21-14 of ACCA Manual J states that, "...a foam encapsulated attic eliminates ceiling leakage to the outdoors (i.e., to a vented attic), which means that the reduction in infiltration Cfm may range from 3 to 30 percent, with an 18 percent mean, as noted above." See Air Conditioning Contractors of America. Manual J, 8th Edition Version 2.10. Nov. 2011, p. 188.

Table 6.3-10: [Attic Encapsulation] Infiltration Reduction Deemed Demand Savings (kW/home)

| Peak Type | Heating Type | Refrigerated Air kW/home |
|-----------|---------------------|--------------------------|
| NCP | Gas | 0.301 |
| | Electric Resistance | 1.031 |
| | Heat Pump | 0.396 |
| CP | All | 0.134 |
| 4CP | All | 0.120 |

Example Deemed Savings Calculation

A contractor seals the attic and adds R-38 insulation to the underside of the roof to a home with 900 square feet of conditioned space below the treated attic with refrigerated air and a gas furnace, which has existing ceiling insulation estimated at R-7. No blower door testing is performed.

Insulation Component Savings:

$$\text{Energy Savings}/ft^2, \text{Insulation to } R - 30 = 0.58 + 0.03 = 0.61 \text{ kWh}/ft^2$$

$$\text{Energy Savings, Insulation to } R - 38 =$$

$$\{0.61 + [(5.44 \times 10^{-3} + 3.11 \times 10^{-4}) \times (38 - 30)]\} \times 900 = 590 \text{ kWh}$$

$$\text{NCP Summer Demand Savings, Insulation to } R - 38 =$$

$$\{8.32 \times 10^{-4} + [5.44 \times 10^{-6} \times (38 - 30)]\} \times 900 = 0.788 \text{ kW}$$

$$\text{CP Summer Demand Savings, Insulation to } R - 38 =$$

$$\{5.49 \times 10^{-4} + [5.44 \times 10^{-6} \times (38 - 30)]\} \times 900 = 0.533 \text{ kW}$$

$$\text{4CP Summer Demand Savings, Insulation to } R - 38 =$$

$$\{5.05 \times 10^{-4} + [5.44 \times 10^{-6} \times (38 - 30)]\} \times 900 = 0.494 \text{ kW}$$

Infiltration Reduction Component Savings:

$$\text{Energy Savings, 18\% Infiltration Reduction} = 178 \text{ kWh}$$

$$\text{NCP Summer Demand Savings, 18\% Infiltration Reduction} = 0.301 \text{ kW}$$

$$\text{CP Summer Demand Savings, 18\% Infiltration Reduction} = 0.134 \text{ kW}$$

$$\text{4CP Summer Demand Savings, 18\% Infiltration Reduction} = 0.120 \text{ kW}$$

Measure Savings:

$$\text{Energy Savings} = 590.4 + 177.9 = 768 \text{ kWh}$$

$$\text{NCP Summer Demand Savings} = 0.788 + 0.301 = 1.089 \text{ kW}$$

$$\text{CP Summer Demand Savings} = 0.533 + 0.134 = 0.667 \text{ kW}$$

$$\text{4CP Summer Demand Savings} = 0.494 + 0.120 = 0.614 \text{ kW}$$

6.3.2.7 Measure Life and Lifetime Savings

According to the GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007),²⁰⁹ the Estimated Useful Life is 25 years for ceiling insulation. The measure life specified for ceiling insulation is also appropriate for attic encapsulation.

6.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Base R-value of original ceiling insulation
- R-value of installed roof deck insulation
- Cooling system type (central refrigerated cooling, room air conditioner, none)
- Heating system type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
- Square footage of ceiling area below encapsulated attic
- For homes with a reported baseline R-value that is less than R-5, the following documentation:
 - Two pictures: (1) a picture showing the entire attic floor, and (2) a close-up picture of a ruler that shows the measurement of the depth of the insulation
 - Note: The second photo type is required for each area of insulation where there are varying R-values less than R-5. Additionally, both photo types are required for all separate attic/ceiling areas, even when the installed R-value is the same

²⁰⁹ GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007).
http://library.cee1.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLightsandHVACGDS_1Jun2007.pdf.

- Indicate whether blower door testing was performed and whether air infiltration reduction component savings are claimed in this measure or separately using the Residential Air Infiltration measure

Document Revision History

Table 6.3-11: [Attic Encapsulation] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Added electric resistance documentation adjustment factor. |
| FY 2026 | Clarified application of electric resistance documentation adjustment factor. |

6.4 WALL INSULATION

6.4.1 Measure Description

Wall insulation is added to the walls surrounding conditioned space in existing homes by removing wall enclosures and applying batt or spray insulation into the cavity space between studs in the walls. Walls may be of either 2x4 or 2x6 construction. Savings are estimated for filling the wall cavities of 2x4 or 2x6 walls with fiberglass batts, cellulose, or closed-cell spray foam, and are presented per square foot of treated wall area (gross wall area less window and door area).

6.4.1.1 Eligibility Criteria

Cooling savings in this measure apply to customers with central or mini-split electric refrigerated air conditioning in their homes. Homes must be centrally heated with either a furnace (gas or electric resistance) or a heat pump to claim heating savings. Customers who participate in hard-to-reach (HTR) or low-income (LI) programs are eligible to claim reduced heating savings for homes heated with gas or electric resistance space heaters by applying an adjustment to deemed savings that is specified for that heat type. Customers participating in HTR or LI programs are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that is specified for homes with central refrigerated air.

Refer to the Baseline Condition section below for eligibility criteria regarding the pre-retrofit level of wall insulation.

6.4.1.2 Baseline Condition

The baseline is a house with little or no wall insulation in the wall cavity. For those homes for which a minimal level of insulation is encountered, the baseline is established at R-4. This baseline should be used to represent homes for which installed insulation covers a very limited amount of the wall area to be treated, is significantly degraded, and/or is less than an inch thick.

Baseline homes may have either 2x4 or 2x6 construction.

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.²¹⁰ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.²¹¹ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Demand Savings Tables sections.

²¹⁰ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

²¹¹ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

6.4.1.3 High-Efficiency Condition

The standard throughout Texas for adding wall insulation to an existing wall cavity is R-13, as prescribed by United States Department of Energy (DOE) and Texas Department of Housing & Community Affairs (TDHCA) programs. The standard is achieved by filling a 2x4 wall cavity with fiberglass batt or cellulose insulation, which typically provides an R-value per inch (thickness) of between 3 and 4 hr·ft²·°F/BTU. Other wall insulation materials may be used, such as closed-cell spray foam, which approximately provides R-6 per inch.

As such, deemed savings are provided for insulating 2x4 and 2x6 walls to the levels presented in Table 6.4-1.

Table 6.4-1: [Wall Insulation] High-Efficiency Condition R-Values for 2x4 and 2x6 Walls

| Insulation Material | 2x4 | 2x6 |
|------------------------------|------|------|
| Fiberglass Batt or Cellulose | R-13 | R-17 |
| Closed-cell Spray Foam | R-21 | R-33 |

Wall insulation reduces the ventilation rate in the home, and therefore, a post-installation blower door test must be conducted. Results must comply with the minimum final ventilation rate discussed in the High-Efficiency Condition section found in the Air Infiltration measure.

6.4.2 Energy and Demand Savings Methodology

6.4.2.1 Savings Algorithms and Input Variables

Calibrated simulation modeling was used to develop these deemed savings values. Specifically, these deemed savings estimates were developed using BEopt 2.6, running EnergyPlus 8.4 as the underlying simulation engine. To model this measure, the prototype home model for San Antonio was modified as follows: the default R-11 insulation was reduced to either R-0 or R-4.

The model runs calculated energy use for the prototypical home prior to the installation of the wall insulation measure. Next, change-case models were run to calculate energy use with the wall insulation measure in place.

Table 6.4-2: [Wall Insulation] Prototypical Home Characteristics

| Shell Characteristic | Value | Source |
|----------------------|------------|---|
| Base Wall Insulation | R-0 R-4 | BEopt estimates wall assembly R-value for uninsulated walls to be 3.6 for 2x4 construction and 3.7 for 2x6 construction. Assembly R-values for R-4 walls are 6.7 and 7.1 for 2x4 and 2x6 construction, respectively. Listed base levels are for the insulation material only. |

| Shell Characteristic | Value | Source |
|------------------------------------|--------------|---|
| Change Wall Insulation 2x4 wall | R-13 R-21 | For retrofit with fiberglass batt/cellulose and closed-cell spray foam, respectively. |
| Change Wall Insulation 2x6 wall | R-17 R-33 | For retrofit with fiberglass batt/cellulose and closed-cell spray foam, respectively. |

Energy Savings

Energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of insulation installed are presented in the deemed energy savings tables below.

Demand Savings

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4CP) demand savings are estimated in accordance with the definitions provided in Section 2.4 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of insulation installed are presented in the deemed demand savings tables below.

6.4.2.2 Deemed Energy Savings Tables

Savings are presented separately for insulating 2x4 wall construction and homes with 2x6 walls. Annual energy savings are the sum of cooling and heating savings for the appropriate equipment types.

Table 6.4-3 through Table 6.4-6 presents the cooling and heating energy savings (kWh) achieved per square foot of ceiling area beneath the encapsulated attic in CPS Energy's service territory. Annual energy savings are the sum of the cooling savings and the heating savings for the appropriate heating equipment type.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.2-2 through Table 6.4-6 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by multiplying heating savings in Table 6.2-2 through Table 6.4-6 by a factor of 0.24.²¹²

For residences reporting electric resistance heat, a documentation adjustment factor of 0.75 will be applied to deemed heating energy savings if no documentation is provided to validate the heating equipment. In all other cases, the documentation adjustment factor is set to 1.0.

²¹² This factor was derived based on expected capacity reduction assuming 1200 sqft (historical analysis of HTR participants) x 0.35 BTU/sqft = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields $10,200 \div 42,000 = 0.24$.

$$\text{Energy Savings } [\Delta kWh] = (\text{Savings}/ft^2_c \times CAF + \text{Savings}/ft^2_H \times HAF \times DAF) \times A$$

Equation 6.4-1

Where:

$\text{Savings}/ft^2_c$ = Deemed cooling energy savings per square feet; see Table 6.2-2 through Table 6.4-6.

CAF = Cooling adjustment factor in Table 6.4-7.

$\text{Savings}/ft^2_H$ = Deemed heating energy savings per square feet; see Table 6.2-2 through Table 6.4-6.

HAF = Heating adjustment factor in Table 6.4-7.

DAF = Documentation adjustment factor, set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases.

A = Area of the wall [ft^2].

2x4 Walls

Table 6.4-3 presents the deemed energy savings values for insulating 2x4 walls to R-13 for San Antonio.

Table 6.4-3: [Wall Insulation] Deemed Annual Energy Savings, Insulation of 2x4 Walls to R- 13 (kWh/sq. ft.)

| Base Case Wall Insulation | Cooling Savings | Heating Savings by Primary Heat Source | | |
|---------------------------|-----------------|--|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| Uninsulated (R-0) | 1.13 | 0.07 | 1.62 | 0.68 |
| R-4 | 0.41 | 0.03 | 0.62 | 0.26 |

Table 6.4-4 presents the deemed energy savings values for insulating 2x4 walls to R-21 for San Antonio.

Table 6.4-4: [Wall Insulation] Deemed Annual Energy Savings, Insulation of 2x4 Walls to R- 21 (kWh/sq. ft.)

| Base Case Wall Insulation | Cooling Savings | Heating Savings by Primary Heat Source | | |
|---------------------------|-----------------|--|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| Uninsulated (R-0) | 1.26 | 0.08 | 1.81 | 0.76 |
| R-4 | 0.54 | 0.03 | 0.81 | 0.34 |

2x6 Walls

Table 6.4-5 presents the deemed energy savings values for insulating 2x6 walls to R-17 for San Antonio.

Table 6.4-5: [Wall Insulation] Deemed Annual Energy Savings, Insulation of 2x6 Walls to R-17 (kWh/sq. ft.)

| Base Case Wall Insulation | Cooling Savings | Heating Savings by Primary Heat Source | | |
|---------------------------|-----------------|--|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| Uninsulated (R-0) | 1.21 | 0.08 | 1.74 | 0.73 |
| R-4 | 0.49 | 0.03 | 0.73 | 0.31 |

Table 6.4-6 presents the deemed energy savings values for insulating 2x6 walls to R-33 for San Antonio.

Table 6.4-6: [Wall Insulation] Deemed Annual Energy Savings, Insulation of 2x6 Walls to R-33 (kWh/sq. ft.)

| Base Case Wall Insulation | Cooling Savings | Heating Savings by Primary Heat Source | | |
|---------------------------|-----------------|--|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| Uninsulated (R-0) | 1.34 | 0.09 | 1.94 | 0.81 |
| R-4 | 0.62 | 0.04 | 0.93 | 0.39 |

Table 6.4-7: [Wall Insulation] CAF/HAF, Cooling & Heating Adjustment Factors

| HVAC System Type | CAF | HAF |
|----------------------------------|------|------|
| Central AC | 1.00 | - |
| Window or Room AC | 0.60 | - |
| Central Furnace or HP | - | 1.00 |
| Electric Resistance Space Heater | - | 0.24 |
| None | - | - |

6.4.2.3 Deemed Demand Savings Tables

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.4-8 through Table 6.4-9 by a factor of 0.6.

$$\text{Demand Savings } [\Delta kW] = \text{Savings}/ft^2 \times AF \times A$$

Equation 6.4-2

Where:

$$\text{Savings}/ft^2 = \text{Deemed NCP, CP, or 4CP demand savings per square feet; see Table 6.4-8}$$

through Table 6.4-9.

$AF =$ Adjustment factor based on HVAC system type in Table 6.4-10.

2x4 Walls

Table 6.4-8 presents the deemed demand savings values for insulating 2x4 walls to R-13 and R-21.

Table 6.4-8: [Wall Insulation] Deemed Demand Savings, Insulation of 2x4 Walls (kW/sq. ft.)

| Base Case Wall Insulation | Peak Type | Primary Heat Source | R-13 Installed | R-21 Installed |
|---------------------------|-----------|---------------------|-----------------------|-----------------------|
| Uninsulated (R-0) | NCP | Gas | 1.64×10^{-3} | 1.73×10^{-3} |
| | | ER | 1.98×10^{-3} | 2.22×10^{-3} |
| | | HP | 9.48×10^{-4} | 1.04×10^{-3} |
| | CP | All | 8.64×10^{-4} | 9.69×10^{-4} |
| | 4CP | All | 8.13×10^{-4} | 9.05×10^{-4} |
| R-4 | NCP | Gas | 8.42×10^{-4} | 9.56×10^{-4} |
| | | ER | 7.62×10^{-4} | 1.01×10^{-3} |
| | | HP | 4.82×10^{-4} | 5.72×10^{-4} |
| | CP | All | 3.11×10^{-4} | 4.17×10^{-4} |
| | 4CP | All | 2.89×10^{-4} | 3.81×10^{-4} |

2x6 Walls

Table 6.4-9 presents deemed demand savings values for insulating 2x6 walls to R-13 and R-21.

Table 6.4-9: [Wall Insulation] Deemed Demand Savings, Insulation of 2x6 Walls (kW/sq. ft.)

| Base Case Wall Insulation | Peak Type | Primary Heat Source | R-17 Installed | R-33 Installed |
|---------------------------|-----------|---------------------|-----------------------|-----------------------|
| Uninsulated (R-0) | NCP | Gas | 1.69×10^{-3} | 1.81×10^{-3} |
| | | ER | 2.14×10^{-3} | 2.40×10^{-3} |
| | | HP | 1.01×10^{-3} | 1.11×10^{-3} |
| | CP | All | 9.43×10^{-4} | 1.04×10^{-3} |
| | 4CP | All | 8.78×10^{-4} | 9.72×10^{-4} |
| R-4 | NCP | Gas | 9.92×10^{-4} | 1.06×10^{-3} |
| | | ER | 9.21×10^{-4} | 1.19×10^{-3} |
| | | HP | 5.72×10^{-4} | 6.39×10^{-4} |

| Base Case Wall Insulation | Peak Type | Primary Heat Source | R-17 Installed | R-33 Installed |
|---------------------------|-----------|---------------------|-----------------------|-----------------------|
| | CP | All | 3.83×10^{-4} | 4.82×10^{-4} |
| | 4CP | All | 3.44×10^{-4} | 4.38×10^{-4} |

Table 6.4-10: [Wall Insulation] AF, Adjustment Factors

| Cooling System Type | NCP Adjustment Factor by Primary Heat Source | | | | CP and 4CP Adjustment Factor by Primary Heat Source | | | |
|---------------------|--|-----|-----|------|---|-----|-----|------|
| | Gas | ER | HP | None | Gas | ER | HP | None |
| Central AC | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Window or Room AC | 0.6 | 1.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| None | - | 1.0 | - | - | - | - | - | - |

6.4.2.4 Measure Life and Lifetime Savings

According to the GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007),²¹³ the Estimated Useful Life is 25 years for wall insulation.

6.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Cooling type (central refrigerated cooling, room air conditioner, none)
- Heating type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
- Square footage of retrofitted wall area (gross wall area less window and door area)

Document Revision History

Table 6.4-11: [Wall Insulation] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
|-------------------|-----------------------|

²¹³ GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007).
http://library.cce1.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLightsandHVACGDS_1Jun2007.pdf.

| | |
|---------|---|
| FY 2025 | Added electric resistance documentation adjustment factor. |
| FY 2026 | Clarified application of electric resistance documentation adjustment factor. |

6.5 FLOOR INSULATION

6.5.1 Measure Description

Floor insulation is installed on the underside of floor areas that sit below conditioned space. Typically, it is installed in ventilated crawlspaces. Savings are presented per square foot of treated floor area.

6.5.1.1 Eligibility Criteria

Cooling savings in this measure apply to customers with central or mini-split electric refrigerated air conditioning in their homes. Homes must be centrally heated with either an electric resistance furnace or a heat pump to claim heating savings. Customers who participate in hard-to-reach (HTR) or low-income (LI) programs are eligible to claim reduced heating savings for homes heated with electric resistance space heaters by applying an adjustment to deemed savings that is specified for that heat type. Customers participating in HTR or LI programs are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that is specified for homes with central refrigerated air.

Homes with gas heating are disqualified for adding floor insulation since this may result in an energy penalty due to floors not getting cooled from the ground during summer.

6.5.1.2 Baseline Condition

The baseline is a house with pier and beam construction and with uninsulated floors beneath the conditioned space.

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.²¹⁴ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.²¹⁵ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Demand Savings Tables sections.

6.5.1.3 High-Efficiency Condition

A floor insulation level of R-19 is recommended for site-built homes throughout Texas as prescribed by DOE and Texas Department of Housing & Community Affairs (TDHCA) programs. Batt insulation is recommended in most cases and must have the vapor barrier installed facing up and against the floor or conditioned area. Insulation should be attached or secured so that it can reasonably be expected to

²¹⁴ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

²¹⁵ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

remain in place for at least 10 years.

Typical floor construction depth of manufactured homes usually does not allow R-19 batt to be installed within the floor joists, so R-15 loose-fill insulation is recommended by TDHCA.

A minimum of 24-inch clearance from bottom of the insulation to the ground is required by Occupational Safety and Health Association (OSHA).

6.5.2 Energy and Demand Savings Methodology

6.5.2.1 Savings Algorithms and Input Variables

Calibrated simulation modeling was used to develop these deemed savings values.

Savings values for the deemed savings estimates for this measure were developed using demand and energy savings calculated using BEopt 2.6, running Energy Plus 8.1 as the underlying simulation engine. To model this measure, the prototype home models for each climate zone were modified as follows: slab foundation was replaced with a crawlspace. A 5/8" thick wood floor is also specified.

The model runs calculated energy use for the prototypical home prior to the installation of the floor insulation measure. Next, change-case models were run to calculate energy use with the floor insulation measure in place.

Table 6.5-1: [Floor Insulation] Prototypical Home Characteristics

| Shell Characteristic | Value | Source |
|-------------------------|---|---|
| Foundation | Crawlspace | Skirting around the perimeter is assumed uninsulated and vented. The ground under the home is assumed to be bare, without any type of moisture barrier. |
| Base Floor Insulation | R-3.1 | BEopt default for floor assembly, assuming 5/8" thick hardwood floor without carpet or another type of covering. |
| Change Floor Insulation | R-19 (except for manufactured housing, R-15) | Efficiency measure - retrofit insulation level as required by DOE and Texas Department of Housing and Community Affairs programs in Texas. Due to the typical floor joists depths found in manufactured housing, TDHCA recommends R-15 loose-fill insulation for manufactured housing and other non-site-built homes. |

Energy Savings

Energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of treated floor area are presented in the deemed energy savings tables below.

Demand Savings

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4 CP) demand savings are estimated in accordance with the definitions provided in Section 2.4 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of insulation installed are presented in the deemed demand savings tables below.

6.5.2.2 Deemed Energy Savings Tables

Table 6.5-2 presents the cooling and heating energy savings (kWh) achieved per square foot of insulation in CPS Energy's service territory. Annual energy savings are the sum of the cooling savings and the heating savings for the appropriate heating equipment type.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.5-2 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by multiplying heating savings in Table 6.5-2 by a factor of 0.24.²¹⁶

For residences reporting electric resistance heat, a documentation adjustment factor of 0.75 will be applied to deemed heating energy savings if no documentation is provided to validate the heating equipment. In all other cases, the documentation adjustment factor is set to 1.0.

$$\text{Energy Savings } [\Delta kWh] = (\text{Savings}/ft^2_c \times CAF + \text{Savings}/ft^2_H \times HAF \times DAF) \times A$$

Equation 6.5-1

Where:

| | | |
|-------------------------|---|---|
| $\text{Savings}/ft^2_c$ | = | Deemed cooling energy savings per square feet; see Table 6.5-2. |
| CAF | = | Cooling adjustment factor in Table 6.5-3. |
| $\text{Savings}/ft^2_H$ | = | Deemed heating energy savings per square feet; see Table 6.5-2. |
| HAF | = | Heating adjustment factor in Table 6.5-3. |
| DAF | = | Documentation adjustment factor, set to 0.75 for residences reporting electric resistance heat with no backup documentation or set to 1.0 in all other cases. |
| A | = | Area of the ceiling beneath the encapsulated attic [ft^2]. |

²¹⁶ This factor was derived based on expected capacity reduction assuming 1200 sqft (historical analysis of HTR participants) x 0.35 BTU/sqft = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields $10,200 \div 42,000 = 0.24$.

Table 6.5-2: [Floor Insulation] Deemed Annual Energy Savings (kWh/sq. ft.)

| Home Type | Cooling Savings | Heating Savings | | |
|------------|-----------------|-----------------|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| Site-Built | 0.090 | 0.042 | 1.153 | 0.460 |
| Mfd. Home | 0.085 | 0.038 | 1.048 | 0.417 |

Table 6.5-3: [Floor Insulation] CAF/HAF, Cooling & Heating Adjustment Factors

| HVAC System Type | CAF | HAF |
|----------------------------------|------|------|
| Central AC | 1.00 | - |
| Window or Room AC | 0.60 | - |
| Central Furnace or HP | - | 1.00 |
| Electric Resistance Space Heater | - | 0.24 |
| None | - | - |

6.5.2.3 Deemed Demand Savings Tables

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.5-4 by a factor of 0.6.

$$\text{Demand Savings } [\Delta kW] = \text{Savings}/ft^2 \times AF \times A$$

Equation 6.5-2

Where:

$\text{Savings}/ft^2$ = Deemed NCP, CP, or 4CP demand savings per square feet; see Table 6.5-4.

AF = Adjustment factor based on HVAC system type in Table 6.5-5

Table 6.5-4: [Floor Insulation] Deemed Annual Demand Savings (kW/sq. ft.)

| Peak Type | Primary Heat Source | Site-Built | Manufactured |
|-----------|---------------------|-----------------------|-----------------------|
| NCP | Gas | 1.74×10^{-4} | 1.57×10^{-4} |
| | Electric Resistance | 1.06×10^{-3} | 9.69×10^{-4} |
| | Heat Pump | 4.75×10^{-4} | 4.37×10^{-4} |
| CP | All | 1.74×10^{-4} | 1.57×10^{-4} |
| 4CP | All | 1.43×10^{-4} | 1.27×10^{-4} |

Table 6.5-5: [Floor Insulation] AF, Adjustment Factors

| Cooling System Type | NCP Adjustment Factor by Primary Heat Source | | | | CP and 4CP Adjustment Factor by Primary Heat Source | | | |
|---------------------|--|-----|-----|------|---|-----|-----|------|
| | Gas | ER | HP | None | Gas | ER | HP | None |
| Central AC | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Window or Room AC | 0.6 | 1.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| None | - | 1.0 | - | - | - | - | - | - |

6.5.2.4 Measure Life and Lifetime Savings

According to the GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007),²¹⁷ the Estimated Useful Life is 25 years for floor insulation.

6.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Cooling type (central refrigerated cooling, room air conditioner, none)
- Heating type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
- Home type (site-built or manufactured)
- Square footage of installed insulation

²¹⁷ GDS Associates Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures (2007). http://library.cce1.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLightsandHVACGDS_1Jun2007.pdf.

Document Revision History

Table 6.5-6: [Floor Insulation] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Added electric resistance documentation adjustment factor. |
| FY 2026 | Clarified application of electric resistance documentation adjustment factor. |

6.6 COOL ROOFS

6.6.1 Measure Description

Reflective roofing materials reduce the overall heat load on a home by reducing the total heat energy absorbed into the building system from incident solar radiation. This reduction in total load provides space cooling energy savings during cooling season but reduces free heat during heating season, so the measure saves energy in the summer but uses more energy in winter. As such, cool roofs are most beneficial in warmer climates, and furthermore may not be recommendable for homes in which the primary heat source is electric resistance. The measure is for retrofit of existing homes.

6.6.1.1 Eligibility Criteria

Cooling savings in this measure apply to customers with central or mini-split electric refrigerated air conditioning in their homes. Homes must be centrally heated with either a furnace (gas or electric resistance) or a heat pump to claim heating savings. Customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs are eligible to claim reduced heating savings for homes heated with gas or electric resistance space heaters by applying an adjustment to deemed savings that is specified for that heat type. Customers participating in HTR or LI programs are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that are specified for homes with central refrigerated air.

6.6.1.2 Baseline Condition

The baseline condition is an existing home with a standard medium- or dark-colored roof.

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.²¹⁸ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.²¹⁹ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Demand Savings Tables sections.

6.6.1.3 High-Efficiency Condition

The ENERGY STAR roofing products certification program was discontinued effective June 1, 2022.²²⁰ Moving forward, installed roofing products will still be required to demonstrate compliance with the previous ENERGY STAR specification.²²¹

²¹⁸ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

²¹⁹ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

²²⁰ ENERGY STAR Roof Products Sunset Decision Memo.

<https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Roof%20Products%20Sunset%20Decision%20Memo.pdf>.

²²¹ ENERGY STAR Program Requirements for Roof Products v2.1.

https://www.energystar.gov/ia/partners/product_specs/program_reqs/roofs_prog_req.pdf.

In lieu of the former ENERGY STAR list of qualified products, roofing products must now have a performance rating that is validated by the Cool Roof Rating Council (CRRC)^{222,223} and be listed on the CRRC Rated Roof Products Directory.²²⁴ This is consistent with the former ENERGY STAR test criteria²²⁵, which allows for products already participating in the CRRC Product Rating Program²²⁶ to submit solar reflectance and thermal emittance product information derived from CRRC certification.

The ENERGY STAR program classifies roofs with slope greater than 2/12 as having a steep slope and roofs with slope less than or equal to 2/12 as low slope roofs. ENERGY STAR performance specifications for cool roof products for use on roofs with steep slopes and low slopes are provided in Table 6.6-1.

If a cool roof is installed concurrent with changes to attic insulation levels, savings should be claimed for the reflective roof according to the post-retrofit (ceiling or roof deck) insulation levels. Savings for changes in insulation levels should be claimed separately according to the attic floor insulation or attic encapsulation measures, assuming the retrofit performed meets the requirements of those measures.

Table 6.6-1: [Cool Roofs] ENERGY STAR Specification

| Roof Slope | Characteristic | Performance Specification |
|----------------------|---------------------------|---------------------------|
| Low Slope ≤ 2/12 | Initial Solar Reflectance | ≥ 0.65 |
| | 3-Year Solar Reflectance | ≥ 0.50 |
| High Slope > 2/12 | Initial Solar Reflectance | ≥ 0.25 |
| | 3-Year Solar Reflectance | ≥ 0.15 |

6.6.2 Energy and Demand Savings Methodology

Energy and demand savings are presented for cool roofs according to the rated 3-year reflectance of the installed cool roof product and the type of roof (low-slope, high-slope) on which it is installed.

6.6.2.1 Savings Algorithms and Input Variables

Calibrated simulation modeling was used to develop these deemed savings values. Specifically, these deemed savings estimates were developed using BEopt 2.6, running EnergyPlus 8.4 as the underlying simulation engine. To model this measure, the prototype home models for San Antonio were modified as follows. Roof slopes were modified to reflect representative levels for the low slope and steep slope roofs. A 1/12 slope was selected for modeling low slope roofs (defined as having slope ≤ 2/12), and a 4/12 slope was selected for modeling steep slope roofs (slope > 2/12). Based on the performance criteria and review of the rated 3-year reflectance of rated products listed in the CRRC database, four reflectance levels were

²²² CRRC guidance for roof rating alternative to discontinued ENERGY STAR® program. <https://coolroofs.org/documents/CRRC-ENERGY-STAR-Sunset-Info-Sheet-2022-03-07.pdf>.

²²³ CRRC Roof Rating Program. <https://coolroofs.org/programs/roof-rating-program>.

²²⁴ CRRC Rated Roof Products Directory. <https://coolroofs.org/directory/roof>.

²²⁵ ENERGY STAR Program Requirements for Roof Products v2.1.

https://www.energystar.gov/ia/partners/product_specs/program_reqs/roofs_prog_req.pdf.

²²⁶ CRRC Rated Products Directory: <https://coolroofs.org/directory>.

selected for modeling: 0.2, 0.4, 0.6 and 0.8, representing 20 to 80 percent reflectance.

Because of the interplay between the performance of insulation and attic/roof deck temperatures, which are directly affected by the installation of a cool roof, savings were estimated for a range of different attic insulation scenarios: a range of attic floor insulation levels from no insulation (R-0) to R-30, and two roof deck insulation levels, R-19 and R-38, were modeled. Savings for a roof deck insulation level of R-30 are provided by interpolating between the R-19 and R-38 scenarios. These modifications are shown in Table 6.6-2.

The model runs calculated energy use for the prototypical home prior to encapsulating the attic. Next, change-case models were run to calculate energy use with the floor insulation measure in place with either R-30 or R-38 insulation.

Table 6.6-2: [Cool Roofs] Prototypical Home Characteristics

| Shell Characteristic | Value | Source |
|--|---|---|
| Base Case Roof Material | Medium Asphalt Shingle, Reflectance = 0.15 | Prototype home default |
| Change Case Roof Material | Medium Asphalt Shingle, Reflectance = 0.2 Reflectance = 0.4 Reflectance = 0.6 Reflectance = 0.8 | Lower reflectance levels only relevant for steep slope roofs. Modeled reflectance levels reflect midpoints of ranges: 0.15 ≤ R < 0.3 Reflectance 0.3 ≤ R < 0.5 Reflectance 0.5 ≤ R < 0.7 Reflectance > 0.7 |
| Roof Slope: Low-Slope Roof | 1/12 | Not modified between base and change cases |
| Roof Slope: Steep Slope Roof | 4/12 | Not modified between base and change cases |
| Ceiling (attic floor) Insulation Levels | < R-5 R5-R8 R9-R14 R15-R22 R-30 | Not modified between base and change cases |
| Roof Deck (underside) Insulation Levels | R-19 R-38 | Not modified between base and change cases |

6.6.2.2 Deemed Energy Savings Tables

Savings are presented first for homes with attic floor insulation, and subsequently for those with roof deck insulation. For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.6-3 through Table 6.6-6 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by

multiplying heating savings in Table 6.6-3 through Table 6.6-6 by a factor of 0.24.²²⁷

Homes with Ceiling Insulation

Table 6.6-3 presents the energy savings (kWh) for installation of a reflective roof on homes with varying levels of ceiling (attic floor) insulation. Annual energy savings are the sum of cooling and heating savings for the appropriate equipment types. Savings are per square foot of treated roof area.

Table 6.6-3: [Cool Roofs] Home with AFI - Deemed Annual Energy Savings (kWh/sq. ft.)

| Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | Cooling Savings (Refrigerated) | Heating Savings | | |
|--------------------------------------|--|--------------------------------------|-----------------|-------|-------|
| | | | Gas | ER | HP |
| Steep Slope | | | | | |
| R-0 to R-4 | 0.15 - 0.29 | 0.09 | 0.00 | -0.03 | -0.01 |
| R-0 to R-4 | 0.3 – 0.49 | 0.47 | -0.01 | -0.17 | -0.07 |
| R-0 to R-4 | 0.5 – 0.69 | 0.86 | -0.01 | -0.32 | -0.13 |
| R-0 to R-4 | ≥ 0.7 | 1.26 | -0.02 | -0.49 | -0.20 |
| R-5 to R-8 | 0.15 - 0.29 | 0.06 | 0.00 | -0.02 | -0.01 |
| R-5 to R-8 | 0.3 – 0.49 | 0.30 | 0.00 | -0.09 | -0.04 |
| R-5 to R-8 | 0.5 – 0.69 | 0.54 | -0.01 | -0.18 | -0.08 |
| R-5 to R-8 | ≥ 0.7 | 0.80 | -0.01 | -0.27 | -0.12 |
| R-9 to R-14 | 0.15 - 0.29 | 0.04 | 0.00 | -0.01 | -0.01 |
| R-9 to R-14 | 0.3 – 0.49 | 0.22 | 0.00 | -0.07 | -0.03 |
| R-9 to R-14 | 0.5 – 0.69 | 0.41 | 0.00 | -0.13 | -0.06 |
| R-9 to R-14 | ≥ 0.7 | 0.61 | -0.01 | -0.19 | -0.09 |
| R-15 to R-22 | 0.15 - 0.29 | 0.03 | 0.00 | -0.01 | 0.00 |
| R-15 to R-22 | 0.3 – 0.49 | 0.17 | 0.00 | -0.05 | -0.02 |
| R-15 to R-22 | 0.5 – 0.69 | 0.32 | 0.00 | -0.09 | -0.04 |
| R-15 to R-22 | ≥ 0.7 | 0.47 | 0.00 | -0.13 | -0.06 |
| R-30 | 0.15 - 0.29 | 0.03 | 0.00 | -0.01 | 0.00 |
| R-30 | 0.3 – 0.49 | 0.14 | 0.00 | -0.03 | -0.02 |
| R-30 | 0.5 – 0.69 | 0.25 | 0.00 | -0.06 | -0.03 |
| R-30 | ≥ 0.7 | 0.37 | 0.00 | -0.09 | -0.04 |

²²⁷ This factor was derived based on expected capacity reduction assuming 1200 sqft (historical analysis of HTR participants) x 0.35 BTU/sqft = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields 10,200 ÷ 42,000 = 0.24.

| Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | Cooling Savings (Refrigerated) | Heating Savings | | |
|--------------------------------------|--|--------------------------------------|-----------------|-------|-------|
| | | | Gas | ER | HP |
| Low Slope | | | | | |
| R-0 to R-4 | 0.5 – 0.69 | 0.93 | -0.01 | -0.35 | -0.14 |
| R-0 to R-4 | ≥ 0.7 | 1.36 | -0.02 | -0.54 | -0.22 |
| R-5 to R-8 | 0.5 – 0.69 | 0.61 | -0.01 | -0.20 | -0.09 |
| R-5 to R-8 | ≥ 0.7 | 0.88 | -0.01 | -0.31 | -0.13 |
| R-9 to R-14 | 0.5 – 0.69 | 0.47 | 0.00 | -0.15 | -0.06 |
| R-9 to R-14 | ≥ 0.7 | 0.68 | -0.01 | -0.22 | -0.10 |
| R-15 to R-22 | 0.5 – 0.69 | 0.37 | 0.00 | -0.10 | -0.05 |
| R-15 to R-22 | ≥ 0.7 | 0.54 | 0.00 | -0.15 | -0.07 |
| R-30 | 0.5 – 0.69 | 0.20 | 0.00 | 0.00 | -0.03 |
| R-30 | ≥ 0.7 | 0.29 | 0.00 | 0.00 | -0.05 |

Homes with Roof Deck Insulation

Table 6.6-4 presents the energy savings (kWh) for installation of a reflective roof on homes with varying levels of roof deck insulation. Annual energy savings are the sum of cooling and heating savings for the appropriate equipment types. Savings are per square foot of treated roof area.

Table 6.6-4: [Cool Roofs] Home with RDI - Deemed Annual Energy Savings (kWh/sq. ft.)

| Roof Deck Insulation R-value | Installed Roof Material 3-Year Reflectance | Cooling Savings (Refrigerated) | Heating Savings | | |
|------------------------------------|--|--------------------------------------|-----------------|------------------------|-------|
| | | | Gas | Electric Resistance | Gas |
| Steep Slope | | | | | |
| R-19 | 0.15 - 0.29 | 0.03 | 0.00 | -0.02 | -0.01 |
| R-19 | 0.3 – 0.49 | 0.18 | 0.00 | -0.09 | -0.04 |
| R-19 | 0.5 – 0.69 | 0.33 | -0.01 | -0.16 | -0.07 |
| R-19 | ≥ 0.7 | 0.49 | -0.01 | -0.24 | -0.10 |
| R-30 | 0.15 - 0.29 | 0.02 | 0.00 | -0.01 | -0.06 |
| R-30 | 0.3 – 0.49 | 0.15 | 0.00 | -0.07 | -0.04 |
| R-30 | 0.5 – 0.69 | 0.27 | 0.00 | -0.13 | -0.07 |
| R-30 | ≥ 0.7 | 0.40 | -0.01 | -0.19 | -0.10 |
| R-38 | 0.15 - 0.29 | 0.02 | 0.00 | -0.01 | -0.10 |
| R-38 | 0.3 – 0.49 | 0.13 | 0.00 | -0.06 | -0.04 |

| Roof Deck Insulation R-value | Installed Roof Material 3-Year Reflectance | Cooling Savings (Refrigerated) | Heating Savings | | |
|------------------------------|--|--------------------------------|-----------------|---------------------|-------|
| | | | Gas | Electric Resistance | Gas |
| R-38 | 0.5 – 0.69 | 0.23 | 0.00 | -0.11 | -0.07 |
| R-38 | ≥ 0.7 | 0.34 | -0.01 | -0.16 | -0.10 |
| Low Slope | | | | | |
| R-19 | 0.5 – 0.69 | 0.32 | 0.00 | -0.14 | -0.06 |
| R-19 | ≥ 0.7 | 0.47 | -0.01 | -0.21 | -0.09 |
| R-30 | 0.5 – 0.69 | 0.27 | 0.00 | -0.11 | -0.07 |
| R-30 | ≥ 0.7 | 0.39 | 0.00 | -0.16 | -0.10 |
| R-38 | 0.5 – 0.69 | 0.23 | 0.00 | -0.09 | -0.07 |
| R-38 | ≥ 0.7 | 0.34 | 0.00 | -0.13 | -0.10 |

6.6.2.3 Deemed Demand Savings Tables

Savings are presented first for homes with attic floor insulation, and subsequently for those with roof deck insulation. For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying appropriate cooling values in Table 6.6-5 through Table 6.6-6 by a factor of 0.6.

Homes with Attic Floor Insulation

Table 6.6-5 presents the demand savings (kW) associated with installation of a reflective roof in homes with varying levels of attic floor insulation. Savings are per square foot of treated roof area.

Table 6.6-5: [Cool Roofs] Home with AFI - Deemed Demand Savings (kW/sq. ft.)

| HVAC Type | Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|--------------------------------|--|----------|----------|----------|
| Steep Slope | | | | | |
| AC + Gas | R-0 to R-4 | 0.15 - 0.29 | 1.26E-04 | 6.91E-05 | 8.41E-05 |
| | R-0 to R-4 | 0.3 – 0.49 | 6.39E-04 | 3.51E-04 | 4.27E-04 |
| | R-0 to R-4 | 0.5 – 0.69 | 1.17E-03 | 6.42E-04 | 7.82E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.71E-03 | 9.36E-04 | 1.14E-03 |
| | R-5 to R-8 | 0.15 - 0.29 | 8.62E-05 | 4.34E-05 | 5.20E-05 |
| | R-5 to R-8 | 0.3 – 0.49 | 4.38E-04 | 2.21E-04 | 2.65E-04 |
| | R-5 to R-8 | 0.5 – 0.69 | 8.04E-04 | 4.05E-04 | 4.85E-04 |
| | R-5 to R-8 | ≥ 0.7 | 1.18E-03 | 5.96E-04 | 7.14E-04 |
| | R-9 to R-14 | 0.15 - 0.29 | 6.82E-05 | 3.17E-05 | 4.33E-05 |

| HVAC Type | Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|--------------------------------|--|----------|----------|----------|
| | R-9 to R-14 | 0.3 – 0.49 | 3.47E-04 | 1.61E-04 | 2.20E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 6.37E-04 | 2.96E-04 | 4.04E-04 |
| | R-9 to R-14 | ≥ 0.7 | 9.37E-04 | 4.36E-04 | 5.95E-04 |
| | R-15 to R-22 | 0.15 - 0.29 | 6.21E-05 | 2.44E-05 | 3.63E-05 |
| | R-15 to R-22 | 0.3 – 0.49 | 3.15E-04 | 1.24E-04 | 1.84E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.77E-04 | 2.27E-04 | 3.37E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.51E-04 | 3.34E-04 | 4.98E-04 |
| | R-30 | 0.15 - 0.29 | 5.69E-05 | 2.04E-05 | 3.22E-05 |
| | R-30 | 0.3 – 0.49 | 2.86E-04 | 1.02E-04 | 1.62E-04 |
| | R-30 | 0.5 – 0.69 | 5.29E-04 | 1.89E-04 | 3.00E-04 |
| | R-30 | ≥ 0.7 | 7.81E-04 | 2.80E-04 | 4.43E-04 |
| Low Slope | | | | | |
| AC + Gas | R-0 to R-4 | 0.5 – 0.69 | 1.28E-03 | 6.88E-04 | 7.94E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.86E-03 | 1.00E-03 | 1.16E-03 |
| | R-5 to R-8 | 0.5 – 0.69 | 8.02E-04 | 4.63E-04 | 5.07E-04 |
| | R-5 to R-8 | ≥ 0.7 | 1.17E-03 | 6.74E-04 | 7.38E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 6.17E-04 | 3.45E-04 | 4.42E-04 |
| | R-9 to R-14 | ≥ 0.7 | 9.02E-04 | 5.05E-04 | 6.46E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.89E-04 | 2.74E-04 | 3.58E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.57E-04 | 4.00E-04 | 5.22E-04 |
| | R-30 | 0.5 – 0.69 | 5.24E-04 | 2.28E-04 | 3.11E-04 |
| | R-30 | ≥ 0.7 | 7.63E-04 | 3.31E-04 | 4.53E-04 |
| Steep Slope | | | | | |
| AC + ER | R-0 to R-4 | 0.15 - 0.29 | 1.32E-04 | 7.53E-05 | 8.67E-05 |
| | R-0 to R-4 | 0.3 – 0.49 | 6.59E-04 | 3.76E-04 | 4.32E-04 |
| | R-0 to R-4 | 0.5 – 0.69 | 1.18E-03 | 6.71E-04 | 7.72E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.66E-03 | 9.48E-04 | 1.09E-03 |
| | R-5 to R-8 | 0.15 - 0.29 | 8.49E-05 | 4.54E-05 | 5.35E-05 |
| | R-5 to R-8 | 0.3 – 0.49 | 4.27E-04 | 2.28E-04 | 2.69E-04 |
| | R-5 to R-8 | 0.5 – 0.69 | 7.71E-04 | 4.12E-04 | 4.86E-04 |
| | R-5 to R-8 | ≥ 0.7 | 1.12E-03 | 5.98E-04 | 7.05E-04 |
| | R-9 to R-14 | 0.15 - 0.29 | 6.92E-05 | 3.32E-05 | 4.45E-05 |
| | R-9 to R-14 | 0.3 – 0.49 | 3.47E-04 | 1.67E-04 | 2.23E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 6.34E-04 | 3.04E-04 | 4.08E-04 |
| | R-9 to R-14 | ≥ 0.7 | 9.25E-04 | 4.43E-04 | 5.94E-04 |

| HVAC Type | Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|--------------------------------|--|----------|----------|----------|
| | R-15 to R-22 | 0.15 - 0.29 | 6.22E-05 | 2.52E-05 | 3.78E-05 |
| | R-15 to R-22 | 0.3 – 0.49 | 3.12E-04 | 1.27E-04 | 1.90E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.70E-04 | 2.31E-04 | 3.46E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.35E-04 | 3.38E-04 | 5.08E-04 |
| | R-30 | 0.15 - 0.29 | 6.10E-05 | 1.97E-05 | 3.17E-05 |
| | R-30 | 0.3 – 0.49 | 3.06E-04 | 9.88E-05 | 1.59E-04 |
| | R-30 | 0.5 – 0.69 | 5.65E-04 | 1.82E-04 | 2.94E-04 |
| | R-30 | ≥ 0.7 | 8.31E-04 | 2.68E-04 | 4.32E-04 |
| Low Slope | | | | | |
| AC + ER | R-0 to R-4 | 0.5 – 0.69 | 1.31E-03 | 7.14E-04 | 8.21E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.85E-03 | 1.01E-03 | 1.16E-03 |
| | R-5 to R-8 | 0.5 – 0.69 | 8.18E-04 | 4.65E-04 | 5.33E-04 |
| | R-5 to R-8 | ≥ 0.7 | 1.17E-03 | 6.63E-04 | 7.60E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 6.21E-04 | 3.42E-04 | 4.45E-04 |
| | R-9 to R-14 | ≥ 0.7 | 8.98E-04 | 4.95E-04 | 6.43E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.88E-04 | 2.77E-04 | 3.60E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.48E-04 | 3.99E-04 | 5.19E-04 |
| | R-30 | 0.5 – 0.69 | 5.24E-04 | 2.28E-04 | 3.21E-04 |
| | R-30 | ≥ 0.7 | 7.57E-04 | 3.30E-04 | 4.64E-04 |
| Steep Slope | | | | | |
| HP | R-0 to R-4 | 0.15 - 0.29 | 7.43E-05 | 5.71E-05 | 5.73E-05 |
| | R-0 to R-4 | 0.3 – 0.49 | 3.76E-04 | 2.89E-04 | 2.90E-04 |
| | R-0 to R-4 | 0.5 – 0.69 | 6.84E-04 | 5.25E-04 | 5.27E-04 |
| | R-0 to R-4 | ≥ 0.7 | 9.89E-04 | 7.59E-04 | 7.63E-04 |
| | R-5 to R-8 | 0.15 - 0.29 | 8.16E-05 | 4.30E-05 | 5.00E-05 |
| | R-5 to R-8 | 0.3 – 0.49 | 4.12E-04 | 2.17E-04 | 2.53E-04 |
| | R-5 to R-8 | 0.5 – 0.69 | 7.52E-04 | 3.96E-04 | 4.61E-04 |
| | R-5 to R-8 | ≥ 0.7 | 1.10E-03 | 5.81E-04 | 6.76E-04 |
| | R-9 to R-14 | 0.15 - 0.29 | 6.48E-05 | 3.18E-05 | 4.22E-05 |
| | R-9 to R-14 | 0.3 – 0.49 | 3.28E-04 | 1.61E-04 | 2.14E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 6.02E-04 | 2.96E-04 | 3.92E-04 |
| | R-9 to R-14 | ≥ 0.7 | 8.83E-04 | 4.34E-04 | 5.75E-04 |
| | R-15 to R-22 | 0.15 - 0.29 | 2.73E-05 | 1.84E-05 | 1.86E-05 |
| | R-15 to R-22 | 0.3 – 0.49 | 1.37E-04 | 9.27E-05 | 9.36E-05 |
| | R-15 to R-22 | 0.5 – 0.69 | 2.51E-04 | 1.70E-04 | 1.71E-04 |

| HVAC Type | Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|--------------------------------|--|----------|----------|----------|
| | R-15 to R-22 | ≥ 0.7 | 3.70E-04 | 2.50E-04 | 2.52E-04 |
| | R-30 | 0.15 - 0.29 | 2.23E-05 | 1.40E-05 | 1.43E-05 |
| | R-30 | 0.3 – 0.49 | 1.12E-04 | 7.03E-05 | 7.17E-05 |
| | R-30 | 0.5 – 0.69 | 2.06E-04 | 1.30E-04 | 1.32E-04 |
| | R-30 | ≥ 0.7 | 3.04E-04 | 1.92E-04 | 1.95E-04 |
| Low Slope | | | | | |
| HP | R-0 to R-4 | 0.5 – 0.69 | 1.23E-03 | 6.80E-04 | 7.78E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.78E-03 | 9.82E-04 | 1.12E-03 |
| | R-5 to R-8 | 0.5 – 0.69 | 7.76E-04 | 4.56E-04 | 5.06E-04 |
| | R-5 to R-8 | ≥ 0.7 | 1.12E-03 | 6.59E-04 | 7.31E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 5.85E-04 | 3.32E-04 | 4.24E-04 |
| | R-9 to R-14 | ≥ 0.7 | 8.52E-04 | 4.84E-04 | 6.18E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.60E-04 | 2.69E-04 | 3.45E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.13E-04 | 3.90E-04 | 5.01E-04 |
| | R-30 | 0.5 – 0.69 | 4.97E-04 | 2.22E-04 | 3.01E-04 |
| | R-30 | ≥ 0.7 | 7.20E-04 | 3.23E-04 | 4.36E-04 |
| Steep Slope | | | | | |
| AC, no heat | R-0 to R-4 | 0.15 - 0.29 | 7.48E-05 | 5.40E-05 | 5.07E-05 |
| | R-0 to R-4 | 0.3 – 0.49 | 3.80E-04 | 2.74E-04 | 2.58E-04 |
| | R-0 to R-4 | 0.5 – 0.69 | 6.96E-04 | 5.02E-04 | 4.72E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.02E-03 | 7.33E-04 | 6.89E-04 |
| | R-5 to R-8 | 0.15 - 0.29 | 4.69E-05 | 3.29E-05 | 3.10E-05 |
| | R-5 to R-8 | 0.3 – 0.49 | 2.34E-04 | 1.64E-04 | 1.55E-04 |
| | R-5 to R-8 | 0.5 – 0.69 | 4.22E-04 | 2.96E-04 | 2.79E-04 |
| | R-5 to R-8 | ≥ 0.7 | 6.25E-04 | 4.38E-04 | 4.13E-04 |
| | R-9 to R-14 | 0.15 - 0.29 | 2.96E-05 | 2.12E-05 | 1.99E-05 |
| | R-9 to R-14 | 0.3 – 0.49 | 1.63E-04 | 1.17E-04 | 1.09E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 3.03E-04 | 2.18E-04 | 2.04E-04 |
| | R-9 to R-14 | ≥ 0.7 | 4.51E-04 | 3.24E-04 | 3.03E-04 |
| | R-15 to R-22 | 0.15 - 0.29 | 6.21E-05 | 2.44E-05 | 3.63E-05 |
| | R-15 to R-22 | 0.3 – 0.49 | 3.14E-04 | 1.23E-04 | 1.84E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.77E-04 | 2.27E-04 | 3.37E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.51E-04 | 3.34E-04 | 4.97E-04 |
| | R-30 | 0.15 - 0.29 | 1.94E-05 | 1.37E-05 | 1.28E-05 |

| HVAC Type | Attic Floor Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|------------|--------------------------------|--|----------|----------|----------|
| | R-30 | 0.3 – 0.49 | 9.75E-05 | 6.89E-05 | 6.47E-05 |
| | R-30 | 0.5 – 0.69 | 1.80E-04 | 1.27E-04 | 1.19E-04 |
| | R-30 | ≥ 0.7 | 2.66E-04 | 1.88E-04 | 1.77E-04 |
| Low Slope | | | | | |
| AC no heat | R-0 to R-4 | 0.5 – 0.69 | 6.97E-04 | 5.49E-04 | 5.24E-04 |
| | R-0 to R-4 | ≥ 0.7 | 1.02E-03 | 8.01E-04 | 7.64E-04 |
| | R-5 to R-8 | 0.5 – 0.69 | 4.38E-04 | 3.36E-04 | 3.17E-04 |
| | R-5 to R-8 | ≥ 0.7 | 6.32E-04 | 4.84E-04 | 4.57E-04 |
| | R-9 to R-14 | 0.5 – 0.69 | 3.29E-04 | 2.47E-04 | 2.37E-04 |
| | R-9 to R-14 | ≥ 0.7 | 4.76E-04 | 3.58E-04 | 3.42E-04 |
| | R-15 to R-22 | 0.5 – 0.69 | 5.88E-04 | 2.74E-04 | 3.58E-04 |
| | R-15 to R-22 | ≥ 0.7 | 8.57E-04 | 3.99E-04 | 5.22E-04 |
| | R-30 | 0.5 – 0.69 | 2.01E-04 | 1.49E-04 | 1.39E-04 |
| | R-30 | ≥ 0.7 | 2.92E-04 | 2.17E-04 | 2.02E-04 |

Homes with Roof Deck Insulation

Table 6.6-6 presents the demand savings (kW) associated with installation of a reflective roof in homes with varying levels of roof deck insulation. Savings are per square foot of treated roof area.

Table 6.6-6: [Cool Roofs] Home with RDI - Deemed Demand Savings (kW/sq. ft.)

| HVAC Type | Roof Deck Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|------------------------------|--|----------|----------|----------|
| Steep Slope | | | | | |
| AC + Gas | R-19 | 0.15 - 0.29 | 4.43E-05 | 9.70E-06 | 1.63E-05 |
| | R-19 | 0.3 – 0.49 | 2.26E-04 | 4.96E-05 | 8.31E-05 |
| | R-19 | 0.5 – 0.69 | 4.17E-04 | 9.14E-05 | 1.53E-04 |
| | R-19 | ≥ 0.7 | 6.18E-04 | 1.35E-04 | 2.27E-04 |
| | R-30 | 0.15 - 0.29 | 2.52E-05 | 6.32E-06 | 9.77E-06 |
| | R-30 | 0.3 – 0.49 | 1.29E-04 | 3.23E-05 | 5.00E-05 |
| | R-30 | 0.5 – 0.69 | 2.37E-04 | 5.95E-05 | 9.21E-05 |
| | R-30 | ≥ 0.7 | 3.51E-04 | 8.82E-05 | 1.36E-04 |
| | R-38 | 0.15 - 0.29 | 1.13E-05 | 3.85E-06 | 5.04E-06 |
| | R-38 | 0.3 – 0.49 | 5.78E-05 | 1.97E-05 | 2.58E-05 |
| | R-38 | 0.5 – 0.69 | 1.06E-04 | 3.63E-05 | 4.75E-05 |

| HVAC Type | Roof Deck Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|------------------------------------|--|----------|----------|----------|
| | R-38 | ≥ 0.7 | 1.57E-04 | 5.38E-05 | 7.04E-05 |
| Low Slope | | | | | |
| AC + Gas | R-19 | 0.5 – 0.69 | 7.71E-04 | 8.74E-05 | 1.44E-04 |
| | R-19 | ≥ 0.7 | 1.14E-03 | 1.30E-04 | 2.14E-04 |
| | R-30 | 0.5 – 0.69 | 5.55E-04 | 7.58E-05 | 8.80E-05 |
| | R-30 | ≥ 0.7 | 8.22E-04 | 1.12E-04 | 1.30E-04 |
| | R-38 | 0.5 – 0.69 | 3.98E-04 | 6.74E-05 | 4.72E-05 |
| | R-38 | ≥ 0.7 | 5.89E-04 | 9.98E-05 | 6.98E-05 |
| Steep Slope | | | | | |
| AC + ER | R-19 | 0.15 - 0.29 | 5.05E-05 | 1.12E-05 | 1.69E-05 |
| | R-19 | 0.3 – 0.49 | 2.60E-04 | 5.74E-05 | 8.71E-05 |
| | R-19 | 0.5 – 0.69 | 4.73E-04 | 1.05E-04 | 1.59E-04 |
| | R-19 | ≥ 0.7 | 6.98E-04 | 1.54E-04 | 2.34E-04 |
| | R-30 | 0.15 - 0.29 | 4.67E-05 | 9.17E-06 | 1.12E-05 |
| | R-30 | 0.3 – 0.49 | 2.44E-04 | 4.77E-05 | 5.81E-05 |
| | R-30 | 0.5 – 0.69 | 4.45E-04 | 8.72E-05 | 1.06E-04 |
| | R-30 | ≥ 0.7 | 6.57E-04 | 1.29E-04 | 1.56E-04 |
| | R-38 | 0.15 - 0.29 | 4.39E-05 | 7.72E-06 | 7.00E-06 |
| | R-38 | 0.3 – 0.49 | 2.32E-04 | 4.07E-05 | 3.70E-05 |
| | R-38 | 0.5 – 0.69 | 4.24E-04 | 7.45E-05 | 6.76E-05 |
| | R-38 | ≥ 0.7 | 6.28E-04 | 1.10E-04 | 1.00E-04 |
| Low Slope | | | | | |
| AC + ER | R-19 | 0.5 – 0.69 | 4.34E-04 | 8.79E-05 | 1.46E-04 |
| | R-19 | ≥ 0.7 | 6.39E-04 | 1.29E-04 | 2.15E-04 |
| | R-30 | 0.5 – 0.69 | 3.39E-04 | 6.50E-05 | 9.74E-05 |
| | R-30 | ≥ 0.7 | 5.01E-04 | 9.59E-05 | 1.44E-04 |
| | R-38 | 0.5 – 0.69 | 2.70E-04 | 4.84E-05 | 6.18E-05 |
| | R-38 | ≥ 0.7 | 4.00E-04 | 7.16E-05 | 9.14E-05 |
| Steep Slope | | | | | |
| HP | R-19 | 0.15 - 0.29 | 2.04E-05 | 1.40E-05 | 1.64E-05 |
| | R-19 | 0.3 – 0.49 | 1.05E-04 | 7.18E-05 | 8.39E-05 |
| | R-19 | 0.5 – 0.69 | 1.92E-04 | 1.32E-04 | 1.54E-04 |
| | R-19 | ≥ 0.7 | 2.85E-04 | 1.96E-04 | 2.28E-04 |

| HVAC Type | Roof Deck Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-------------|------------------------------------|--|----------|----------|----------|
| | R-30 | 0.15 - 0.29 | 1.67E-05 | 8.15E-06 | 9.60E-06 |
| | R-30 | 0.3 – 0.49 | 8.56E-05 | 4.18E-05 | 4.93E-05 |
| | R-30 | 0.5 – 0.69 | 1.57E-04 | 7.68E-05 | 9.05E-05 |
| | R-30 | ≥ 0.7 | 2.33E-04 | 1.14E-04 | 1.34E-04 |
| | R-38 | 0.15 - 0.29 | 1.40E-05 | 3.88E-06 | 4.68E-06 |
| | R-38 | 0.3 – 0.49 | 7.19E-05 | 2.00E-05 | 2.41E-05 |
| | R-38 | 0.5 – 0.69 | 1.32E-04 | 3.66E-05 | 4.41E-05 |
| | R-38 | ≥ 0.7 | 1.95E-04 | 5.41E-05 | 6.52E-05 |
| Low Slope | | | | | |
| HP | R-19 | 0.5 – 0.69 | 1.77E-04 | 1.24E-04 | 1.44E-04 |
| | R-19 | ≥ 0.7 | 2.63E-04 | 1.84E-04 | 2.12E-04 |
| | R-30 | 0.5 – 0.69 | 1.77E-04 | 7.30E-05 | 8.46E-05 |
| | R-30 | ≥ 0.7 | 2.61E-04 | 1.08E-04 | 1.25E-04 |
| | R-38 | 0.5 – 0.69 | 1.76E-04 | 3.57E-05 | 4.18E-05 |
| | R-38 | ≥ 0.7 | 2.60E-04 | 5.28E-05 | 6.18E-05 |
| Steep Slope | | | | | |
| AC no heat | R-19 | 0.15 - 0.29 | 2.28E-05 | 1.89E-05 | 1.72E-05 |
| | R-19 | 0.3 – 0.49 | 1.16E-04 | 9.64E-05 | 8.77E-05 |
| | R-19 | 0.5 – 0.69 | 2.15E-04 | 1.78E-04 | 1.62E-04 |
| | R-19 | ≥ 0.7 | 3.18E-04 | 2.63E-04 | 2.40E-04 |
| | R-30 | 0.15 - 0.29 | 1.85E-05 | 1.53E-05 | 1.40E-05 |
| | R-30 | 0.3 – 0.49 | 9.48E-05 | 7.84E-05 | 7.15E-05 |
| | R-30 | 0.5 – 0.69 | 1.75E-04 | 1.44E-04 | 1.32E-04 |
| | R-30 | ≥ 0.7 | 2.59E-04 | 2.14E-04 | 1.95E-04 |
| | R-38 | 0.15 - 0.29 | 1.54E-05 | 1.27E-05 | 1.17E-05 |
| | R-38 | 0.3 – 0.49 | 7.91E-05 | 6.53E-05 | 5.97E-05 |
| | R-38 | 0.5 – 0.69 | 1.46E-04 | 1.20E-04 | 1.10E-04 |
| | R-38 | ≥ 0.7 | 2.15E-04 | 1.78E-04 | 1.63E-04 |
| Low Slope | | | | | |
| AC no heat | R-19 | 0.5 – 0.69 | 1.80E-04 | 1.54E-04 | 1.45E-04 |
| | R-19 | ≥ 0.7 | 2.67E-04 | 2.29E-04 | 2.14E-04 |
| | R-30 | 0.5 – 0.69 | 1.47E-04 | 1.26E-04 | 1.17E-04 |
| | R-30 | ≥ 0.7 | 2.18E-04 | 1.86E-04 | 1.74E-04 |

| HVAC Type | Roof Deck Insulation R-value | Installed Roof Material 3-Year Reflectance | NCP | CP | 4CP |
|-----------|------------------------------|--|----------|----------|----------|
| | R-38 | 0.5 – 0.69 | 1.23E-04 | 1.05E-04 | 9.73E-05 |
| | R-38 | ≥ 0.7 | 1.83E-04 | 1.55E-04 | 1.44E-04 |

6.6.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID BS-LtRoof.²²⁸

6.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- R-value of insulation (as is, post measure installation of ceiling/roof insulation)
- For homes with a reported baseline R-value that is less than R-5:
 - Two pictures: (1) a picture showing the entire attic floor, and (2) a close-up picture of a ruler that shows the measurement of the depth of the insulation
 - Note: The second photo type is required for each area of insulation where there are varying R-values less than R-5. Additionally, both photo types are required for all separate attic/ceiling areas, even when the installed R-value is the same
- Cooling type (central refrigerated cooling, room air conditioner, none)
- Heating type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
 - Because heating savings are negative, no adjustment factor will be applied to projects with missing documentation
- Square footage of reflective roofing material installed
- Slope of the roof (low or high)
- Three-year solar reflectance as rated by Cool Roof Rating Certification of the reflective

²²⁸ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

material installed

- Proof of purchase with date of purchase, quantity, model number, and treated square feet
 - Alternative: photo of unit installed or another pre-approved method of installation verification

Document Revision History

Table 6.6-7: [Cool Roofs] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

6.7 SOLAR SCREENS

6.7.1 Measure Description

Savings are presented for the installation of solar screens on west- and/or south-facing windows or glass doors. Deemed savings are calculated per square foot of treated window or door opening.

6.7.1.1 Eligibility Criteria

Cooling savings in this measure apply to customers with central or mini-split electric refrigerated air conditioning in their homes. The heating savings penalty applies to homes that are centrally heated with either a furnace (gas or electric resistance) or a heat pump. Customers who participate in hard-to-reach (HTR) or low-income (LI) programs are eligible to claim reduced heating savings for homes heated with gas or electric resistance space heaters by applying an adjustment to deemed savings that is specified for that heat type. Customers participating in HTR or LI programs are also eligible to claim reduced cooling savings for homes cooled by one or more room air conditioners by applying an adjustment to deemed savings that is specified for homes with central refrigerated air.

Solar screens must be installed on windows or glass doors that face west or south and receive significant direct sun exposure. Solar screens must block at least 65 percent of the solar heat gain to qualify for deemed savings.

6.7.1.2 Baseline Condition

The baseline is a single pane, clear glass, unshaded, west- or south-facing window with a solar heat gain coefficient of 0.68. The baseline window area is assumed to be 7.5 percent of the total wall area.

Electric resistance heating baselines may refer to residences heated by a centralized forced-air furnace or by individual space heaters.²²⁹ Space heating refers primarily to electric baseboard zonal heaters controlled by thermostats or to portable plug-load heaters.²³⁰ Electric resistance heat controlled by a wall thermostat is eligible to claim the deemed savings presented in this measure. Homes with portable space heaters may be eligible for reduced savings as described in the Deemed Energy and Demand Savings Tables sections.

6.7.1.3 High-Efficiency Condition

Solar screens are installed on the west- or south-facing windows must reduce solar heat gain by at least 65 percent. Solar screens are not recommended for homes with electric resistance heat.

²²⁹ Electric Resistance Heating: <https://www.energy.gov/energysaver/home-heating-systems/electric-resistance-heating>.

²³⁰ Portable Heaters: <https://www.energy.gov/energysaver/home-heating-systems/portable-heaters>.

6.7.2 Energy and Demand Savings Methodology

6.7.2.1 Savings Algorithms and Input Variables

Deemed savings values have been estimated using calibrated simulation models. Specifically, these deemed savings estimates were developed by using NREL's BEopt 2.6 software, running EnergyPlus 8.4 as the underlying simulation engine. A single modification was made to the prototype models for the different HVAC types to create the base case models for estimating savings for the solar screens measure. Windows facing all directions are assumed to be single-pane windows with U-Values of 1.16 BTU/h-ft²-R and Solar Heat Gain Coefficients (SHGC) of 0.76.

For the change case models, an 80 percent reduction was applied to the solar heat gain coefficient and a 10 percent reduction was applied to the U-value for the treated windows.

Coincident peak demand savings are estimated by taking the difference in demand for the 20 hours identified from the TMY3 datasets in which the peak demand is most likely to occur. Non-coincident peak demand savings (NCP) are set by the single hour in which the base case model energy use most exceeds that of the change case model. ERCOT 4 CP demand savings are estimated by extracting the modeled demand difference in the hour ending 5 PM for all weekdays in each month and taking the 90th percentile of the differences in each month.

The model assumes the average solar screen installed blocks 80% of the solar heat gain attributed to the treated windows based on performance data from solar screens analyzed at sun angles of 30, 45 and 75 degrees to the window.²³¹

While it is strongly recommended that solar screens be removed during winter to allow the advantage of free heat from the sun, often they are not removed seasonally. This practice may be because of solar screens serving as an insect screen in addition to blocking the sun or simply that they're installed in difficult-to-reach areas such as second floor windows. The savings estimates presented herein assume that the installed solar screens remain in place year-round.

Thermal Performance Improvement

Manual J and other studies researched indicate a thermal improvement to a window with a solar screen due to reduced air infiltration. The National Certified Testing Laboratories provided a report stating a 15 percent reduction in the thermal transmittance of a single pane, ¼" clear glass window with a solar screen added to the exterior.

Another study that was conducted for NFRC indicated between a 22 percent and 4 percent improvement to the U-value of a window with a solar screen. A single pane, clear window has a 22 percent improvement with the addition of a solar screen, whereas a double pane, spectrally selective low-E window may only have a 4 percent improvement. The deemed savings models assume an average

²³¹ Performance data from Matrix, Inc., Mesa, Arizona testing facility for Phifer Wire Products' SunTex screen, blocks 80% of solar heat gain. <https://www.phifer.com/product/suntex-80-90/>.

10 percent improvement in thermal performance with the addition of a solar screen.

Window Frame

The window frame accounts for 10-30 percent of the window area²³² and because it is opaque and blocks sunlight from entering the home, it is factored into the model. An average of 15 percent frame area was incorporated into the performance of the window.

Energy Savings

Energy savings are estimated according to the differences in annual energy use in the pre-retrofit (base case) and post-retrofit (change case) models. Estimated savings per square foot of solar screen installed are presented by window orientation in the deemed energy savings tables below. The energy savings are additive: if windows are installed on multiple orientations, the sum of the cooling savings and appropriate heating savings values for each orientation in Table 6.7-1 should be multiplied by the square feet of treated window area in that orientation. The resulting values should be summed to estimate total energy savings.

Demand Savings

Coincident Peak (CP), Non-coincident Peak (NCP) and ERCOT 4 Coincident Peak (4 CP) demand savings are estimated in accordance with the definitions provided in Section 2.3 of this document. All are estimated according to the differences in energy use in specific hours of the simulations of the pre-retrofit (base case) and post-retrofit (change case) models.

Non-coincident Peak (NCP) savings for installations with individual orientations are calculated exactly as in Section 2.3, by taking the 99.9th percentile value from the 8,760 hourly savings values in the delta load shape. NCP savings for projects with multiple treated fenestration orientations are estimated differently. First, the absolute maximum NCP interval is identified by analyzing the delta load shape from a simulation model run representing the completed project with two or three treated orientations. For each treated orientation, the hourly savings value is extracted and normalized to the model treated window area for that orientation. These normalized values are then summed to obtain the NCP demand savings.

Similarly, CP and 4 CP demand savings for installations on multiple orientations are estimated by summing the normalized CP and 4 CP demand savings estimated for each orientation.

Estimated savings per square foot of solar screen installed are presented in the deemed demand savings tables below. Demand savings are presented for installations on individual window orientations and for installations on combinations of window orientations. The demand savings presented in Table 6.7-3 are not additive.

²³² Residential Windows – A Guide to New Technologies and Energy Performance, 2000.

6.7.2.2 Deemed Energy Savings Tables

Table 6.7-1 presents the cooling and heating energy savings (kWh) achieved per square foot of ceiling area beneath the encapsulated attic in CPS Energy’s service territory. Annual energy savings are the sum of the cooling savings and the heating savings for the appropriate heating equipment type.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.7-1 by a factor of 0.6. Similarly, for HTR/LI customers, heating savings may be claimed for homes with electric resistance space heaters serving as the primary heating source by multiplying heating savings in Table 6.7-1 by a factor of 0.24.²³³

$$\text{Energy Savings } [\Delta kWh] = (\text{Savings}/ft^2_c \times CAF + \text{Savings}/ft^2_H \times HAF) \times A$$

Equation 6.7-1

Where:

Savings/ft² = Deemed cooling and heating energy savings per square feet; see Table 6.7-1.

A = Solar screen area [ft²].

CAF = Cooling adjustment factor in Table 6.7-2.

HAF = Heating adjustment factor in Table 6.7-2.

Table 6.7-1: [Solar Screens] Deemed Energy Savings per Installed Square Foot (kWh/sq. ft.)

| Window Orientation Treated | Cooling Savings | Heating Savings by Primary Heat Source | | |
|----------------------------|-----------------|--|---------------------|-----------|
| | | Gas | Electric Resistance | Heat Pump |
| East | 10.72 | -0.20 | -5.90 | -2.10 |
| South | 7.67 | -0.25 | -8.04 | -3.07 |
| West | 12.48 | -0.17 | -4.95 | -1.77 |

²³³ This factor was derived based on expected capacity reduction assuming 1200 sqft (historical analysis of HTR participants) x 0.35 BTU/sqft = 42,000 BTU for central electric furnaces and two 1,500-watt portable heaters per home rated at 5,100 BTU/heater. Taking the ratio of portable to furnace capacity yields 10,200 ÷ 42,000 = 0.24.

Table 6.7-2: [Solar Screens] CAF/HAF, Cooling & Heating Adjustment Factors

| HVAC System Type | CAF | HAF |
|----------------------------------|------|------|
| Central AC | 1.00 | - |
| Window or Room AC | 0.60 | - |
| Central Furnace or HP | - | 1.00 |
| Electric Resistance Space Heater | - | 0.24 |
| None | - | - |

6.7.2.3 Deemed Demand Savings Tables

Table 6.7-3 presents the deemed peak demand savings value per square foot of solar screen installed.

For customers who participate in Hard-to-Reach (HTR) or Low Income (LI) programs, cooling savings may be claimed for homes cooled by one or more room air conditioners by multiplying cooling savings in Table 6.7-3 by a factor of 0.6.

$$\text{Demand Savings } [\Delta kW] = \text{Savings}/ft^2 \times AF \times A$$

Equation 6.7-2

Where:

$\text{Savings}/ft^2$ = Deemed NCP, CP, or 4CP demand savings per square feet; see Table 6.7-3.

AF = Adjustment factor based on HVAC system type in Table 6.7-4.

Table 6.7-3: [Solar Screens] Deemed Demand Savings per Installed Square Foot (kW/sq. ft.)

| Window Orientation Treated | NCP by Primary Heat Source | | | CP | 4CP |
|----------------------------|----------------------------|------------------------|------------------------|------------------------|------------------------|
| | Gas | Electric Resistance | Heat Pump | | |
| East | 8.92×10^{-03} | 7.17×10^{-03} | 7.17×10^{-03} | 2.49×10^{-03} | 1.93×10^{-03} |
| South | 9.74×10^{-03} | 8.41×10^{-03} | 8.40×10^{-03} | 1.73×10^{-03} | 1.78×10^{-03} |
| West | 1.39×10^{-02} | 7.15×10^{-03} | 7.25×10^{-03} | 6.29×10^{-03} | 6.96×10^{-03} |
| East and West | 1.91×10^{-02} | 9.98×10^{-03} | 9.80×10^{-03} | 8.78×10^{-03} | 9.41×10^{-03} |
| South and West | 1.80×10^{-02} | 9.12×10^{-03} | 9.60×10^{-03} | 8.02×10^{-03} | 9.22×10^{-03} |
| West, South and East | 2.89×10^{-02} | 1.46×10^{-02} | 1.54×10^{-02} | 1.05×10^{-02} | 1.07×10^{-02} |

Table 6.7-4: [Solar Screens] AF, Adjustment Factors

| Cooling System Type | NCP Adjustment Factor by Primary Heat Source | | | | CP and 4CP Adjustment Factor by Primary Heat Source | | | |
|---------------------|--|-----|-----|------|---|-----|-----|------|
| | Gas | ER | HP | None | Gas | ER | HP | None |
| Central AC | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Window or Room AC | 0.6 | 1.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| None | - | 1.0 | - | - | - | - | - | - |

6.7.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for solar screens, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID BS-WinFilm.²³⁴

6.7.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Cooling type (central refrigerated cooling, room air conditioner, none)
- Heating type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach); sampling is allowed for multifamily complexes
 - Because heating savings are negative, no adjustment factor will be applied to projects with missing documentation
- Square footage of windows or door openings treated
- Proof of purchase with date of purchase, quantity, and model number
 - Alternative: photo of unit installed or other pre-approved method of installation verification

²³⁴ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 6.7-5: [Solar Screens] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

7. RESIDENTIAL: WATER HEATING

7.1 ELECTRIC TANKLESS WATER HEATER REPLACEMENTS

7.1.1 Measure Description

This measure involves installing a new electric tankless²³⁵ water heater in place of an electric storage water heater.

7.1.1.1 Eligibility Criteria

This measure involves installing an electric instantaneous (tankless) water heater in place of an electric storage water heater that meets all the additional requirements described below. Currently, there are no conventional, electrically fueled storage units that sufficiently exceed the new federal standard to merit inclusion as an efficient condition in these deemed savings.

Savings may be awarded for installations in newly constructed homes where customer and utility representatives provide written indication that an electric storage water heater would otherwise have been installed, along with relevant design documentation showing an electric storage water heater.

7.1.1.2 Baseline Condition

The baseline condition is an electric storage water heater with baseline efficiency Uniform Energy Factor (UEF) determined by tank size and first hour rating (FHR), a proxy for draw pattern. This baseline is specified according to the current federal energy efficiency standards for residential water heaters with tank sizes from 20 to 120 gallons, effective April 16, 2015, as published in 10 CFR Part 430.32 of the Federal Register (see Table 7.1-1).²³⁶

The baseline applies to replace-on-burnout and new construction applications. No additional savings are awarded for early retirement. Early retirement projects should calculate savings using an assumed replace-on-burnout baseline.

²³⁵ Currently, most electric tankless water heaters are rated at or near the federal standard and may yield negative or no energy savings using the current baseline. However, this measure maintains eligibility for any electric tankless water heaters that may be rated above current minimum efficiency requirements.

²³⁶ 10 CFR Part 430.32 Energy and water conservation standards and their effective dates.
https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=32.

Table 7.1-1: [Tankless DHW] Federal Standard for Residential Electric Storage Water Heaters

| Rated Storage Volume | Draw Pattern | FHR ^{237,238} | UEF ²³⁹ |
|------------------------|--------------|---------------------------|--------------------------------|
| ≥ 20 gal and ≤ 55 gal | Very small | $0 \leq \text{FHR} < 18$ | $0.8808 - (0.0008 \times V_r)$ |
| | Low | $18 \leq \text{FHR} < 51$ | $0.9254 - (0.0003 \times V_r)$ |
| | Medium | $51 \leq \text{FHR} < 75$ | $0.9307 - (0.0002 \times V_r)$ |
| | High | $75 \leq \text{FHR}$ | $0.9349 - (0.0001 \times V_r)$ |
| > 55 gal and ≤ 120 gal | Very small | $0 \leq \text{FHR} < 18$ | $1.9236 - (0.0011 \times V_r)$ |
| | Low | $18 \leq \text{FHR} < 51$ | $2.0440 - (0.0011 \times V_r)$ |
| | Medium | $51 \leq \text{FHR} < 75$ | $2.1171 - (0.0011 \times V_r)$ |
| | High | $75 \leq \text{FHR}$ | $2.2418 - (0.0011 \times V_r)$ |

7.1.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v5.0 specification effective April 18, 2023, with qualified products meeting the minimum requirements from Table 7.1-2.²⁴⁰

However, the ENERGY STAR specification does not cover electric tankless water heaters with an FHR less than 51. In these cases, the high efficiency condition corresponds to the respective federal standards for residential water heaters.²⁴¹ Table 7.1-2 has consolidated both sources in one location for ease of reference.

For water heater replacement, the new unit must meet the following federal minimum energy factor shown in Table 7.1-2. Water heaters must be installed in accordance with local code requirements.

FHR does not apply to tankless water heaters, which are rated in terms of max gallons per minute (GPM).

²³⁷ "The Revised Method of Test for Residential Water Heating and Its Impact on Incentive Programs" presentation, Glanville, Paul. ACEEE Hot Water Forum. February 24, 2015. <https://aceee.org/sites/default/files/pdf/conferences/hwf/2015/6B-Glanville.pdf>.

²³⁸ Assume FHR equal to that of installed water heater.

²³⁹ V_r is the Rated Storage Volume (in gallons), as determined pursuant to 10 CFR 429.17.

²⁴⁰ ENERGY STAR v5.0 Program Requirements for Residential Water Heaters.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Residential%20Water%20Heaters%20Version%205.0%20Specification%20and%20Partner%20Commitments_0.pdf.

²⁴¹ 10 CFR Part 430.32 Energy and water conservation standards and their effective dates.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=32.

Table 7.1-2: [Tankless DHW] Federal Standard for Residential Electric Storage Water Heaters

| DHW type | Rated Storage Volume | Draw Pattern | FHR | UEF |
|----------------------------------|----------------------|--------------|-----|------|
| Electric tankless ²⁴² | < 2 gal | Very small | N/A | 0.91 |
| | | Low | | 0.91 |
| | | Medium | | 0.91 |
| | | High | | 0.92 |

7.1.2 Energy and Demand Savings Methodology

7.1.2.1 Savings Algorithms and Input Variables

All deemed savings values are calculated using the following standard algorithms for water heating. These algorithms assume a replace-on-burnout or new construction scenario but may be used to award savings for early retirement projects.

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = \frac{\rho \times C_p \times GPY \times (T_{SP} - T_{supply,annual}) \times \left(\frac{1}{UEF_{pre}} - \frac{1}{UEF_{post}} \right)}{3,412}$$

Equation 7.1-1

Where:

| | | |
|--------|---|--|
| ρ | = | Water density = 8.33 lbs/gallons. |
| C_p | = | Specific heat of water = 1 Btu/lb·°F. |
| GPY | = | Estimated annual hot water use in gallons/year; specified by number of bedrooms in the home; see Table 7.1-3. For midstream/upstream applications, the number of bedrooms is assumed to be 3. ²⁴³ |

Table 7.1-3: [Tankless DHW] Water Heater Consumption (gal/year)²⁴⁴

| Number of Bedrooms | | | |
|--------------------|--------|--------|--------|
| 1 | 2 | 3 | 4 |
| 13,924 | 17,018 | 20,112 | 23,206 |

²⁴² There is no ENERGY STAR tankless water heater category because all products perform at or near the federal standard. These units are still eligible to claim savings against the electric storage water heater baseline if FHR and UEF can be verified using manufacturer specification sheets or other documentation.

²⁴³ Weighted average of number of bedrooms in West South-Central Region. 2020 RECS Survey Data – Table HC2.8 Structural and geographic characteristics of homes in the South and West regions, 2020. <https://www.eia.gov/consumption/residential/data/2020/>.

²⁴⁴ Building America Research Benchmark Definition. December 2009. Available online: <http://www.nrel.gov/docs/fy10osti/47246.pdf>.

| | | |
|---------------------|---|--|
| T_{SP} | = | Water heater set point = 120°F. ²⁴⁵ |
| $T_{supply,annual}$ | = | Average supply water temperature = 75.9°F. ²⁴⁶ |
| UEF_{pre} | = | Baseline uniform energy factor Table 7.1-1. ²⁴⁷ |
| UEF_{post} | = | Uniform energy factor of new water heater (must meet or exceed values from Table 7.1-2). |
| 3,412 | = | Constant to convert from Btu to kWh. |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = DF \times \frac{\rho \times C_p \times GPY \times (T_{SP} - T_{supply,summer}) \times \left(\frac{1}{UEF_{pre}} - \frac{1}{UEF_{post}} \right)}{365 \times 3,412}$$

Equation 7.1-2

Where:

| | | |
|---------------------|---|--|
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 7.1-4. |
| $T_{supply,summer}$ | = | For NCP, use average supply water temperature, 75.9°F ²⁴⁸ ; for CP and 4CP, use summer supply water temperature 85.41°F. ²⁴⁹ |

Table 7.1-4: [Tankless DHW] Demand Factors²⁵⁰

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

7.1.2.2 Deemed Energy Savings Tables

There are no deemed energy savings tables for this measure. Please see the algorithms above.

²⁴⁵ The data collection discussed in Appendix D of the Texas EM&V team's Annual Statewide Portfolio Report for Program Year 2014-Volume 1, Project Number 40891 (August 2015) supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

²⁴⁶ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

²⁴⁷ Note that for efficient water heater installations in residential new construction, the baseline energy factor is the efficiency of the electric storage water heater that would otherwise have been installed, according to appropriate design documentation.

²⁴⁸ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

²⁴⁹ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, August, and September.

²⁵⁰ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

7.1.2.3 Deemed Demand Savings Tables

There are no deemed demand savings tables for this measure. Please see the algorithms above.

7.1.2.4 Measure Life and Lifetime Savings

The Estimated Useful Life (EUL) is 20 years for an electric tankless water heater, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-Instant-Res.²⁵¹

7.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Number of bedrooms (not required for upstream/midstream program delivery)
- Water heater quantity
- Manufacturer and model number of new water heater
- Baseline volume (gallons), FHR, and UEF
- New water heater volume (gallons, zero if tankless), FHR, and UEF
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

Document Revision History

Table 7.1-5: [Tankless DHW] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Removed requirement to install HPWH for DHW > 55 gallons. Incorporated updated ENERGY STAR specification v5.0. Updated documentation requirements. |
| FY 2026 | No revision. |

²⁵¹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

7.2 ENERGY STAR® HEAT PUMP WATER HEATERS

7.2.1 Measure Description

This measure involves the installation of an ENERGY STAR-compliant heat pump water heater (HPWH). Note that this measure does not account for the interactive air conditioning energy savings and heating penalty associated with the HPWH when installed inside conditioned space.

7.2.1.1 Eligibility Criteria

This measure applies to residential, electric, storage-type heat pump water heaters. Heat pump add-ons to existing storage water heaters are ineligible. The measure does not apply to the replacement of gas water heaters.

First hour rating (FHR) is a proxy for draw pattern. There are no certified ENERGY STAR water heaters in the very small usage category, and that draw pattern is not covered in the current ENERGY STAR specification. Approximately 94 percent of certified units are in the medium and high usage categories. However, HPWHs with low usage draw patterns are eligible as long as they comply with minimum ENERGY STAR FHR requirements.

7.2.1.2 Baseline Condition

The baseline condition is an electric storage water heater (EWH) with baseline efficiency Uniform Energy Factor (UEF) determined by tank size and first hour rating (FHR). This baseline is specified according to the current federal energy efficiency standards for residential water heaters with tank sizes 20 to 120 gallons, effective April 16, 2015, as published in 10 CFR Part 430.32 of the Federal Register.²⁵²

This baseline applies to replace-on-burnout and new construction applications. No additional savings are awarded for early retirement at this time. Early retirement projects should calculate savings using an assumed replace-on-burnout baseline. However, the Department of Energy (DOE) issued an updated final rule for consumer water heaters effective July 5, 2024.²⁵³ Compliance with the new federal standard will be enforced as of May 6, 2029. The Guidebook will add an early retirement baseline after the effective date for the new standard.

²⁵² 10 CFR Part 430.32 Energy and water conservation standards and their effective dates. www.ecfr.gov/cgi-bin/textidx?SID=80dfa785ea350ebee184bb0ae03e7f0&mc=true&node=se10.3.430_132&rgn=div8.

²⁵³ Energy Conservation Program: Energy Conservation Standards for Consumer Water Heaters. <https://www.regulations.gov/document/EERE-2017-BT-STD-0019-0063>.

Table 7.2-1: [HPWHs] Federal Standard for Residential Water Heaters

| Rated Storage Volume | Draw Pattern | FHR ^{254 255} | UEF ²⁵⁶ |
|------------------------|------------------|---------------------------|--------------------------------|
| ≥ 20 gal and ≤ 55 gal | Very Small Usage | $0 \leq \text{FHR} < 18$ | $0.8808 - (0.0008 \times V_r)$ |
| | Low Usage | $18 \leq \text{FHR} < 51$ | $0.9254 - (0.0003 \times V_r)$ |
| | Medium Usage | $51 \leq \text{FHR} < 75$ | $0.9307 - (0.0002 \times V_r)$ |
| | High Usage | $75 \leq \text{FHR}$ | $0.9349 - (0.0001 \times V_r)$ |
| > 55 gal and ≤ 120 gal | Very Small Usage | $0 \leq \text{FHR} < 18$ | $1.9236 - (0.0011 \times V_r)$ |
| | Low Usage | $18 \leq \text{FHR} < 51$ | $2.0440 - (0.0011 \times V_r)$ |
| | Medium Usage | $51 \leq \text{FHR} < 75$ | $2.1171 - (0.0011 \times V_r)$ |
| | High Usage | $75 \leq \text{FHR}$ | $2.2418 - (0.0011 \times V_r)$ |

7.2.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v5.0 specification, effective April 18, 2023. Qualified products must meet the minimum requirements from Table 7.2-2.²⁵⁷

Table 7.2-2: [HPWHs] ENERGY STAR Specification

| Criteria | ENERGY STAR Requirement |
|---|--|
| Integrated HPWH | UEF ≥ 3.30 |
| Integrated HPWH, 120 volt/15 amp circuit | UEF ≥ 2.20 |
| Split-system HPWHT | UEF ≥ 2.20 |
| First-hour rating | FHR ≥ 45 gallons per hour |
| Warranty | Warranty ≥ 6 years on sealed system |
| Safety | UL 174 and UL 1995 or UL 60335-2-40 |
| Lower compressor cut-off temperature (reporting requirement only) | Report ambient temperature below which the compressor cuts off and electric-resistance-only operation begins |

A complete list of certified ENERGY STAR HPWHs can be accessed via the ENERGY STAR program website.²⁵⁸

²⁵⁴ “The Revised Method of Test for Residential Water Heating and Its Impact on Incentive Programs” presentation, Glanville, Paul. ACEEE Hot Water Forum. February 24, 2015. <https://aceee.org/sites/default/files/pdf/conferences/hwf/2015/6B-Glanville.pdf>.

²⁵⁵ Assume FHR equal to that of installed water heater.

²⁵⁶ V_r is the Rated Storage Volume (in gallons), as determined pursuant to 10 CFR 429.17.

²⁵⁷ ENERGY STAR HPWH Program Requirements for Residential Water Heaters.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Residential%20Water%20Heaters%20Version%205.0%20Specification%20and%20Partner%20Commitments_0.pdf.

²⁵⁸ ENERGY STAR Certified Water Heaters qualified product listing. <https://www.energystar.gov/productfinder/product/certified-heat-pump-water-heaters/results>.

HPWHs depend on adequate ventilation for proper functioning, including adequate space for both inlet and outlet air flow, and should be installed in spaces in which temperature does not drop below a certain level. The Department of Energy recommends installation in locations that remain above 40°F year-round and provide a minimum of 1,000 cubic feet of air space around the water heater.²⁵⁹ Modern HPWHs operate with little to no change in performance with considerably less air volume. Updated recommendations reduce the air volume requirement to 700 cubic feet.²⁶⁰ These conditions are not enforced as an eligibility requirement but should be considered when installing an HPWH.

7.2.2 Energy and Demand Savings Methodology

7.2.2.1 Savings Algorithms and Input Variables

HPWH savings are calculated on a per-unit basis. Deemed savings are calculated utilizing the standard algorithms outlined below for water heating. Consumption in gallons per year is estimated using data from Building America Performance Analysis Procedures for Existing Homes.²⁶¹ Temperature data are based on TMY3 dataset.²⁶²

For upstream/midstream program delivery, a default of three bedrooms may be used to calculate the annual hot water use in gallons per year (GPY). The default number of bedrooms was estimated by taking the weighted average calculated from 2020 RECS Survey Data.

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = \frac{\rho \times C_p \times GPY \times (T_{SP} - T_{supply,annual}) \times \left(\frac{1}{UEF_{pre}} - \frac{1}{UEF_{post}} \right)}{3,412}$$

Equation 7.2-1

Where:

| | | |
|--------|---|--|
| ρ | = | Water density = 8.33 lbs/gallons. |
| C_p | = | Specific heat of water = 1 Btu/lb·°F. |
| GPY | = | Estimated annual hot water use in gallons/year, specified by number of bedrooms in the home; see Table 7.2-3. For midstream/upstream applications, the number of bedrooms is assumed to be 3. ²⁶³ |

²⁵⁹ Heat Pump Water Heaters. Department of Energy, May 2012. <http://energy.gov/energysaver/articles/heat-pump-water-heaters>.

²⁶⁰ Heat Pump Water Heaters – Code Compliance Brief, U.S. Department of Energy Building Technologies Office. <https://basc.pnnl.gov/code-compliance/heat-pump-water-heaters-code-compliance-brief>.

²⁶¹ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

²⁶² TMY data is available through the National Solar Radiation Database (NSRDB) Data Viewer, <https://maps.nrel.gov/nsrdb-viewer/>. Data for Texas climate zones can also be accessed directly here: <https://texasefficiency.com/index.php/regulatory-filings/deemed-savings>.

²⁶³ Weighted Average of number of bedrooms in West South Central Region. 2020 RECS Survey Data – Table HC2.8 Structural and geographic characteristics of homes in the South and West regions, 2020. <https://www.eia.gov/consumption/residential/data/2020/>.

Table 7.2-3: [HPWHs] Water Heater Consumption (Gal/Year)²⁶⁴

| Number of Bedrooms | | | |
|--------------------|--------|--------|--------|
| 1 | 2 | 3 | 4 |
| 13,924 | 17,018 | 20,112 | 23,206 |

| | | |
|---------------------|---|--|
| T_{SP} | = | Water heater set point = 120°F. ²⁶⁵ |
| $T_{supply,annual}$ | = | Average supply water temperature = 75.9°F. ²⁶⁶ |
| UEF_{pre} | = | Baseline uniform energy factor Table 7.1-1. ²⁶⁷ |
| UEF_{post} | = | Uniform energy factor of new water heater (must exceed values from Table 7.2-2). |
| 3,412 | = | Constant to convert from Btu to kWh. |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{\rho \times C_p \times GPY \times (T_{SP} - T_{supply,summer}) \times \left(\frac{1}{UEF_{pre}} - \frac{1}{UEF_{post}} \right)}{365 \times 3,412} \times CF_{S/W}$$

Equation 7.2-2

Where:

| | | |
|---------------------|---|--|
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 7.2-4. |
| $T_{supply,summer}$ | = | For NCP, use average supply water temperature, 75.9°F ²⁶⁸ ; for CP and 4CP, use summer supply water temperature 85.41°F. ²⁶⁹ |

Table 7.2-4: [HPWH] Demand Factors²⁷⁰

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

²⁶⁴ Building America Research Benchmark Definition. December 2009, p 13. Available online: <http://www.nrel.gov/docs/fy10osti/47246.pdf>.

²⁶⁵ The data collection discussed in Appendix D of the Texas EM&V team's Annual Statewide Portfolio Report for Program Year 2014-Volume 1, Project Number 40891 (August 2015) supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

²⁶⁶ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

²⁶⁷ Note that for efficient water heater installations in residential new construction, the baseline energy factor is the efficiency of the electric storage water heater that would otherwise have been installed, according to appropriate design documentation.

²⁶⁸ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

²⁶⁹ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, August, and September.

²⁷⁰ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

7.2.2.2 Deemed Energy Savings Tables

There are no deemed energy savings tables for this measure. Please see the algorithms above.

7.2.2.3 Deemed Demand Savings Tables

There are no deemed demand savings tables for this measure. Please see the algorithms above.

7.2.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 13 years for HPWHs.²⁷¹

7.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Number of bedrooms (not required for upstream/midstream program delivery)
- Manufacturer and model number of new HPWH
- ENERGY STAR certificate matching model number (if applicable)
- HPWH quantity
- HPWH type (integrated HPWH, integrated HPWH 120v/15A circuit, split-system HPWH)
- Baseline volume (gallons), FHR, and UEF
- New HPWH volume (gallons), FHR, and UEF
- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

²⁷¹ 2010 ACEEE Summer Study on Energy Efficiency in Buildings, LBNL, “Heat Pump Water Heaters and American Homes: A Good Fit?” p 9-74. <https://www.aceee.org/files/proceedings/2010/data/papers/2205.pdf>.

Document Revision History

Table 7.2-5: [HPWH] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Incorporated updated ENERGY STAR specification v5.0. Updated documentation requirements. |
| FY 2026 | Clarified forthcoming federal standard effective and compliance dates. |

7.3 ENERGY STAR® SOLAR WATER HEATERS

7.3.1 Measure Description

This measure involves installing a new solar water heater in place of an electric storage water heater. Solar water heating deemed savings values are calculated based on the Solar Rating and Certification Corporation's (SRCC) test for solar water heaters (test OG-300).

7.3.1.1 Eligibility Criteria

These deemed savings are for solar water heaters installed as a replace-on-burnout measure or as an early retirement measure in existing homes and in new construction homes. However, savings are calculated under the assumption of replace-on-burnout.

7.3.1.2 Baseline Condition

The baseline condition is an electric storage water heater with baseline efficiency Uniform Energy Factor (UEF) determined by tank size and first hour rating (FHR), a proxy for draw pattern. according to the current federal energy efficiency standards for residential water heaters with tank sizes from 20 to 120 gallons, effective April 16, 2015, as published in 10 CFR Part 430.32 of the Federal Register (see Table 7.3-1).

This baseline applies to replace-on-burnout, early retirement, and new construction applications. No additional savings are awarded for early retirement. Early retirement projects should calculate savings using an assumed replace-on-burnout baseline. However, the Department of Energy (DOE) issued a notice of proposed rulemaking for consumer water heaters on July 27, 2023.²⁷² The TRM will add an early retirement baseline after the effective date for the new standard.

Table 7.3-1: [Solar DHW] Federal Standard for Residential Electric Storage Water Heaters

| Rated storage volume | Draw pattern | FHR ^{273,274} | UEF ²⁷⁵ |
|-----------------------|------------------|------------------------|------------------------|
| ≥ 20 gal and ≤ 55 gal | Very Small Usage | 0 ≤ FHR < 18 | 0.8808 – (0.0008 × Vr) |
| | Low Usage | 18 ≤ FHR < 51 | 0.9254 – (0.0003 × Vr) |
| | Medium Usage | 51 ≤ FHR < 75 | 0.9307 – (0.0002 × Vr) |
| | High Usage | 75 ≤ FHR | 0.9349 – (0.0001 × Vr) |

²⁷² Energy Conservation Program: Energy Conservation Standards for Consumer Water Heaters. <https://www.regulations.gov/document/EERE-2017-BT-STD-0019-0063>.

²⁷³ "The Revised Method of Test for Residential Water Heating and Its Impact on Incentive Programs" presentation, Glanville, Paul. ACEEE Hot Water Forum. February 24, 2015. <https://aceee.org/sites/default/files/pdf/conferences/hwf/2015/6B-Glanville.pdf>.

²⁷⁴ Assume FHR equal to that of installed water heater.

²⁷⁵ Vr is the Rated Storage Volume (in gallons), as determined pursuant to 10 CFR 429.17.

| Rated storage volume | Draw pattern | FHR ^{273,274} | UEF ²⁷⁵ |
|------------------------|------------------|---------------------------|--------------------------------------|
| > 55 gal and ≤ 120 gal | Very Small Usage | $0 \leq \text{FHR} < 18$ | $1.9236 - (0.0011 \times \text{Vr})$ |
| | Low Usage | $18 \leq \text{FHR} < 51$ | $2.0440 - (0.0011 \times \text{Vr})$ |
| | Medium Usage | $51 \leq \text{FHR} < 75$ | $2.1171 - (0.0011 \times \text{Vr})$ |
| | High Usage | $75 \leq \text{FHR}$ | $2.2418 - (0.0011 \times \text{Vr})$ |

7.3.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v5.0 specification, effective April 18, 2023. Qualified products must have a solar uniform energy factor (SUEF) greater than or equal to 3.0, and warranties of ≥ 10 years on collectors, ≥ 6 years on sealed systems, ≥ 2 years on controls, and ≥ 1 year on piping and parts.²⁷⁶ A complete list of certified ENERGY STAR solar water heaters can be accessed via the ENERGY STAR program website.²⁷⁷

Solar water heaters must be certified according to the current SRCC OG-300 standard based on tank size and final SUEF.²⁷⁸

7.3.2 Energy and Demand Savings Methodology

Solar water heating savings values are on a per-unit basis. Variables used to compute deemed savings include tank volume and installed unit SUEF as rated in the Solar Rating and Certification Corporation (SRCC) "Summary of SRCC Certified Solar Collector and Water Heating System Ratings." The SUEF is determined under SRCC's Operating Guideline 300, "Operating Guidelines and Minimum Standards for Certifying Solar Water Heating Systems" and was developed to compare solar water heating systems with conventional water heating systems rated with a UEF and listed in the Gas Appliance Manufacturers Association Directory of Certified Water Heating Products.

Both UEF and SUEF are based on the same environmental and hot water use conditions used in the DOE Test Procedures for Water Heaters. The only significant difference is that the DOE test does not specify solar radiation. So SRCC uses a 1500 Btu/sq.ft./day solar radiation profile—a value typical of Sunbelt states (note - the annual average solar radiation for Dallas is 1533 Btu/sq.ft./day. (Information on the SRCC can be found at <http://www.solar-rating.org/>.)

All deemed savings values are calculated using the following standard algorithms for water heating. These algorithms assume a replace-on-burnout or new construction scenario but may be used to award savings for early retirement projects.

²⁷⁶ ENERGY STAR Requirements (effective January 5th, 2022, released March 29, 2022).

https://www.energystar.gov/products/water_heaters/residential_water_heaters_key_product_criteria.

²⁷⁷ ENERGY STAR-certified water heaters qualified product listing. <https://www.energystar.gov/productfinder/product/certified-water-heaters/results>.

²⁷⁸ ENERGY STAR certification for residential water heaters. <https://solar-rating.org/programs/estar/>.

7.3.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = \frac{\rho \times C_p \times GPY \times (T_{SP} - T_{supply,annual}) \times \left(\frac{1}{UEF_{pre}} - \frac{1}{SUEF_{post}} \right)}{3,412}$$

Equation 7.3-1

Where:

| | | |
|--------|---|--|
| ρ | = | Water density = 8.33 lbs/gallons. |
| C_p | = | Specific heat of water = 1 Btu/lb·°F. |
| GPY | = | Estimated annual hot water use in gallons/year, specified by number of bedrooms in the home; see Table 7.3-2. For midstream/upstream applications, the number of bedrooms is assumed to be 3. ²⁷⁹ |

Table 7.3-2: [Solar DHW] Water Heater Consumption (Gal/Year)²⁸⁰

| Number of Bedrooms | | | |
|--------------------|--------|--------|--------|
| 1 | 2 | 3 | 4 |
| 13,924 | 17,018 | 20,112 | 23,206 |

| | | |
|---------------------|---|---|
| T_{SP} | = | Water heater set point = 120°F. ²⁸¹ |
| $T_{supply,annual}$ | = | Average supply water temperature = 75.9°F. ²⁸² |
| UEF_{pre} | = | Baseline uniform energy factor Table 7.3-1. |
| $SUEF_{post}$ | = | Solar uniform energy factor of new water heater. |
| 3,412 | = | Constant to convert from Btu to kWh. |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = DF \times \frac{\rho \times C_p \times GPY \times (T_{SP} - T_{supply,summer}) \times \left(\frac{1}{UEF_{pre}} - \frac{1}{SUEF_{post}} \right)}{365 \times 3,412}$$

Equation 7.3-2

²⁷⁹ Weighted average of number of bedrooms in West South-Central Region. 2020 RECS Survey Data – Table HC2.8 Structural and geographic characteristics of homes in the South and West regions, 2020. <https://www.eia.gov/consumption/residential/data/2020/>.

²⁸⁰ Building America Research Benchmark Definition. December 2009, p 13. Available online: <http://www.nrel.gov/docs/fy10osti/47246.pdf>.

²⁸¹ The data collection discussed in Appendix D of the Texas EM&V team's Annual Statewide Portfolio Report for Program Year 2014-Volume 1, Project Number 40891 (August 2015) supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

²⁸² Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

$T_{supply,summer}$ = For NCP, use average supply water temperature, 75.9°F²⁸³; for CP and 4CP, use summer supply water temperature, 85.41°F.²⁸⁴

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 7.3-3.

Table 7.3-3: [Solar DHW] Demand Factors²⁸⁵

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

7.3.2.2 Deemed Savings Tables

There are no deemed energy savings tables for this measure. Please see the algorithms above.

7.3.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) of a solar water heater is 15 years, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-SWH.²⁸⁶

7.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Number of bedrooms (not required for upstream/midstream program delivery)
- Solar DHW quantity
- Manufacturer and model number of new solar water heater
- Baseline volume (gallons), FHR, and UEF
- New solar water heater volume (gallons), FHR, and SUEF

²⁸³ Calculated according to the method in the Burch and Christensen 2007 paper “Towards Development of an Algorithm for Mains Water Temperature” and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

²⁸⁴ Calculated according to the method in the Burch and Christensen 2007 paper “Towards Development of an Algorithm for Mains Water Temperature” and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, August, and September.

²⁸⁵ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

²⁸⁶ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of unit installed or another pre-approved method of installation verification.

Document Revision History

Table 7.3-4: [Solar DHW] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | Measure origin. |
| FY 2026 | No revision. |

7.4 WATER HEATER TANK INSULATION

7.4.1 Measure Description

This measure requires the installation of tank wrap insulation on an uninsulated water heater tank.

7.4.1.1 Eligibility Criteria

Water heater tank insulation is a residential retrofit measure. New construction and water heater replacements are not eligible for this measure because they must meet current code requirements. Tank insulation must be installed on an uninsulated electric resistance water heater.

To be eligible for this measure, water heaters must have been manufactured prior to April 16, 2015. Water heaters manufactured after this date are compliant with the current federal standard²⁸⁷ and are built with a thicker tank with a higher baseline R-value. Modern water heaters are expected to be rated at a minimum of R-24.^{288,289}

7.4.1.2 Baseline Condition

The baseline is assumed to be a typical electric water heater with no insulation. The baseline tank is assumed to be one to two inches thick with an assumed R-value of approximately R-8 per inch.²⁹⁰

7.4.1.3 High-Efficiency Condition

The high-efficiency condition is a water heater tank wrap or insulated blanket with an R-value of at least 8. The manufacturer's instructions on the water heater jacket and the water heater itself should be followed. Thermostat and heating element access panels must be left uncovered.

²⁸⁷ "Energy Conservation Program for Consumer Products: Energy Conservation Standards for Residential Water Heaters, Direct Heating Equipment, and Pool Heaters". Effective 6/15/2010 with compliance starting 5/16/2015. <https://www.federalregister.gov/documents/2010/04/16/2010-7611/energy-conservation-program-energy-conservation-standards-for-residential-water-heaters-direct>.

²⁸⁸ "Do-It-Yourself Savings Project: Insulate Water Heater Tank," U.S. Department of Energy. <https://www.energy.gov/energysaver/do-it-yourself-savings-project-insulate-water-heater-tank>.

²⁸⁹ "Water Heating Products," Air-Conditioning, Heating, and Refrigeration Institute (AHRI). <https://www.ahrinet.org/scholarships-education/education/homeowners/save-energy/water-heating-products>.

²⁹⁰ "Energy Conservation Program for Consumer Products: Energy Conservation Standards for Water Heaters", Section V. Analytical Results and Conclusion, subsection C. Lessening of Utility or Performance of Products. Effective 1/20/2004. <https://www.federalregister.gov/documents/2001/01/17/01-1081/energy-conservation-program-for-consumer-products-energy-conservation-standards-for-water-heaters>.

7.4.2 Energy and Demand Savings Methodology

7.4.2.1 Savings Algorithms and Input Variables

Energy Savings

Hot water tank insulation energy savings are calculated by using the following formula:

$$\text{Energy Savings } [\Delta kWh] = (U_{pre} - U_{post}) \times A \times (T_{tank} - T_{ambient,annual}) \times \left(\frac{1}{RE}\right) \times \frac{\text{hours}}{3,412}$$

Equation 7.4-1

Where:

| | | |
|------------|---|--|
| R_{pre} | = | Uninsulated tank R-value = 12 [sq. ft. °F hr/Btu]. ²⁹¹ |
| R_{post} | = | Tank insulation R-value = 12 + 8 = 20 [sq. ft. °F hr/Btu]. |
| U_{pre} | = | $1 / R_{pre} = 1 / 12 = 0.083 \text{ Btu/hr sq.ft. °F.}$ |
| U_{post} | = | $1 / R_{post} = 1 / 20 = 0.05 \text{ Btu/hr sq.ft. °F.}$ |
| A | = | Tank surface area insulated in square feet (πDL) with L (length) and D (tank diameter) in feet. If the tank area is not known, use Table 7.4-1. |

Table 7.4-1: [Tank Insulation] Estimated Tank Area²⁹²

| Volume (gal) | A (sf.) |
|--------------|---------|
| 30 | 17.45 |
| 40 | 21.81 |
| 50 | 22.63 |
| 60 | 26.94 |
| 80 | 30.36 |
| 120 | 38.73 |

| | | |
|------------|---|--|
| T_{tank} | = | Average temperature of the tank, default use 120°F. ²⁹³ |
|------------|---|--|

²⁹¹ Baseline storage tank assembly is assumed to have thermal performance of R12, assuming an average tank thickness of 1-2 inches (average 1.5) and an approximate R-value of R-8 per inch.

²⁹² Tank area was obtained from a survey of electric water heater manufacturer data from A.O. Smith and Whirlpool conducted in 2013. Dimensions for each tank size were collected and averaged to determine typical square footage of each size water heater.

²⁹³ Data collection discussed in Appendix D of the EM&V team's Annual Statewide Portfolio Report for Program Year 2014-Volume 1, Texas PUC Project Number 40891 (August 2015), supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

| | | |
|----------------------|---|---|
| $T_{ambient,annual}$ | = | Ambient annual temperature [°F]. Use 78.3°F ²⁹⁴ for water heaters located in unconditioned space and 71.7°F ²⁹⁵ for water heaters located in conditioned space. |
| RE | = | Recovery efficiency; default = 0.98 for electric resistance water heaters. ²⁹⁶ |
| hours | = | 8,760 hours per year. |
| 3,412 | = | Constant to convert from Btu to kilo-watt hours. |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = (U_{pre} - U_{post}) \times A \times (T_{tank} - T_{ambient,summer}) \times \frac{1}{RE} \times \frac{DF}{3,412}$$

Equation 7.4-2

Where:

| | | |
|----------------------|---|--|
| $T_{ambient,summer}$ | = | Summer seasonal ambient temperature [°F]. For NCP, use 78.3°F for water heaters located in unconditioned space ²⁹⁷ and 71.7°F for water heaters located in conditioned space ²⁹⁸ ; for CP and 4CP, use 86.04°F for water heaters located in unconditioned space ²⁹⁹ and 73.2°F for water heaters located in conditioned space. ³⁰⁰ |
| DF | = | Demand factor for NCP, CP, or 4CP peak demand = 1. ³⁰¹ |

7.4.2.2 Deemed Energy Savings Tables

Table 7.4-2: [Tank Insulation] Energy Savings

| Volume (gal) | Unconditioned | Conditioned |
|--------------|---------------|-------------|
| 30 | 64 | 74 |
| 40 | 79 | 92 |
| 50 | 82 | 95 |

²⁹⁴ Average ambient temperatures were taken from TMY3 data for Kelly AFB, with a 7°F increase in winter and an 11°F increase in summer based on ASHRAE 152 Heating System & Cooling System Location Temperatures (Garage).

²⁹⁵ Average ambient temperatures for conditioned space were taken from the 2020 US Energy Information Administration Residential Energy Consumption Survey (RECS), tables hc7.8 and hc6.8. Summer and winter indoor temperature averages are weighted by the number of homes. Annual temperature is weighted by the number of days from the summer peak months from the Texas peak definition in Volume 1.

²⁹⁶ Default values based on median recovery efficiency of residential water heaters by fuel type in the AHRI database.

<https://www.ahridirectory.org/>.

²⁹⁷ Average ambient temperatures were taken from TMY3 data, with an 11°F increase in summer based on ASHRAE 152 Heating System & Cooling System Location Temperatures (Garage).

²⁹⁸ See $T_{ambient,annual}$ footnote.

²⁹⁹ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, and August.

³⁰⁰ Average ambient temperatures for conditioned space were taken from the 2020 US Energy Information Administration Residential Energy Consumption Survey (RECS), tables hc7.8 and hc6.8. Annual temperature is weighted by the number of days from the summer peak months from the Texas peak definition in Volume 1..

³⁰¹ Demand factor of 1 assumes a constant tank and near tank piping temperature is maintained across all hours of the year.

| Volume (gal) | Unconditioned | Conditioned |
|--------------|---------------|-------------|
| 60 | 98 | 114 |
| 80 | 111 | 128 |
| 120 | 141 | 163 |

7.4.2.3 Deemed Demand Savings Tables

Table 7.4-3: [Tank Insulation] Demand Savings

| Volume (gal) | NCP | | CP and 4CP | |
|--------------|---------------|-------------|---------------|-------------|
| | Unconditioned | Conditioned | Unconditioned | Conditioned |
| 30 | 0.0073 | 0.0084 | 0.0059 | 0.0081 |
| 40 | 0.0091 | 0.0105 | 0.0074 | 0.0102 |
| 50 | 0.0094 | 0.0109 | 0.0077 | 0.0106 |
| 60 | 0.0112 | 0.0130 | 0.0091 | 0.0126 |
| 80 | 0.0126 | 0.0146 | 0.0103 | 0.0142 |
| 120 | 0.0161 | 0.0186 | 0.0131 | 0.0181 |

7.4.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 7 years for water heater tank insulation, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-TankIns-Elec.³⁰²

7.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Water heater location (conditioned, unconditioned)
- R-value of the installed insulation
- Tank volume (30, 40, 50, 60, 80, 120)
- The R-value of the installed tank insulation
- Water heater model number and manufacture date

³⁰² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 7.4-4: [Tank Insulation] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Clarified baseline and added deemed savings. Updated documentation requirements. |
| FY 2026 | Updated ambient temperatures and deemed savings. |

7.5 WATER HEATER PIPE INSULATION

7.5.1 Measure Description

This measure requires the installation of pipe insulation on un-insulated water heater pipes that are served by an electric water heater.

7.5.1.1 Eligibility Criteria

Water heaters plumbed with functioning heat traps are not eligible to receive incentives for this measure. It is recommended that the installer (or contractor) checks to see if the water heater heat trap works properly before declaring the water heater ineligible.

Water heater pipe insulation is a residential retrofit measure. New construction and retrofits involving the installation of new water heaters are not eligible for this measure, because they must meet current code requirements. To be awarded these deemed savings, the fuel type of the water heater must be electricity.

7.5.1.2 Baseline Condition

The baseline is assumed to be a typical electric water heater with no functioning heat traps and no insulation on water heater pipes.

Table 7.5-1: [Pipe Insulation] Baseline Standard

| Baseline |
|------------------------------|
| Un-insulated hot water pipes |

7.5.1.3 High-Efficiency Condition

The efficiency standard requires an insulation thickness R-3.³⁰³

Table 7.5-2: [Pipe Insulation] Efficiency Standard

| Efficiency Standard |
|---------------------------|
| Minimum insulation of R-3 |

All visible hot water piping must be insulated. Savings are based on a maximum allowable insulation length of 6 feet of piping.

³⁰³ According to the International Residential Code (IRC) 2018 section N1103.4: Mechanical system piping requires R-3 insulation.

7.5.2 Energy and Demand Savings Methodology

7.5.2.1 Savings Algorithms and Input Variables

Energy Savings

Hot water pipe insulation energy savings are calculated using the following formula:

$$\text{Energy Savings } [\Delta kWh] = (U_{pre} - U_{post}) \times A \times (T_{pipe} - T_{ambient,annual}) \times \left(\frac{1}{RE}\right) \times \frac{8,760}{3,412}$$

Equation 7.5-1

Where:

$$U_{pre} = \frac{1}{2.03} = 0.49 \text{ Btu/hr sq. ft. } ^\circ\text{F.}^{304}$$

$$U_{post} = \frac{1}{2.03 + R_{insulation}} \text{ Btu/hr sq. ft. } ^\circ\text{F.}$$

$$R_{insulation} = \text{R-value of installed insulation.}$$

$$A = \text{Pipe surface area insulated in square feet } (\pi DL) \text{ with } L \text{ (length) and } D \text{ (pipe diameter) in feet. The maximum length allowable for insulation is 6 feet. If the pipe area is unknown, use the following table.}$$

Table 7.5-3: [Pipe Insulation] Estimated Pipe Surface Area

| Nominal Pipe Diameter (in.) | Outside Diameter (in.) | Pipe Surface Area (square feet) ³⁰⁵ |
|-----------------------------|------------------------|--|
| 0.5 | 0.625 | 0.16 x required input "Pipe Length insulated (feet)" |
| 0.75 | 0.875 | 0.23 x required input "Pipe Length insulated (feet)" |
| 1.0 | 1.125 | 0.29 x required input "Pipe Length insulated (feet)" |

$$T_{pipe} = \text{Water temperature in pipe } [^\circ\text{F}]. \text{ Use } 120^\circ\text{F.}^{306}$$

$$T_{ambient,annual} = \text{Ambient annual temperature } [^\circ\text{F}]. \text{ Use } 78.3^\circ\text{F}^{307} \text{ for water heaters located in unconditioned space; } 71.7^\circ\text{F}^{308} \text{ for water heaters located in conditioned space.}$$

³⁰⁴ 2.03 is the R-value representing the film coefficients between water and the inside of the pipe, and between the surface and air. Mark's Standard Handbook for Mechanical Engineers, 8th edition.

³⁰⁵ Factors used in the calculation for pipe area were determined by using the outside diameter of the pipe in inches, converting it to feet, and multiplying by π .

³⁰⁶ Data collection discussed in Appendix D of the EM&V team's Annual Statewide Portfolio Report for Program Year 2014-Volume 1, Project Number 40891 (August 2015), supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

³⁰⁷ Average ambient temperatures were taken from TMY3 data, with a 7°F increase in winter and an 11°F increase in summer based on ASHRAE 152 Heating System & Cooling System Location Temperatures (Garage).

³⁰⁸ Average ambient temperatures for conditioned space were taken from the 2020 US Energy Information Administration Residential Energy

RE = Recovery Efficiency (or in the case of heat pump water heaters, COP). If unknown, use 0.98 as a default for electric resistance water heaters or 2.2 for heat pump water heaters.³⁰⁹

8,760 = Total hours per year.

3,412 = Constant to convert from Btu to kWh.

Demand Savings

$$\text{Demand Savings } [\Delta kW] = (U_{pre} - U_{post}) \times A \times (T_{Pipe} - T_{ambient,summer}) \times \left(\frac{1}{RE}\right) \times \frac{DF}{3,412}$$

Equation 7.5-2

Where:

T_{ambient,summer} = Summer seasonal ambient temperature [°F]. For NCP, use 78.3°F for water heaters located in unconditioned space³¹⁰ and 71.7°F for water heaters located in conditioned space³¹¹; for CP and 4CP, use 86.04°F for water heaters located in unconditioned space³¹² and 73.2°F for water heaters located in conditioned space.³¹³

DF = Demand factor for NCP, CP, or 4CP peak demand = 1.³¹⁴

7.5.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.5.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

Consumption Survey (RECS), tables hc7.8 and hc6.8. Summer indoor temperature averages are weighted by the number of homes. Annual temperature is weighted by the number of days from the summer peak months from the Texas peak definition in Volume 1.

³⁰⁹ Default values based on median recovery efficiency of residential water heaters by fuel type in the AHRI database.

<https://www.ahridirectory.org/>.

³¹⁰ Average ambient temperatures were taken from TMY3 data, with an 11°F increase in summer based on ASHRAE 152 Heating System & Cooling System Location Temperatures (Garage).

³¹¹ See *T_{ambient,annual}* footnote.

³¹² Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, and August.

³¹³ Average ambient temperatures for conditioned space were taken from the 2020 US Energy Information Administration Residential Energy Consumption Survey (RECS), tables hc7.8 and hc6.8. Summer indoor temperature averages are weighted by the number of homes. Annual temperature is weighted by the number of days from the summer peak months from the Texas peak definition in Volume 1.

³¹⁴ Demand factor of 1 assumes a constant tank and near tank piping temperature is maintained across all hours of the year.

7.5.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 13 years for water heater pipe insulation, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-WH-PipeIns-Elec.³¹⁵

7.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Water heater location (conditioned, unconditioned)
- R-value of the installed insulation
- Recovery Efficiency (RE) or COP, if available
- Pipe length insulated (feet)
- Pipe surface area insulated in square feet (at least the pipe diameter in inches)

Document Revision History

Table 7.5-4: [Pipe Insulation] Revision History

| Guidebook version | Description of change |
|-------------------|-------------------------------|
| FY 2025 | No revision. |
| FY 2026 | Updated ambient temperatures. |

³¹⁵ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

7.6 FAUCET AERATORS

7.6.1 Measure Description

This measure involves installing aerators on kitchen and bathroom water faucets as a retrofit measure.

7.6.1.1 Eligibility Criteria

The savings values are per faucet aerator installed. It is not a requirement that all faucets in a home be treated for the deemed savings to be applicable.

These deemed savings are for residential, retrofit-only installation of kitchen and bathroom faucet aerators. To be awarded these deemed savings, the fuel type of the water heater must be electricity.

Aerators that have been defaced to make the flow rating illegible are not eligible for replacement. For direct install programs, all aerators removed shall be collected by the contractor and held for possible inspection by the utility until all inspections for invoiced installations have been completed.

7.6.1.2 Baseline Condition

The 2.2 gallon per minute (GPM) baseline faucet flow rate is based on the Department of Energy (DOE) maximum flow rate standard.³¹⁶ The deemed savings assume that the existing faucet aerators have a flow rate of 2.2 GPM.

7.6.1.3 High-Efficiency Condition

Flow rates of installed faucet aerators must meet or exceed the requirements list in the US EPA WaterSense specification for faucet aerators: 1.5 GPM.³¹⁷

7.6.2 Energy and Demand Savings Methodology

7.6.2.1 Savings Algorithms and Input Variables

Energy Savings

The deemed savings for any faucet aerator change case using aerators with flow rates of 1.5 GPM or lower are calculated as follows:

³¹⁶ DOE maximum flow rate for faucet aerators. https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=40.

³¹⁷ "High Efficiency Lavatory Faucet Specification," WaterSense, U.S. Environmental Protection Agency, Office of Wastewater Management. http://www.epa.gov/watersense/partners/faucets_final.html.

$$\text{Energy Savings } [\Delta kWh] = \frac{\rho \times C_P \times (GPM_{base} - GPM_{low}) \times N \times t \times 365 \times (T_{faucet,avg} - T_{supply,avg})}{FPH \times RE \times 3,412}$$

Equation 7.6-1

Where:

| | | |
|------------------|---|--|
| ρ | = | Water density, 8.33 lbs./gallon. |
| C_P | = | Specific heat of water, 1 Btu/lb°F. |
| GPM_{base} | = | Average baseline flow rate of aerator = 2.2 gallons per minute. |
| GPM_{low} | = | Post-installation flow rate of aerator, typically 1.5, 1.0, or 0.5 gallons per minute; if unknown, assume 1.5 gallons per minute. |
| N | = | Average number of persons per household = 2.83 persons. ³¹⁸ |
| t | = | Average time in minutes of hot water usage per person per day; default = 2.34 min/person/day. ³¹⁹ |
| $T_{faucet,avg}$ | = | Average faucet temperature = 88°F. ³²⁰ |
| $T_{supply,avg}$ | = | Average supply water temperature, 75.9°F. ³²¹ |
| RE | = | Recovery Efficiency (or in the case of heat pump water heaters, COP). If unknown, use 0.98 as a default for electric resistance water heaters or 2.2 for heat pump water heaters. ³²² |
| FPH | = | Average number of faucets per household = 3.99 faucets. ³²³ |
| 3,412 | = | Constant to convert from Btu to kWh. |

Demand Savings

Demand savings are calculated by substituting the average supply temperature for the average seasonal temperature, multiplying by a demand factor equivalent to the daily fraction hot water use during the weighted peak hour, and dividing by 365 days/year, with 365 canceling from the savings algorithm

³¹⁸ Occupants per home for Texas from US Census Bureau, "Persons per household, 2016-2020."

<https://www.census.gov/quickfacts/fact/table/TX,US/PST045221>.

³¹⁹ Cadmus and Opinion Dynamics Evaluation Team, "Memorandum: Showerhead and Faucet Aerator Meter Study." Prepared for Michigan Evaluation Working Group. Derived by taking weighted average of average minutes per person per day specified for kitchens (4.5) and bathrooms (1.6) assuming 1 kitchen aerator and 2.93 bathrooms.

³²⁰ Cadmus and Opinion Dynamics Evaluation Team, "Memorandum: Showerhead and Faucet Aerator Meter Study." Prepared for Michigan Evaluation Working Group. Derived by taking weighted average of average temperature for kitchens (93°F) and bathrooms (86°F) assuming 1 kitchen aerator and 2.93 bathrooms.

³²¹ Based on typical meteorological year (TMY) dataset for TMY3, available through the National Solar Radiation Database (NSRDB) Data Viewer, <https://nsrdb.nrel.gov/data-sets/archives.html>.

³²² Default values based on median recovery efficiency of residential water heaters by fuel type in the AHRI database. <https://www.ahridirectory.org/>.

³²³ Faucets per home assumed to be equal to one per kitchen and each half-bath plus 1.5 per each full bathroom per home. Bathroom counts extracted from the 2020 Residential Energy Consumption Survey (RECS), Table HC2.8. Structural and Geographic Characteristics of Homes in West South-Central region. <https://www.eia.gov/consumption/residential/data/2020/>.

numerator and denominator.

$$Demand\ Savings\ [\Delta kW] = \frac{\rho \times C_p \times (GPM_{base} - GPM_{low}) \times N \times t \times (T_{faucet,avg} - T_{supply})}{FPH \times RE \times Conversion\ Factor} \times DF$$

Equation 7.6-2

Where:

$T_{supply,summer}$ = For NCP, use average supply water temperature, 75.9°F.³²⁴; for CP and 4CP, use summer supply water temperature 85.41°F.³²⁵

DF = Demand factor for NCP, CP, or 4CP peak demand; see Table 7.6-1.

Table 7.6-1: [Faucet Aerators] Demand Factors³²⁶

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

7.6.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.6.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.6.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for faucet aerators, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-WH-Aertr.³²⁷

³²⁴ Calculated according to the method in the Burch and Christensen 2007 paper “Towards Development of an Algorithm for Mains Water Temperature” and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

³²⁵ Based on typical meteorological year (TMY) dataset for TMY3, available through the National Solar Radiation Database (NSRDB) Data Viewer, <https://nsrdb.nrel.gov/data-sets/archives.html>.

³²⁶ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

³²⁷ DEER READI (Remote Ex-Ante Database Interface). <http://www.deerresources.com/index.php/readi>.

7.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Recovery Efficiency (RE) or COP, if available
- Flow rate in gallons per minute (GPM) of faucet installed
- Water heater type (e.g., heat pump, electric resistance)
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

Document Revision History

Table 7.6-2: [Faucet Aerators] Revision History

| Guidebook version | Description of change |
|-------------------|-------------------------------------|
| FY 2025 | No revision. |
| FY 2026 | Updated number of faucets per home. |

7.7 LOW-FLOW SHOWERHEADS

7.7.1 Measure Description

This measure consists of removing existing showerheads and installing low-flow showerheads in residences.

7.7.1.1 Eligibility Criteria

The incentive is for replacement of an existing showerhead with a new showerhead rated at or below 2.0 gallons per minute (GPM). The only showerheads eligible for installation are those that are not easily modified to increase the flow rate.

These deemed savings are for showerheads installed as a retrofit measure in existing homes. To be awarded these deemed savings, the fuel type of the water heater must be electricity.

In addition to meeting the baseline requirements above, existing showerheads that have been defaced to make the flow rating illegible are not eligible for replacement. All showerheads removed shall be collected by the contractor and held for possible inspection by the utility until all inspections for invoiced installations have been completed.

7.7.1.2 Baseline Condition

The baseline flow rate is assumed to meet federal standards set at a maximum flow rate of 2.5 GPM.³²⁸

7.7.1.3 High-Efficiency Condition

Flow rates of installed showerheads must meet or exceed the US Environmental Protection Agency (EPA) WaterSense Program efficiency standards for showerheads of 2.0 GPM.³²⁹

³²⁸Federal energy conservation standards specified in the Code of Federal Regulations at 10 CFR 430.32(p).

http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/37.

³²⁹WaterSense, U.S. Environmental Protection Agency, Office of Wastewater Management
<http://www.epa.gov/watersense/products/showerheads.html>.

7.7.2 Energy and Demand Savings Methodology

7.7.2.1 Savings Algorithms and Input Variables

Energy Savings

Energy savings for this measure are calculated as follows:

$$\text{Energy Savings } [\Delta kWh] = \frac{\rho \times C_p \times (GPM_{base} - GPM_{low}) \times N \times t \times 365 \times (T_{shower} - T_{supply,avg})}{SPH \times RE \times 3,412}$$

Equation 7.7-1

Where:

| | | |
|------------------|---|--|
| ρ | = | Water density, 8.33 lbs/gallon. |
| C_p | = | Specific heat of water, 1 Btu/lb°F. |
| GPM_{base} | = | Average baseline flow rate of aerator = 2.5 gallons per minute. |
| GPM_{low} | = | Post-installation flow rate of aerator; if unknown, assume 2.0 gallons per minute. |
| N | = | Average number of persons per household = 2.83 persons. ³³⁰ |
| t | = | Average time in minutes of hot water usage per person per day; default = 7.8 min/person/day. ³³¹ |
| T_{shower} | = | Average shower temperature = 101°F. ³³² |
| $T_{supply,avg}$ | = | Average supply water temperature: 75.9°F. ³³³ |
| SPH | = | Average number of showerheads per household = 1.80 showerheads. ³³⁴ |
| RE | = | Recovery Efficiency (or in the case of heat pump water heaters, COP). If unknown, use 0.98 as a default for electric resistance water heaters or 2.2 for heat pump water heaters. ³³⁵ |

³³⁰ Occupants per home for Texas from US Census Bureau, "Persons per household, 2016-2020."

<https://www.census.gov/quickfacts/fact/table/TX,US/PST045221>.

³³¹ Cadmus and Opinion Dynamics Evaluation Team, "Memorandum: Showerhead and Faucet Aerator Meter Study." Prepared for Michigan Evaluation Working Group.

³³² Ibid.

³³³ Based on typical meteorological year (TMY) dataset for TMY3, available through the National Solar Radiation Database (NSRDB) Data Viewer, <https://nsrdb.nrel.gov/data-sets/archives.html>.

³³⁴ Showerheads per home assumed to be equal to the number of full bathrooms per home. Bathroom counts extracted from the 2020 Residential Energy Consumption Survey (RECS), Table HC2.8. Structural and geographic characteristics of homes in the West South-Central region. <https://www.eia.gov/consumption/residential/data/2020/>.

³³⁵ Default values based on median recovery efficiency of residential water heaters by fuel type in the AHRI database. <https://www.ahridirectory.org/>.

$$3,412 = \text{Constant to convert from Btu to kWh.}$$

Demand Savings

Demand savings are calculated by substituting the average supply temperature for the average seasonal temperature, multiplying by a demand factor equivalent to the daily fraction hot water use during the weighted peak hour, and dividing by 365 days/year, with 365 canceling from the savings algorithm numerator and denominator.

$$\text{Demand Savings } [\Delta kW] = \frac{\rho \times C_p \times (GPM_{base} - GPM_{low}) \times N \times t \times (T_{shower} - T_{supply,summer})}{SPH \times RE \times \text{Conversion Factor}} \times DF$$

Equation 7.7-2

Where:

$$T_{supply,summer} = \text{For NCP, use average supply water temperature, } 75.9^{\circ}\text{F}^{336}; \text{ for CP and 4CP, use summer supply water temperature } 85.41^{\circ}\text{F}^{337}$$

$$DF = \text{Demand factor for NCP, CP, or 4CP peak demand; see Table 7.7-1.}$$

Table 7.7-1: [LFSHs] Demand Factors³³⁸

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

7.7.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.7.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.7.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for low-flow showerheads, as specified in the California

³³⁶ Calculated according to the method in the Burch and Christensen 2007 paper “Towards Development of an Algorithm for Mains Water Temperature” and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

³³⁷ Based on typical meteorological year (TMY) dataset for TMY3, available through the National Solar Radiation Database (NSRDB) Data Viewer, <https://nsrdb.nrel.gov/data-sets/archives.html>.

³³⁸ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

7.7.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Recovery Efficiency (RE) or COP, if available
- Flow rate in gallons per minute (GPM) of showerhead installed
- Water heater type (e.g., heat pump, electric resistance)
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

Document Revision History

Table 7.7-2: [LFSHs] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | No revision. |
| FY 2026 | Updated number of showerheads per home. |

³³⁹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

7.8 SHOWERHEAD TEMPERATURE SENSITIVE RESTRICTOR VALVES

7.8.1 Measure Description

This measure consists of installing a temperature sensitive restrictor valve (TSRV) between the existing shower arm and showerhead. The valve restricts hot water flow through the showerhead once the water reaches a set temperature (generally 95°F) to prevent water from going down the drain prior to the user entering the shower, thereby eliminating behavioral waste.

7.8.1.1 Eligibility Criteria

These deemed savings are for temperature sensitive restrictor valves installed in new construction or as a retrofit measure in residential applications. Residences must have electrically fueled hot water to be eligible for this measure.

7.8.1.2 Baseline Condition

The baseline condition is the residential shower arm and standard (2.5 gpm) showerhead without a temperature sensitive restrictor valve installed.

7.8.1.3 High-Efficiency Condition

The high-efficiency condition is a temperature sensitive restrictor valve installed on a residential shower arm and showerhead with either a standard (2.5 gpm) or low-flow (2.0, 1.75, or 1.5 gpm) showerhead. If this measure is installed in conjunction with a low-flow showerhead, refer to the Low-Flow Showerheads measure and claim additional savings as outlined in that measure.

7.8.2 Energy and Demand Savings Methodology

7.8.2.1 Savings Algorithms and Input Variables

To determine gallons of behavioral waste (defined as hot water that goes down the drain before the user enters the shower) per year, the following formula was used:

$$\text{Annual Showerhead Behavioral Waste} = SHFR \times BW \times N_s \times 365 \times \frac{N_o}{N_{SH}}$$

Equation 7.8-1

Where:

SHFR = Showerhead flow rate, gallons per minute [gpm]; see Table 7.8-1.

BW = Behavioral waste, minutes per shower; see Table 7.8-1.

N_s = Number of showers per person per day; see Table 7.8-1.

| | | |
|----------|-----|--|
| 365 | $=$ | Constant to convert days to years. |
| N_O | $=$ | Number of occupants per home; see Table 7.8-1. |
| N_{SH} | $=$ | Number of showerheads per home; see Table 7.8-1. |

Applying the formula to the values returns the following values for baseline behavioral waste in gallons per showerhead per year:

$$\text{Showerhead (2.5 GPM): } 2.5 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} = 681 \text{ gal}$$

$$\text{Showerhead (2.0 GPM): } 2.0 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} = 545 \text{ gal}$$

$$\text{Showerhead (1.75 GPM): } 1.75 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} = 477 \text{ gal}$$

$$\text{Showerhead (1.5 GPM): } 1.5 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} = 409 \text{ gal}$$

Gallons of hot water saved per year can be found by multiplying the baseline behavioral waste gallons per year by the percent of hot water from Table 7.8-1.

$$\text{Gallons of hot water saved per year} = \text{Annual Behavioral Waste} \times \text{HW\%}$$

Equation 7.8-2

Where:

$$\text{HW\%} = \text{Hot water percentage; see Table 7.8-1.}$$

$$\text{Gallons of hot water saved per year (2.5 GPM): } 681 \times 0.825 = 562 \text{ gal}$$

$$\text{Gallons of hot water saved per year (2.0 GPM): } 545 \times 0.825 = 450 \text{ gal}$$

$$\text{Gallons of hot water saved per year (1.75 GPM): } 477 \times 0.825 = 393 \text{ gal}$$

$$\text{Gallons of hot water saved per year (1.5 GPM): } 409 \times 0.825 = 337 \text{ gal}$$

Table 7.8-1: [Showerhead TSRVs] Hot Water Usage Reduction

| Description | 2.5 gpm | 2.0 gpm | 1.75 gpm | 1.5 gpm |
|--|---------|---------|----------|---------|
| Average behavioral waste (minutes per shower) ³⁴⁰ | 0.783 | | | |
| Showers/person/day ³⁴¹ | 0.6 | | | |
| Occupants per home ³⁴² | 2.83 | | | |

³⁴⁰ "Disaggregating Residential Shower Warm-Up Waste," Sherman, Troy. August 2014. Derived by dividing average behavioral waste time (47 seconds) by 60 seconds.

³⁴¹ Cadmus and Opinion Dynamics Evaluation Team, "Memorandum: Showerhead and Faucet Aerator Meter Study." Prepared for Michigan Evaluation Working Group. June 2013.

³⁴² Occupants per home for Texas from US Census Bureau, "Persons per household, 2016-2020." <https://www.census.gov/quickfacts/fact/table/TX,US/PST045221>.

| Description | 2.5 gpm | 2.0 gpm | 1.75 gpm | 1.5 gpm |
|--|-----------------------------|---------|----------|---------|
| Showerheads/home ³⁴³ | 1.80 | | | |
| Gallons behavioral waste per showerhead per year | 681 | 545 | 477 | 409 |
| Percent hot water ³⁴⁴ | 80-85%, or 82.5% on average | | | |
| Gallons hot water saved per year | 562 | 450 | 393 | 337 |

Energy Savings

Energy savings for this measure are calculated as follows:

$$\text{Energy Savings } [\Delta \text{kWh}] = \frac{\rho \times C_p \times V \times (T_{SP} - T_{\text{supply,avg}})}{RE \times 3,412}$$

Equation 7.8-3

Where:

| | | |
|-------------------------|---|--|
| ρ | = | Water density, 8.33 lbs/gallon. |
| C_p | = | Specific heat of water, 1 Btu/lb°F. |
| V | = | Gallons of hot water saved per year per showerhead; see Table 7.8-1. |
| T_{SP} | = | Average shower temperature, 120°F. ³⁴⁵ |
| $T_{\text{supply,avg}}$ | = | Average supply water temperature, 75.9°F. ³⁴⁶ |
| RE | = | Recovery Efficiency (or in the case of heat pump water heaters, COP). If unknown, use 0.98 as a default for electric resistance water heaters, 2.2 for heat pump water heaters, or 0.8 for gas hot water heaters. ³⁴⁷ |
| 3,412 | = | Constant to convert from Btu to kWh. |

³⁴³ Showerheads per home assumed to be equal to the number of full bathrooms per home. Bathroom counts extracted from the 2020 Residential Energy Consumption Survey (RECS) Table HC2.8 Structural and geographic characteristics of homes in the West South Central region. <https://www.eia.gov/consumption/residential/data/2020/>.

³⁴⁴ "Calculating Savings For: Auto-Diverting Tub Spout System with ShowerStart TSV," Sherman, Troy. Evolve Technologies. December 15, 2015.

³⁴⁵ Data collection discussed in Appendix D of the Texas EM&V team's Annual Statewide Portfolio Report for Program Year 2014-Volume 1, Project Number 40891 (August 2015), also supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

³⁴⁶ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

³⁴⁷ Default values based on median recovery efficiency of residential water heaters by fuel type in the AHRI database, at http://cafs.ahrinet.org/gama_cafs/sdpsearch/search.jsp?table=CWH.

Demand Savings

Demand savings are calculated by substituting the average supply temperature for the average seasonal temperature, multiplying by a demand factor equivalent to the daily fraction hot water use during the weighted peak hour, and dividing by 365 days/year, with 365 canceling from the savings algorithm numerator and denominator.

$$\text{Demand Savings } [\Delta kW] = \frac{\rho \times C_P \times V \times (T_{SP} - T_{supply,summer})}{RE \times 3,412 \times 365} \times DF$$

Equation 7.8-4

Where:

$T_{supply,summer}$ = For NCP, use average supply water temperature, 75.9°F;³⁴⁸ for CP and 4CP, use summer supply water temperature 85.41°F.³⁴⁹

DF = Demand factor for NCP, CP, or 4CP peak demand; see Table 7.8-2.

Table 7.8-2: [Showerhead TSRVs] Demand Factors³⁵⁰

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

7.8.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.8.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.8.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for showerhead TSRVs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-WH-Shrhd.³⁵¹

³⁴⁸ Calculated according to the method in the Burch and Christensen 2007 paper “Towards Development of an Algorithm for Mains Water Temperature” and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

³⁴⁹ Calculated according to the method in the Burch and Christensen 2007 paper “Towards Development of an Algorithm for Mains Water Temperature” and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, August, and September.

³⁵⁰ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

³⁵¹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

7.8.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Flow rate in gallons per minute (gpm) of showerhead installed
- Water heater type (e.g., heat pump, electric resistance)
- DHW recovery efficiency (RE) or COP, if available
- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

Document Revision History

Table 7.8-3: [Showerhead TSRVs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Updated number of showerheads per home and resulting behavioral waste and hot water saved assumptions. |

7.9 TUB SPOUT AND SHOWERHEAD TEMPERATURE SENSITIVE RESTRICTOR VALVES

7.9.1 Measure Description

This measure consists of replacing existing tub spouts and shower heads with an automatically diverting tub spout and showerhead system with a temperature sensitive restrictor valve (TSRV) between the existing shower arm and showerhead. The tub spout will contain **temperature sensitive** restrictor technology that will cause the tub spout to automatically engage the anti-leak diverter once the water reaches a set temperature (generally 95°F). The water will divert to a showerhead with a normally closed valve that will prevent the hot water from going down the drain prior to the user entering the shower, thereby eliminating behavioral waste and tub spout leakage waste.

7.9.1.1 Eligibility Criteria

These deemed savings are for tub spout and showerhead systems with temperature sensitive restrictor technology installed in new construction or as a retrofit measure in existing homes. Residences must have electrically fueled hot water to be eligible for this measure.

7.9.1.2 Baseline Condition

The baseline condition is the residential tub spout with a standard diverter, and a standard (2.5 gpm) showerhead.

7.9.1.3 High-Efficiency Condition

The high-efficiency condition is an anti-leak, automatically diverting tub spout system with **temperature sensitive** restrictor technology installed on a residential showerarm and showerhead with a standard (2.5 gpm) or low-flow (2.0, 1.75, or 1.5 gpm) showerhead. If this measure is installed in conjunction with a low-flow showerhead, refer to the Low-Flow Showerheads measure and claim additional savings as outlined in that measure.

7.9.2 Energy and Demand Savings Methodology

7.9.2.1 Savings Algorithms and Input Variables

This system provides savings in two parts: elimination of behavioral waste (hot water that goes down the drain prior to the user entering the shower) and elimination of tub spout diverter leakage.

Part 1: To determine baseline gallons of behavioral waste per year, the following formula was used:

$$\text{Annual Showerhead Behavioral Waste} = \%WUE_{SH} \times SHFR \times BW \times N_S \times 365 \times \frac{N_O}{N_{SH}}$$

Equation 7.9-1

$$\text{Annual Tub Spout Behavioral Waste} = \%WUE_{TS} \times TSFR \times BW \times N_S \times 365 \times \frac{N_O}{N_{SH}}$$

Equation 7.9-2

Where:

| | | |
|--------------|---|--|
| $\%WUE_{SH}$ | = | Showerhead percentage of warm-up events; see Table 7.9-1. |
| $\%WUE_{TS}$ | = | Tub spout percentage of warm-up events; see Table 7.9-1. |
| $SHFR$ | = | Showerhead flow rate, gallons per minute [gpm]; see Table 7.9-1. |
| $TSFR$ | = | Tub spout flow rate, gallons per minute [gpm]; see Table 7.9-1. |
| BW | = | Behavioral waste, minutes per shower; see Table 7.9-1. |
| N_S | = | Number of showers per person per day; see Table 7.9-1. |
| 365 | = | Constant to convert days to years. |
| N_O | = | Number of occupants per home; see Table 7.9-1. |
| N_{SH} | = | Number of showerheads per home; see Table 7.9-1. |

Applying the formula to the values returns the following values:

$$\begin{aligned} \text{Showerhead (1.5 GPM): } & 0.6 \times \left(1.5 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} \right) = 245 \\ \text{Showerhead (1.75 GPM): } & 0.6 \times \left(1.75 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} \right) = 286 \\ \text{Showerhead (2.0 GPM): } & 0.6 \times \left(2.0 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} \right) = 327 \\ \text{Showerhead (2.5 GPM): } & 0.6 \times \left(2.5 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} \right) = 409 \\ \text{Tub Spout (5.0 GPM): } & 0.4 \times \left(5.0 \times 0.783 \times 0.6 \times 365 \times \frac{2.86}{1.80} \right) = 545 \end{aligned}$$

Part 2: To determine baseline gallons of diverter leakage per year, the following formula was used:

$$\text{Annual Diverter Waste} = DLR \times t_S \times N_S \times 365 \times \frac{N_O}{N_{SH}}$$

Equation 7.9-3

Where:

| | | |
|-------|---|---|
| DLR | = | Diverter leakage rate [gpm]; see Table 7.9-1. |
|-------|---|---|

$$t_s = \text{Shower time [min/shower]; see Table 7.9-1.}$$

Applying the formula to the values returns the following values:

$$\text{Diverter (0.8 GPM): } 0.8 \times 7.8 \times 0.6 \times 365 \times \frac{2.86}{1.80} = 2,171$$

Part 3: To determine gallons of water saved per year can be found by multiplying the total waste by the percent of hot water from Table 7.9-1.

$$\text{Gallons of hot water saved} = (SHBW + TSBW) \times HW\%_{SH,TS} + DW \times HW\%_D$$

Equation 7.9-4

Where:

$$SHBW = \text{Showerhead behavioral waste [gal].}$$

$$TSBW = \text{Tub spout behavioral waste [gal].}$$

$$DW = \text{Diverter waste [gal].}$$

$$HW\%_{SH,TS} = \text{Showerheads and tub spout hot water percentage; see Table 7.9-1.}$$

$$HW\%_D = \text{Diverter hot water percentage; see Table 7.9-1.}$$

Applying the formula to the values returns the following values:

$$\text{Total Annual Waste (1.5 gpm): } (245 + 545) \times 0.825 + 2,171 \times 0.737 = 2,252$$

$$\text{Total Annual Waste (1.75 gpm): } (286 + 545) \times 0.825 + 2,171 \times 0.737 = 2,286$$

$$\text{Total Annual Waste (2.0 gpm): } (327 + 545) \times 0.825 + 2,171 \times 0.737 = 2,320$$

$$\text{Total Annual Waste (2.5 gpm): } (409 + 545) \times 0.825 + 2,171 \times 0.737 = 2,387$$

Table 7.9-1: [Showerhead/Tub TSVs] Hot Water Usage Reduction

| Description | Part 1 – Behavioral Waste | | Part 2 – Diverter Leakage | Part 3 – Total |
|--|---------------------------|-------------------|---------------------------|----------------|
| | Showerhead Warm-up | Tub spout Warm-up | | |
| Baseline showerhead flow rate (gpm) | 1.5, 1.75, 2.0, or 2.5 | | | - |
| Tub spout flow rate (gpm) ³⁵² | - | 5.0 | | - |
| Percent of warm up events ³⁵³ | 60% | 40% | | - |
| Average behavioral waste (minutes per shower) ³⁵⁴ | 0.783 | | | - |

³⁵² Assumption from (Sherman 2015) Calculating Savings For: Auto-Diverting Tub Spout System with ShowerStart TSV.

³⁵³ Percent of warm up events from (Sherman 2014) Disaggregating Residential Shower Warm-Up Waste (Appendix B, Question 8).

³⁵⁴ “Disaggregating Residential Shower Warm-Up Waste,” Sherman, Troy. August 2014. Derived by dividing average behavioral waste time (47 seconds) by 60 seconds.

| Description | Part 1 – Behavioral Waste | | Part 2 – Diverter Leakage | Part 3 – Total |
|---|---------------------------|-------------------|---------------------------|----------------|
| | Showerhead Warm-up | Tub spout Warm-up | | |
| Average diverter leakage rate (gpm) ³⁵⁵ | - | | 0.80 | - |
| Average shower time (minutes) ³⁵⁶ | - | | 7.8 | - |
| Showers/person/day ³⁵⁷ | 0.6 | | | |
| Occupants per home ³⁵⁸ | 2.83 | | | |
| Showerheads per home ³⁵⁹ | 1.80 | | | |
| Gallons behavioral waste per tub spout/showerhead per year (1.5 gpm) | 245 | 545 | 2,171 | 2,961 |
| Gallons behavioral waste per tub spout/showerhead per year (1.75 gpm) | 286 | | | 3,002 |
| Gallons behavioral waste per tub spout/showerhead per year (2.0 gpm) | 327 | | | 3,043 |
| Gallons behavioral waste per tub spout/showerhead per year (2.5 gpm) | 409 | | | 3,125 |
| Percent hot water ³⁶⁰ | 80-85%, or 82.5% average | | 73.7% | - |
| Gallons hot water saved per year (1.5 gpm) | - | | | 2,252 |
| Gallons hot water saved per year (1.75 gpm) | - | | | 2,286 |
| Gallons hot water saved per year (2.0 gpm) | - | | | 2,320 |
| Gallons hot water saved per year (2.5 gpm) | - | | | 2,387 |

Energy Savings

Energy savings for this measure are calculated as follows:

$$\text{Energy Savings } [\Delta kWh] = \frac{\rho \times C_p \times V \times (T_{SP} - T_{supply,avg})}{RE \times 3,412}$$

Equation 7.9-5

³⁵⁵ Average diverter leak rate from (Taitem 2011) Taitem Tech Tip – Leaking Shower Diverter.

³⁵⁶ Cadmus and Opinion Dynamics Evaluation Team, “Memorandum: Showerhead and Faucet Aerator Meter Study.” Prepared for Michigan Evaluation Working Group.

³⁵⁷ Cadmus and Opinion Dynamics Evaluation Team, “Memorandum: Showerhead and Faucet Aerator Meter Study.” Prepared for Michigan Evaluation Working Group. June 2013.

³⁵⁸ Occupants per home for Texas from US Census Bureau, “Persons per household, 2016-2020.”

<https://www.census.gov/quickfacts/fact/table/TX,US/PST045221>.

³⁵⁹ Showerheads per home assumed to be equal to the number of full bathrooms per home. Bathroom counts extracted from the 2020 Residential Energy Consumption Survey (RECS) Table HC2.8 Structural and geographic characteristics of homes in the West South-Central region. <https://www.eia.gov/consumption/residential/data/2020/>.

³⁶⁰ “Calculating Savings For: Auto-Diverting Tub Spout System with ShowerStart TSV.” Sherman, Troy. Evolve Technologies. December 15, 2015.

Where:

| | | |
|------------------|---|--|
| ρ | = | Water density, 8.33 lbs/gallon. |
| C_p | = | Specific heat of water, 1 Btu/lb°F. |
| V | = | Gallons of hot water saved per year per showerhead; see Table 7.9-1. |
| T_{SP} | = | Average shower temperature = 101°F. ³⁶¹ |
| $T_{supply,avg}$ | = | Average supply water temperature: 75.9°F. ³⁶² |
| RE | = | Recovery Efficiency (or in the case of heat pump water heaters, COP). If unknown, use 0.98 as a default for electric resistance water heaters, 2.2 for heat pump water heaters, or 0.8 for gas hot water heaters. ³⁶³ |
| 3,412 | = | Constant to convert from Btu to kWh. |

Demand Savings

Demand savings are calculated by substituting the average supply temperature for the average seasonal temperature, multiplying by a demand factor equivalent to the daily fraction hot water use during the weighted peak hour, and dividing by 365 days/year, with 365 canceling from the savings algorithm numerator and denominator.

$$\text{Demand Savings } [\Delta kW] = \frac{\rho \times C_p \times V \times (T_{SP} - T_{supply,summer})}{RE \times 3,412 \times 365} \times DF$$

Equation 7.9-6

Where:

| | | |
|---------------------|---|---|
| $T_{supply,summer}$ | = | For NCP, use average supply water temperature, 75.9°F. ³⁶⁴ ; for CP and 4CP, use summer supply water temperature 85.41°F. ³⁶⁵ |
| DF | = | Demand factor for NCP, CP, or 4CP peak demand; see Table 7.9-2. |

³⁶¹ Data collection discussed in Appendix D of the Texas EM&V team's Annual Statewide Portfolio Report for Program Year 2014 -Volume 1, Project Number 40891 (August 2015), also supports a default value of 120°F.

<http://interchange.puc.texas.gov/Search/Documents?controlNumber=40891&itemNumber=19>.

³⁶² Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

³⁶³ Default values based on median recovery efficiency of residential water heaters by fuel type in the AHRI database, at http://cafs.ahrinet.org/gama_cafs/sdpsearch/search.jsp?table=CWH.

³⁶⁴ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

³⁶⁵ Calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base, taking the average mains temperature for June, July, August, and September.

Table 7.9-2: [Showerhead/Tub TSRVs] Demand Factors³⁶⁶

| Peak Type | DF |
|-----------|-------|
| NCP | 0.105 |
| CP | 0.038 |
| 4CP | 0.040 |

7.9.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.9.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

7.9.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for tub spout and showerhead TSRVs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID WtrHt-WH-Shrhd.³⁶⁷

7.9.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Flow rate in gallons per minute (GPM) of showerhead installed
- Water heater type (e.g., heat pump, electric resistance)
- DHW recovery efficiency (RE) or COP, if available
- Proof of purchase with date of purchase and quantity
 - Alternative: photo of replacement unit nameplate or other pre-approved method of installation verification

³⁶⁶ Building America Performance Analysis Procedures for Existing Homes, page 18, figure 4: combined domestic hot water use profile. <https://www.nrel.gov/docs/fy06osti/38238.pdf>.

³⁶⁷ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 7.9-3: [Showerhead/Tub TSRVs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Updated number of showerheads per home and resulting behavioral waste and hot water saved assumptions. |

8. RESIDENTIAL: APPLIANCES

8.1 ENERGY STAR® CLOTHES WASHERS

8.1.1 Measure Description

This measure involves the installation of an ENERGY STAR clothes washer.

8.1.1.1 Eligibility Criteria

This measure applies to ENERGY STAR-certified clothes washers.³⁶⁸

8.1.1.2 Baseline Condition

Effective January 1, 2018, the baseline condition is the Department of Energy (DOE) minimum efficiency standard³⁶⁹ for Integrated Modified Energy Factor (IMEF) and Integrated Water Factor (IWF) of top-loading clothes washers. While the DOE provides criteria for both top and front-loading washers, only the standards for top-loading washers are listed below, as a top-loading unit is assumed to be the baseline equipment. This approach is based on customers having the option to install a top-loading clothes washer. Therefore, savings are calculated using the lower top-loading baseline condition.

The DOE has published a Federal Register notice of Direct Final Rule pertaining to energy conservation standards for residential clothes washers, effective July 15, 2024.³⁷⁰ This standard will transition the efficiency metric from IMEF to EER. However, compliance is not required until March 1, 2028.

Table 8.1-1: [Clothes Washers] Federal Standard

| Product Type | Current Criteria As of Jan 1, 2018 |
|--|---------------------------------------|
| Top-loading, Standard (≥ 1.6 ft ³ capacity) | IMEF ≥ 1.57 IWF ≤ 6.5 |
| Top-loading, Compact (< 1.6 ft ³ capacity) | IMEF ≥ 1.15 IWF ≤ 12.0 |

8.1.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v8.1 specification, effective

³⁶⁸ ENERGY STAR Clothes Washers qualified product listing: <https://www.energystar.gov/productfinder/product/certified-clothes-washers/results>.

³⁶⁹ DOE minimum efficiency standard for residential clothes washers.
https://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/39.

³⁷⁰ New DOE final rule.
<https://www.energy.gov/eere/buildings/consumer-clothes-washers>.

February 5, 2018.³⁷¹ Qualified products must meet the minimum requirements from Table 8.1-2.

Table 8.1-2: [Clothes Washers] ENERGY STAR Specification

| Product Type | Current Criteria As of Feb 5, 2018 |
|---|---------------------------------------|
| Residential Front-loading (> 2.5 ft ³ capacity) | IMEF ≥ 2.76 IWF ≤ 3.2 |
| Residential Top-loading (> 2.5 ft ³ capacity) | IMEF ≥ 2.06 IWF ≤ 4.3 |
| Residential Small or Compact (< 2.5 ft ³ capacity) | IMEF ≥ 2.07 IWF ≤ 4.2 |

8.1.2 Energy and Demand Savings Methodology

Energy savings for this measure were derived using the ENERGY STAR Appliance Savings Calculator found on the ENERGY STAR website..³⁷² This document will be updated regularly to apply the values provided in the latest available ENERGY STAR Appliance Savings Calculator. The most recent Guidebook version should be referenced to determine the savings for this measure.

8.1.2.1 Savings Algorithms and Input Variables

Energy Savings

Energy savings can be derived by using the following:

$$\text{Energy Savings } [\Delta kWh] = kWh_{baseline} - kWh_{ES}$$

Equation 8.1-1

$$kWh_{baseline} = kWh_{conv,machine} + kWh_{conv,WH} + kWh_{conv,dryer} + kWh_{conv,LPM}$$

Equation 8.1-2

$$kWh_{conv,machine} = MCF \times RUEC_{conv} \times \frac{LPY}{RLPY}$$

Equation 8.1-3

$$kWh_{conv,WH} = WHCF \times RUEC_{conv} \times \frac{LPY}{RLPY}$$

Equation 8.1-4

³⁷¹ ENERGY STAR Program Requirements Product Specification for Clothes Washers..

<https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Final%20Version%208.0%20Clothes%20Washer%20Partner%20Commitments%20and%20Eligibility%20Criteria.pdf>.

³⁷² ENERGY STAR Appliance Savings Calculator (updated October 2016). The previously cited URL is no longer available, but a copy of the calculator can be provided upon request.

$$kWh_{savings} = \left[\left(\frac{Cap_{conv}}{IMEF_{FS}} \times LPY \right) - \left(RUEC_{conv} \times \frac{LPY}{RLPY} \right) - kWh_{conv,LPM} \right] \times \frac{DU_{DW}}{DUF}$$

Equation 8.1-5

$$kWh_{conv,LPM} = kW_{conv,LPM} \times (8,760 - LPY)$$

Equation 8.1-6

$$kWh_{ES} = kWh_{ES,machine} + kWh_{ES,WH} + kWh_{ES,dryer} + kWh_{ES,LPM}$$

Equation 8.1-7

$$kWh_{ES,machine} = MCF \times RUEC_{ES} \times \frac{LPY}{RLPY}$$

Equation 8.1-8

$$kWh_{ES,WH} = WHCF \times RUEC_{ES} \times \frac{LPY}{RLPY}$$

Equation 8.1-9

$$kWh_{savings} = \left[\left(\frac{Cap_{ES}}{IMEF_{ES}} \times LPY \right) - \left(RUEC_{ES} \times \frac{LPY}{RLPY} \right) - kWh_{ES,LPM} \right] \times \frac{DU_{DW}}{DUF}$$

Equation 8.1-10

$$kWh_{ES,LPM} = kW_{ES,LPM} \times (8,760 - LPY)$$

Equation 8.1-11

Where:

| | | |
|----------------------|---|--|
| $kWh_{baseline}$ | = | Federal standard baseline energy usage. |
| kWh_{ES} | = | ENERGY STAR average energy usage. |
| $kWh_{conv,machine}$ | = | Conventional machine energy usage. |
| $kWh_{ES,machine}$ | = | ENERGY STAR machine energy usage. |
| $kWh_{conv,WH}$ | = | Conventional water heater energy usage. |
| $kWh_{ES,WH}$ | = | ENERGY STAR water heater energy usage. |
| $kWh_{conv,LPM}$ | = | Conventional combined low-power mode energy usage. |
| $kWh_{ES,LPM}$ | = | ENERGY STAR combined low-power mode energy usage. |
| $kWh_{conv,dryer}$ | = | Conventional dryer energy usage. |
| $kWh_{ES,dryer}$ | = | ENERGY STAR dryer energy usage. |
| MCF | = | Machine consumption factor = 20%. |
| $WHCF$ | = | Water heater consumption factor = 80%. |
| LPY | = | Loads per year = 295. |

| | | |
|-----------------|---|--|
| $RLPY$ | = | Reference loads per year = 392. |
| $RUEC_{conv}$ | = | Conventional rated unit electricity consumption = 381 kWh/year (top-loading, standard), 163 kWh/year (top-loading, compact). |
| $RUEC_{ES}$ | = | ENERGY STAR rated unit electricity consumption; see Table 8.1-3. |
| Cap_{conv} | = | Average conventional machine capacity = 4.5 ft ³ (top-loading, standard), 2.1 ft ³ (top-loading, compact). |
| Cap_{ES} | = | Average ENERGY STAR machine capacity; see Table 8.1-3. |
| $IMEF_{FS}$ | = | Federal standard integrated modified energy factor; see Table 8.1-1. |
| $IMEF_{ES}$ | = | ENERGY STAR integrated modified energy factor; see Table 8.1-2. |
| $kW_{conv,LPM}$ | = | Conventional combined low-power mode wattage = 0.00115 kW (top-loading, standard), 0.00144 kW (top-loading, compact). |
| $kW_{ES,LPM}$ | = | ENERGY STAR combined low-power mode wattage; see Table 8.1-3. |
| DU_{DW} | = | Dryer usage in households with both a washer and a dryer = 95%. |
| DUF | = | Dryer use factor (percentage of washer loads dried in machine) = 91%. |
| 8,760 | = | Total hours per year. |

Table 8.1-3: [Clothes Washers] ENERGY STAR Clothes Washer Characteristics

| Product Type | RUEC (kWh) | Average Capacity (ft ³) | LPM Wattage (kW) |
|---|------------|-------------------------------------|------------------|
| Residential Front-loading (> 2.5 ft ³ capacity) | 127 | 4.0 | 0.00160 |
| Residential Top-loading (> 2.5 ft ³ capacity) | 230 | 4.5 | 0.00155 |
| Residential Small or Compact (< 2.5 ft ³ capacity) | 108 | 2.1 | 0.00144 |

Demand Savings

Demand savings can be derived by using the following:

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{\text{savings}}}{AOH} \times DF$$

Equation 8.1-12

$$AOH = LPY \times d$$

Equation 8.1-13

Where:

$$AOH = \text{Annual operating hours.}$$

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.1-4.

d = Average wash cycle duration = 1 hour.^{373,374}

Table 8.1-4: [Clothes Washers] Demand Factors³⁷⁵

| Peak Type | DF |
|-----------|-------|
| NCP | 0.076 |
| CP | 0.041 |
| 4CP | 0.041 |

8.1.2.2 Deemed Energy Savings Tables

Table 8.1-5: [Clothes Washers] Energy Savings

| Washer Type | Water Heater Fuel Type | Dryer Fuel Type | kWh Savings |
|--|------------------------|-----------------|-------------|
| Front-loading > 2.5 ft ³ | Electric | Electric | 428 |
| | | Gas | 187 |
| | Gas | Electric | 275 |
| | | Gas | 34 |
| Top-loading > 2.5 ft ³ | Electric | Electric | 205 |
| | | Gas | 114 |
| | Gas | Electric | 114 |
| | | Gas | 23 |
| Compact ≤ 2.5 ft ³ | Electric | Electric | 248 |
| | | Gas | 41 |
| | Gas | Electric | 215 |
| | | Gas | 8 |

³⁷³ Weighted average of Consumer Reports Cycle Times for Top and Front-Loading Clothes Washers.

³⁷⁴ Consumer Reports. "Top-loading washers remain more popular with Americans." April 13, 2010. Weighted average of 75 percent Top-Loading Clothes Washers and 25 percent Front-Loading Clothes Washers.

³⁷⁵ US Department of Energy's Building America B10 Benchmark load profiles for clothes washers.

8.1.2.3 Deemed Demand Savings Tables

Table 8.1-6: [Clothes Washers] Demand Savings

| Washer Type | Water Heater Fuel Type | Dryer Fuel Type | NCP kW Savings | CP kW Savings | 4CP kW Savings |
|--|------------------------|-----------------|----------------|---------------|----------------|
| Front-loading > 2.5 ft ³ | Electric | Electric | 0.110 | 0.060 | 0.060 |
| | | Gas | 0.048 | 0.026 | 0.026 |
| | Gas | Electric | 0.071 | 0.038 | 0.038 |
| | | Gas | 0.009 | 0.005 | 0.005 |
| Top-loading > 2.5 ft ³ | Electric | Electric | 0.053 | 0.028 | 0.028 |
| | | Gas | 0.029 | 0.016 | 0.016 |
| | Gas | Electric | 0.029 | 0.016 | 0.016 |
| | | Gas | 0.006 | 0.003 | 0.003 |
| Compact ≤ 2.5 ft ³ | Electric | Electric | 0.064 | 0.340 | 0.340 |
| | | Gas | 0.011 | 0.006 | 0.006 |
| | Gas | Electric | 0.055 | 0.030 | 0.030 |
| | | Gas | 0.002 | 0.001 | 0.001 |

1.1.1.1 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 11 years for clothes washers, which is consistent with the Technical Support Document for the current DOE Final Rule standards for residential clothes washers.³⁷⁶

8.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Unit quantity
- Clothes washer type (top-loading, front-loading, compact)
- DHW fuel type (gas, electric)

³⁷⁶ The median lifetime was calculated using the survival function outlined in the DOE Technical Support Document. Final Rule: Standards, Federal Register, 77 FR 32308 (May 31, 2012) and associated Technical Support Document. https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=68&action=viewlive. Download TSD at: <http://www.regulations.gov/#!documentDetail;D=EERE-2008-BT-STD-0019-0047>.

- Dryer fuel type (gas, electric)
- Proof of purchase with date of purchase, quantity, and model
 - Alternative: photo of unit installed or other pre-approved method of installation verification
- ENERGY STAR certificate matching new unit model number

Document Revision History

Table 8.1-7: [Clothes Washers] Revision History

| Guidebook version | Description of change |
|-------------------|--------------------------------------|
| FY 2025 | No revision. |
| FY 2026 | Clarified upcoming federal standard. |

8.2 ENERGY STAR® DISHWASHERS

8.2.1 Measure Description

This measure presents the accepted deemed savings awarded for the installation of an ENERGY STAR dishwasher. Savings are awarded at a flat per-unit rate, both for energy and demand savings. This measure will apply to existing homes and new construction.

8.2.1.1 Eligibility Criteria

This measure applies to both standard and compact dishwasher types.

8.2.1.2 Baseline Condition

Effective May 30, 2013, the baseline is the Department of Energy (DOE) minimum efficiency standard³⁷⁷ for dishwashers.

Table 8.2-1: [Dishwashers] Federal Standards for Dishwashers

| Product type | Estimated annual energy use (kWh/year) | Water consumption (gallons/cycle) |
|-------------------------------|--|-----------------------------------|
| Standard (≥ 8 place settings) | ≤ 307 | ≤ 5.0 |
| Compact (< 8 place settings) | ≤ 222 | ≤ 3.5 |

The DOE issued an updated direct final rule effective August 22, 2024. However, compliance with the amended federal standard is not required until April 23, 2027.³⁷⁸ The baseline will be updated at that time to reflect the current federal standard.

8.2.1.3 High-Efficiency Condition

The following table displays the ENERGY STAR Final Version 7.0 requirements for eligible dishwashers effective July 19, 2023.^{379,380} These values are subject to updates in ENERGY STAR specifications; energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

³⁷⁷ DOE minimum efficiency standard for residential dishwashers.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=38&action=viewlive..

³⁷⁸ DOE minimum efficiency standard for residential dishwashers. <https://www.regulations.gov/document/EERE-2019-BT-STD-0039-0065>.

³⁷⁹ ENERGY STAR Dishwashers Final Version 7.0 Program Requirements.

<https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%207.0%20Residential%20Dishwasher%20Final%20Specification.pdf>.

³⁸⁰ Available for download at:

http://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Residential%20Dishwasher%20Version%206.0%20Final%20Program%20Requirements_0.pdf.

Table 8.2-2: [Dishwashers] ENERGY STAR Specifications for Dishwashers

| Product type | Estimated annual energy use (kWh/year) | Water consumption (gallons/cycle) |
|--|--|-----------------------------------|
| Standard (≥ 8 place settings + 6 serving pieces) | ≤ 240 | ≤ 3.2 |
| Compact (< 8 place settings + 6 serving pieces) | ≤ 155 | ≤ 2.0 |

8.2.2 Energy and Demand Savings Methodology

8.2.2.1 Savings Algorithms and Input Variables

Energy Savings

Energy savings for this measure were derived using the ENERGY STAR Appliance Savings Calculator found on the ENERGY STAR website and the revised ENERGY STAR specification in Table 8.2-2.³⁸¹ Default values were taken directly from the ENERGY STAR calculator. This measure will be updated regularly to apply the values provided in the latest available ENERGY STAR specification and appliance calculator. The most recent TRM version should be referenced to determine measure savings for this measure.

$$\text{Energy Savings } [\Delta kWh] = kWh_{\text{baseline}} - kWh_{ES}$$

Equation 8.2-1

$$kWh_{\text{baseline}} = kWh_{\text{conv,machine}} + kWh_{\text{conv,WH}}$$

Equation 8.2-2

$$kWh_{\text{conv,machine}} = RUEC_{\text{conv}} \times MCF$$

Equation 8.2-3

$$kWh_{\text{conv,WH}} = RUEC_{\text{conv}} \times WHCF$$

Equation 8.2-4

$$kWh_{ES} = kWh_{ES,machine} + kWh_{ES,WH}$$

Equation 8.2-5

$$kWh_{ES,machine} = RUEC_{ES} \times MCF$$

Equation 8.2-6

$$kWh_{ES,WH} = RUEC_{ES} \times WHCF$$

Equation 8.2-7

³⁸¹ ENERGY STAR Appliance Savings Calculator (updated October 2016). <https://www.energystar.gov/buildings/facility-owners-and-managers/existing-buildings/save-energy/purchase-energy-saving-products>.

Where:

| | | |
|----------------------|---|---|
| $kWh_{baseline}$ | = | Federal standard baseline energy usage. |
| kWh_{ES} | = | ENERGY STAR average energy usage. |
| $kWh_{conv,machine}$ | = | Conventional machine energy. |
| $kWh_{conv,WH}$ | = | Conventional water heater energy. |
| $kWh_{ES,machine}$ | = | ENERGY STAR machine energy. |
| $kWh_{ES,WH}$ | = | ENERGY STAR water heater energy. |
| $RUEC_{conv}$ | = | Conventional rated use electricity consumption = 307 kWh/year for standard and 222 kWh/year for compact; see Table 8.2-1. |
| $RUEC_{ES}$ | = | ENERGY STAR rated use electricity consumption = 240 kWh/year for standard and 155 kWh/year for compact; see Table 8.2-2. |
| MCF | = | Machine consumption factor = 44%. |
| $WHCF$ | = | Water heater consumption factor = 56%. |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{savings}}{AOH} \times DF$$

Equation 8.2-8

$$AOH = CPY \times d$$

Equation 8.2-9

Where:

| | | |
|-------|---|---|
| AOH | = | Annual operating hours. |
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.2-3. |
| CPY | = | Cycles per year = 215. |
| d | = | Average wash cycle duration = 2.1 hours. ³⁸² |

Table 8.2-3: [Dishwashers] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 0.163 |
| CP | 0.042 |

³⁸² Average of Consumer Reports Cycle Times for Dishwashers.

| Peak Type | DF |
|-----------|-------|
| 4CP | 0.041 |

8.2.2.2 Deemed Energy Savings Tables

Table 8.2-4: [Dishwashers] Energy Savings

| Product type | Electric DHW | Gas DHW |
|--------------|--------------|---------|
| Standard | 67 | 29 |
| Compact | | |

8.2.2.3 Deemed Demand Savings Tables

Table 8.2-5: [Dishwashers] Peak Demand Savings

| Water heating fuel | NCP | CP | 4CP |
|--------------------|-------|-------|-------|
| Electric | 0.024 | 0.006 | 0.006 |
| Gas | 0.011 | 0.003 | 0.003 |

1.1.1.2 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years based on the Technical Support Document for the current DOE Final Rule standards for residential dishwashers.³⁸³

8.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Unit quantity
- Dishwasher type (standard or compact)
- DHW fuel type (gas or electric)

³⁸³ The median lifetime was calculated using the survival function outlined in the DOE Technical Support Document. Final Rule: Standards, Federal Register, 77 FR 31918 (May 30, 2012) and associated Technical Support Document.
https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=38&action=viewlive.

- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of unit installed or another pre-approved method of installation verification
- ENERGY STAR certificate matching new unit model number

Document Revision History

Table 8.2-6: [Dishwashers] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | No revision. |
| FY 2026 | Clarified upcoming federal standard. Incorporated latest ENERGY STAR specification. |

8.3 ENERGY STAR® REFRIGERATORS

8.3.1 Measure Description

This measure applies to all ENERGY STAR refrigerators that meet the criteria for the ENERGY STAR label specified below.

8.3.1.1 Eligibility Criteria

To qualify for early retirement, the ENERGY STAR unit must replace an existing, full-size unit with a maximum age of 20 years. To determine the remaining useful life of an existing unit, see Table 8.3-4. All retired refrigerators must be dismantled in an environmentally safe manner in accordance with applicable federal, state, and local regulations. The installer will provide documentation of proper disposal of refrigerators. To receive early retirement savings, the unit to be replaced must be functioning at the time of removal.

Newly installed refrigerators must meet current ENERGY STAR efficiency levels.

8.3.1.2 Baseline Condition

For new construction or replace-on-burnout, the baseline is the Department of Energy (DOE) minimum efficiency standard³⁸⁴ for refrigerators, effective September 15, 2014.

The DOE issued an updated direct final rule effective June 13, 2024. However, compliance with the new amended standard is not required until either January 31, 2029 or January 31, 2030 depending on the product class.³⁸⁵ The baseline will be updated at that time to reflect the current federal standard.

For early retirement, the baseline for refrigerators is the annual unit energy consumption of an assumed refrigerator's adjusted energy usage rating based on an average of values reported by the Midwest Energy Performance Analytics (MwEPA) Refrigerator and Freezer Energy Rating Database.³⁸⁶ Since the federal standard effective date occurred in late 2014, existing units manufactured as of 2015 are not eligible for early retirement.

8.3.1.3 High-Efficiency Condition

Table 8.3-1 displays the ENERGY STAR Final Version 5.1 Requirements for eligible consumer refrigeration products, effective September 15, 2014.³⁸⁷ Energy efficiency service providers are expected to comply

³⁸⁴ DOE minimum efficiency standard for residential refrigerators and freezers.

http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/43.

³⁸⁵ Notice of new DOE minimum efficiency standard for residential refrigerators and freezers.

<https://www.regulations.gov/document/EERE-2017-BT-STD-0003-0116>.

³⁸⁶ Refrigerator and Freezer Energy Rating Database. Midwest Energy Performance Analytics, Inc. in combination with the State of Wisconsin and US Department of Energy's Weatherization Assistance Program. <http://www.kouba-cavallo.com/refmods.htm>.

³⁸⁷ ENERGY STAR Consumer Refrigeration Products Final Version 5.1 Program Requirements.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%205.1%20Consumer%20Refrigeration%20Products%20Final%20Specification_0.pdf.

with the latest ENERGY STAR requirements.

Table 8.3-1: [Refrigerators] ENERGY STAR Specifications for Refrigerators

| Product type | Volume | Criteria as of September 15, 2014 |
|---|----------------------------|--|
| Full-size Refrigerators and Refrigerator-Freezers | 7.75 cubic feet or greater | Approximately 10 percent more energy efficient than the minimum federal standard (see Table 325) |

Table 8.3-2: [Refrigerators] ENERGY STAR Criteria by Refrigerator Product Category and Adjusted Volume³⁸⁸

| Product number | Product class | Baseline energy usage federal standard as of September 15, 2014 (kWh/year) ³⁸⁹ | Average ENERGY STAR energy usage (kWh/year) ³⁹⁰ | Adjusted volume ³⁹¹ (cubic feet) | Baseline energy usage (kWh/year) | ENERGY STAR energy usage (kWh/year) |
|----------------|---|---|--|---|----------------------------------|-------------------------------------|
| 3 | Refrigerator freezers—automatic defrost with top-mounted freezer without an automatic icemaker | $8.07 \times AV + 233.7$ | $7.26 \times AV + 210.3$ | 16.9 | 370.1 | 333.0 |
| 5 | Refrigerator-freezers—automatic defrost with bottom-mounted freezer without an automatic icemaker | $8.85 \times AV + 317.0$ | $7.97 \times AV + 285.3$ | 18.6 | 481.5 | 433.5 |
| 5A | Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker with TTD ice service | $9.25 \times AV + 475.4$ | $8.33 \times AV + 436.3$ | 32.1 | 772.1 | 703.5 |
| 7 | Refrigerator-freezers—automatic defrost with side-mounted freezer with an automatic icemaker with TTD ice service | $8.54 \times AV + 432.8$ | $7.69 \times AV + 397.9$ | 30.4 | 692.1 | 631.4 |

³⁸⁸ Available for download at <http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf>. Select product classes excluded.

³⁸⁹ <http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf>.

³⁹⁰ Approximately 10 percent more efficient than baseline, as specified in the ENERGY STAR Appliance Savings Calculator (updated September 2015).

http://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx.

³⁹¹ AV is calculated as a simple average across all refrigerators in the corresponding Product Class utilizing data provided by <https://www.energystar.gov/productfinder/product/certified-residential-refrigerators/results>.

8.3.2 Energy and Demand Savings Methodology

8.3.2.1 Savings Algorithms and Input Variables

New Construction or Replace-on-Burnout

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{\text{baseline}} - kWh_{\text{ES}}$$

Equation 8.3-1

Where:

kWh_{baseline} = Federal standard baseline energy usage; see Table 8.3-1: [Refrigerators] ENERGY STAR Specifications for Refrigerators

| Product type | Volume | Criteria as of September 15, 2014 |
|---|----------------------------|--|
| Full-size Refrigerators and Refrigerator-Freezers | 7.75 cubic feet or greater | Approximately 10 percent more energy efficient than the minimum federal standard (see Table 325) |

Table 8.3-2.

kWh_{ES} = ENERGY STAR average energy usage; see Table 8.3-1: [Refrigerators] ENERGY STAR Specifications for Refrigerators

| Product type | Volume | Criteria as of September 15, 2014 |
|---|----------------------------|--|
| Full-size Refrigerators and Refrigerator-Freezers | 7.75 cubic feet or greater | Approximately 10 percent more energy efficient than the minimum federal standard (see Table 325) |

Table 8.3-2.

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{\text{savings}}}{8,760} \times DF$$

Equation 8.3-2

Where:

8,760 = Total hours per year.

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.3-3.

Table 8.3-3: [Refrigerators] Demand Factors³⁹²

| Peak Type | DF |
|-----------|-------|
| NCP | 1.325 |
| CP | 1.134 |
| 4CP | 1.155 |

Early Retirement

Annual energy (kWh) and peak demand (kW) savings must be calculated separately for two time periods:

1. The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
2. The remaining time in the EUL period (EUL – RUL)

Annual energy and peak demand savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

Where:

RUL = Remaining useful life; see Table 8.3-4; if unknown, assume the age of the replaced unit is equal to the EUL resulting in a default RUL of 5.0 years.

EUL = Estimated useful life = 16 years.³⁹³

Table 8.3-4: [Refrigerators] Remaining Useful Life (RUL) of Replaced Refrigerator³⁹⁴

| Age of replaced refrigerator (years) | RUL (years) | Age of replaced refrigerator (years) | RUL (years) |
|--------------------------------------|-------------|--------------------------------------|-------------|
| 1 | 15.2 | 12 | 7.0 |
| 2 | 14.2 | 13 | 6.6 |
| 3 | 13.2 | 14 | 6.3 |
| 4 | 12.2 | 15 | 6.0 |
| 5 | 11.2 | 16 | 5.0 |
| 6 | 10.3 | 17 | 4.0 |
| 7 | 9.6 | 18 | 3.0 |

³⁹² See Section 2.3.

³⁹³ Department of Energy, Federal Register, 76 Final Rule 57516, Technical Support Document: 8.2.3.1 Estimated Survival Function. September 15, 2011. http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/43. Download TSD at: <https://www.regulations.gov/document/EERE-2008-BT-STD-0012-0128>.

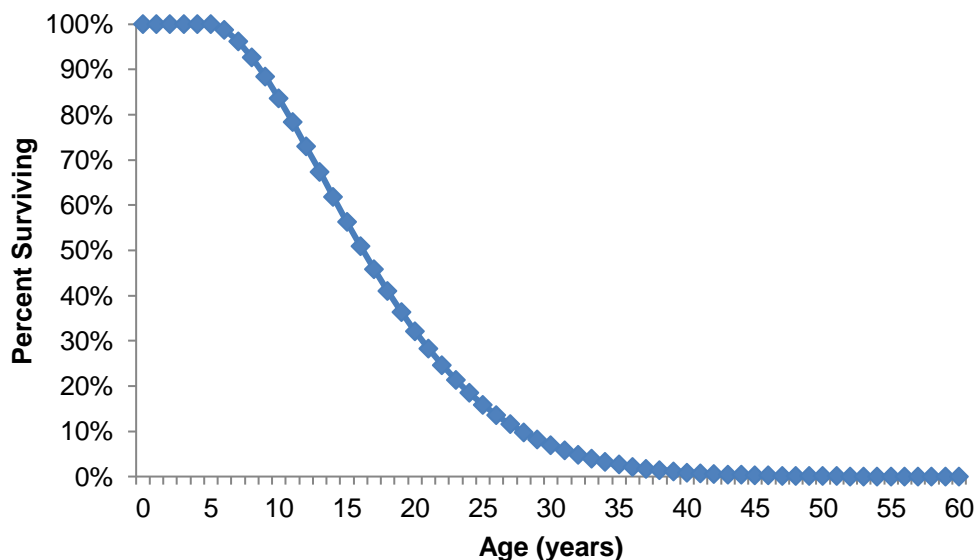
³⁹⁴ Current federal standard effective date is 9/15/2014. Since the federal standard effective date occurred in late 2014, existing units manufactured as of 2015 are not eligible to use the early retirement baseline and should use the ROB baseline instead.

| Age of replaced refrigerator (years) | RUL (years) | Age of replaced refrigerator (years) | RUL (years) |
|--------------------------------------|-------------|--------------------------------------|-------------|
| 8 | 8.9 | 19 | 2.0 |
| 9 | 8.3 | 20 | 1.0 |
| 10 | 7.8 | 21 ^{395,396} | 0.0 |
| 11 | 7.4 | | |

Derivation of RULs

ENERGY STAR refrigerators have an estimated useful life of 16 years. This estimate is consistent with the age at which approximately 50 percent of the refrigerators installed in a given year will no longer be in service, as described by the survival function in Figure 8.3-1.

Figure 8.3-1: [Refrigerators] Survival Function³⁹⁷



The method to estimate the remaining useful life (RUL) of a replaced system uses the age of the existing system to re-estimate the projected unit lifetime based on the survival function shown in Figure 8.3-1. The age of the refrigerator being replaced is found on the horizontal axis, and the corresponding percentage of surviving refrigerators is determined from the chart. The surviving percentage value is then divided in half, creating a new estimated useful lifetime applicable to the current unit age. Then,

³⁹⁵ RULs are capped at the 75th percentile of equipment age, 21 years, as determined based on DOE survival curves. Systems older than 21 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

³⁹⁶ Ward, B., Bodington, N., Farah, H., Reeves, S., and Lee, L. "Considerations for early replacement of residential equipment." Prepared by the Evaluation, Measurement, and Verification (EM&V) team for the Electric Utility Marketing Managers of Texas (EUMMOT). January 2015. This document has been made available to all Texas investor-owned utilities through the EM&V team's SharePoint.

³⁹⁷ Department of Energy, Federal Register, 76 Final Rule 57516, Technical Support Document: 8.2.3.1 Estimated Survival Function. September 15, 2011. http://www1.eere.energy.gov/buildings/appliance_standards/pdfs/refrig_finalrule_tsd.pdf.

the age (year) that corresponds to this new percentage is read from the chart. RUL is estimated as the difference between that age and the current age of the system being replaced.

For example, assume a refrigerator being replaced is 15 years old. The corresponding percent surviving value is 56 percent. Half of 56 percent is 28 percent. The age corresponding to 28 percent on the chart is 21 years. Therefore, the RUL of the refrigerator being replaced is $(21-15) = 6$ years.

Energy Savings

For the RUL period:

$$kWh_{savings,ER} = kWh_{manf} - kWh_{ES}$$

Equation 8.3-3

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

$$kWh_{savings,ROB} = kWh_{baseline} - kWh_{ES}$$

Equation 8.3-4

Where:

$$kWh_{manf} = \text{Baseline annual energy consumption of existing refrigerator} = 940 \text{ kWh.}^{398}$$

Demand Savings

To calculate demand savings for the early retirement of a refrigerator, a similar methodology is used as for replace-on-burnout installations, with separate savings calculated for the remaining useful life of the unit, and the remainder of the EUL as outlined in the section above.

For the RUL period:

$$kW_{savings,ER} = \frac{kWh_{savings,ER}}{8,760} \times DF$$

Equation 8.3-5

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

³⁹⁸ Existing unit consumption is derived from the MwEPA Refrigerator and Freezer Database. Consumption is weighted using appliance characteristics from the 2020 Residential Energy Consumption Survey (RECS) for units greater than 15 years old. Data for models manufactured prior to 1975 were excluded.

<https://www.energy.gov/scep/wap/articles/refrigerator-and-freezer-energy-rating-online-search-tool>.
<https://www.eia.gov/consumption/residential/data/2020/hc/pdf/HC%203.8.pdf>.

$$kW_{savings,ROB} = \frac{kWh_{savings,ROB}}{8,760} \times DF$$

Equation 8.3-6

Annual deemed peak demand savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

8.3.2.2 Deemed Energy Savings Tables

Table 8.3-5: [Refrigerators] Energy Savings (kWh) by Refrigerator Type

| Through-the-door ice? | Door type | Product class | ROB savings (kWh/year) | ER savings (kWh/year) |
|--|----------------|---|------------------------|-----------------------|
| No | Top Freezer | 3: Refrigerator freezers—automatic defrost with a top-mounted freezer without an automatic icemaker | 37 | 215 |
| | Bottom Freezer | 5: Refrigerator-freezers—automatic defrost with a bottom-mounted freezer without an automatic icemaker | 48 | 191 |
| Yes | Bottom Freezer | 5A: Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker with TTD ice service | 69 | 138 |
| | Side-by-Side | 7: Refrigerator-freezers—automatic defrost with side-mounted freezer with an automatic icemaker with TTD ice service | 61 | 121 |
| Unknown or Average Refrigerator ³⁹⁹ | | | 44 | 196 |

³⁹⁹ An “Unknown or Average” refrigerator’s savings are calculated as the difference between the weighted average of baseline energy usage ratings and the weighted average of ENERGY STAR energy usage ratings for the four selected refrigerator categories, with weights ascertained from averages of refrigerators in 10-14 year-old, 5-9 year-old, and 2-4 year-old age groups. The data used to calculate weights is hosted by Natural Resources Canada (NRCAN) at the following link which contains a table of the distribution of refrigerator types in households by year: <http://oee.nrcan.gc.ca/corporate/statistics/neud/dpa/showTable.cfm?type=CM§or=aaa&juris=ca&rn=3&page=1>. Weights were similarly calculated utilizing data from RECS (data which is summarized, i.e. not yearly, and located here: <https://www.eia.gov/consumption/residential/data/2015/hc/php/hc3.6.php>). While the reported distribution of refrigerator types between the two sets of data varies, we prefer the year-level granularity of the data from NRCAN considering that the differences between both sets of weighted average baseline energy usage and weighted average ENERGY STAR energy usage were nearly identical. Hence, we elect to utilize the more detailed weightings derived from the data hosted by NRCAN.

8.3.2.3 Deemed Demand Savings Tables

Table 8.3-6: [Refrigerators] Replace-on-Burnout Demand Savings (kW) by Refrigerator Type

| Through-the-door ice? | Door type | Product class | NCP | CP | 4CP |
|---------------------------------|----------------|---|--------|--------|--------|
| No | Top Freezer | 3: Refrigerator freezers—automatic defrost with a top-mounted freezer without an automatic icemaker | 0.0056 | 0.0048 | 0.0049 |
| | Bottom Freezer | 5: Refrigerator-freezers—automatic defrost with a bottom-mounted freezer without an automatic icemaker | 0.0073 | 0.0062 | 0.0063 |
| Yes | Bottom Freezer | 5A: Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker with TTD ice service | 0.0104 | 0.0089 | 0.0090 |
| | Side-by-Side | 7: Refrigerator-freezers—automatic defrost with side-mounted freezer with an automatic icemaker with TTD ice service | 0.0092 | 0.0079 | 0.0080 |
| Unknown or Average Refrigerator | | | 0.0067 | 0.0057 | 0.0058 |

Table 8.3-7: [Refrigerators] Early Retirement Demand Savings (kW) by Refrigerator Type

| Through-the-door ice? | Door type | Product class | NCP | CP | 4CP |
|-----------------------|----------------|--|-------|-------|-------|
| No | Top Freezer | 3: Refrigerator freezers—automatic defrost with a top-mounted freezer without an automatic icemaker | 0.033 | 0.028 | 0.028 |
| | Bottom Freezer | 5: Refrigerator-freezers—automatic defrost with a bottom-mounted freezer without an automatic icemaker | 0.029 | 0.025 | 0.025 |

| Through-the-door ice? | Door type | Product class | NCP | CP | 4CP |
|---------------------------------|----------------|---|-------|-------|-------|
| Yes | Bottom Freezer | 5A: Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker with TTD ice service | 0.018 | 0.016 | 0.016 |
| | Side-by-Side | 7: Refrigerator-freezers—automatic defrost with side-mounted freezer with an automatic icemaker with TTD ice service | 0.021 | 0.018 | 0.018 |
| Unknown or Average Refrigerator | | | 0.030 | 0.025 | 0.026 |

1.1.1.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 16 years based on the current DOE Final Rule standards for residential refrigerators.⁴⁰⁰

8.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- ENERGY STAR certificate matching new unit model number
- Unit quantity
- Baseline type (new construction, replace-on-burnout, or early retirement)
- Photograph demonstrating functionality of existing equipment and/or customer responses to survey questionnaire documenting the condition of the replaced unit and their motivation for measure replacement for early retirement eligibility determination (early retirement only)
- Document proper disposal of the existing refrigerator (early retirement only)

⁴⁰⁰ Final Rule: Standards, Federal Register, 76 FR 57516 (Sept. 15, 2011) and associated Technical Support Document. http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/43. Download TSD at: <http://www.regulations.gov/#!documentDetail;D=EERE-2008-BT-STD-0012-0128>.

- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of unit installed or another pre-approved method of installation verification

Document Revision History

Table 8.3-8: [Refrigerators] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated early retirement age eligibility. |
| FY 2026 | Updated early retirement age eligibility and weighting using latest RECs data. Updated resulting early retirement savings tables. Clarified upcoming federal standard. |

8.4 ENERGY STAR® FREEZERS

8.4.1 Measure Description

This measure applies to all ENERGY STAR freezers that meet the criteria for the ENERGY STAR label specified below.

8.4.1.1 Eligibility Criteria

To qualify for early retirement, the ENERGY STAR unit must replace an existing, full-size unit with a maximum age of 27 years. To determine the remaining useful life of an existing unit, see Table 8.4-4. All retired freezers must be dismantled in an environmentally safe manner in accordance with applicable federal, state, and local regulations. The installer will provide documentation of proper disposal of freezers. To receive early retirement savings, the unit to be replaced must be functioning at the time of removal.

Newly installed freezers must meet current ENERGY STAR efficiency levels.

8.4.1.2 Baseline Condition

For new construction or replace-on-burnout, the baseline is the Department of Energy (DOE) minimum efficiency standard⁴⁰¹ for freezers, effective September 15, 2014.

The DOE issued an updated direct final rule effective June 13, 2024. However, compliance with the new amended federal standard is not required until either January 31, 2029 or January 31, 2030 depending on product class.⁴⁰² The baseline will be updated at that time to reflect the current federal standard.

For early retirement, the baseline for freezers is the annual unit energy consumption of a freezer's adjusted energy usage rating based on an average of values reported by the Midwest Energy Performance Analytics (MwEPA) Refrigerator and Freezer Energy Rating Database.⁴⁰³ Since the federal standard effective date occurred in late 2014, existing units manufactured as of 2015 are not eligible for early retirement.

Alternatively, the baseline annual energy usage of the freezer being replaced may be estimated by metering for a period of at least two hours using the measurement protocol specified in the DOE report, "Incorporating Refrigerator Replacement into the Weatherization Assistance Program."⁴⁰⁴

⁴⁰¹ DOE minimum efficiency standard for residential refrigerators and freezers. https://www.ecfr.gov/cgi-bin/text-idx?SID=48f64e166fe3561666f871e521996e13&mc=true&node=se10.3.430_132&rgn=div8.

⁴⁰² Notice of new DOE minimum efficiency standard for residential refrigerators and freezers. <https://www.regulations.gov/document/EERE-2017-BT-STD-0003-0116>.

⁴⁰³ Refrigerator and Freezer Energy Rating Database. Midwest Energy Performance Analytics, Inc. in combination with the State of Wisconsin and US Department of Energy's Weatherization Assistance Program. <http://www.kouba-cavallo.com/refmods.htm>.

⁴⁰⁴ Alex Moore, DandR International, Ltd. "Incorporating Refrigerator Replacement into the Weatherization Assistance Program" Information Tool Kit." Department of Energy. November 19, 2001. https://aceee.org/files/proceedings/2002/data/papers/SS02_Panel2_Paper16.pdf.

To determine annual kWh of the freezer being replaced, use the following formula:

$$\text{Annual kWh Usage} = \frac{WH \times 8,760}{h \times 1,000}$$

Equation 8.4-1

Where:

| | | |
|--------------|---|---|
| <i>WH</i> | = | <i>Watt-hours metered during a period.</i> |
| <i>h</i> | = | <i>Measurement time (hours).</i> |
| <i>8,760</i> | = | <i>Total hours per year.</i> |
| <i>1,000</i> | = | <i>Constant to convert from watts to kilowatts.</i> |

8.4.1.3 High-Efficiency Condition

Table 8.4-1 displays the ENERGY STAR Final Version 5.1 Requirements for eligible consumer refrigeration products, effective September 15, 2014.⁴⁰⁵ Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

Table 8.4-1: [Freezers] ENERGY STAR Specifications for Freezers⁴⁰⁶

| Product type | Volume | Criteria as of September 15, 2014 |
|--------------|----------------------------|--|
| Standard | 7.75 cubic feet or greater | Approximately 10 percent more energy efficient than the minimum federal standard (see Table 8.4-2) |
| Compact | Less than 7.75 cubic feet | Approximately 10 percent more energy efficient than the minimum federal standard (see Table 8.4-2) |

⁴⁰⁵ ENERGY STAR Consumer Refrigeration Products Final Version 5.1 Program Requirements.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%205.1%20Consumer%20Refrigeration%20Products%20Final%20Specification_0.pdf.

⁴⁰⁶ https://www.energystar.gov/products/appliances/refrigerators/key_product_criteria

Table 8.4-2: [Freezers] ENERGY STAR Criteria by Select Freezer Product Category and Adjusted Volume⁴⁰⁷

| Product number | Full product name ⁴⁰⁸ | Product class | Baseline energy usage federal standard (kWh/year) ⁴⁰⁹ | Average ENERGY STAR® energy usage (kWh/year) ⁴¹⁰ | Adjusted volume ⁴¹¹ (cubic feet) | Baseline energy usage (kWh/year) | ENERGY STAR energy usage (kWh/year) |
|----------------|---|----------------------------------|--|---|---|----------------------------------|-------------------------------------|
| 8 | Upright freezers with manual defrost | Upright (Manual Defrost) | $5.57 \times AV + 193.7$ | $5.01 \times AV + 174.3$ | 16.12 | 283.5 | 255.1 |
| 9 | Upright freezers with automatic defrost without an automatic icemaker | Upright (Auto Defrost) | $8.62 \times AV + 228.3$ | $7.76 \times AV + 205.5$ | 29.96 | 486.6 | 438.0 |
| 10 | Chest freezers and all other freezers except compact freezers | Chest | $7.29 \times AV + 107.8$ | $6.56 \times AV + 97$ | 25.25 | 291.8 | 262.6 |
| 16 | Compact upright freezers with manual defrost | Compact Upright (Manual Defrost) | $8.65 \times AV + 225.7$ | $7.79 \times AV + 203.1$ | 5.34 | 271.9 | 244.7 |
| 17 | Compact upright freezers with automatic defrost | Compact Upright (Auto Defrost) | $10.17 \times AV + 351.9$ | $9.15 \times AV + 316.7$ | 7.95 | 432.7 | 389.4 |
| 18 | Compact chest freezers | Compact Chest | $9.25 \times AV + 136.8$ | $8.33 \times AV + 123.1$ | 9.06 | 220.6 | 198.6 |

⁴⁰⁷ Available for download at <http://www.gpo.gov/fdsys/pkg/CFR-2012-title10-vol3/pdf/CFR-2012-title10-vol3-sec430-32.pdf>. Select product classes excluded.

⁴⁰⁸ Note that when calculating deemed savings for upright freezers, we calculated a weighted average of adjusted energy usage of manual versus automatic defrost upright freezers, with weights based on the number of millions-of-households which contain these types of freezers, obtained from the Residential Energy Consumption Survey, or RECS, (<https://www.eia.gov/consumption/residential/data/2015/hc/php/hc3.6.php>), thus eliminating this input from consideration.

⁴⁰⁹ https://www.ecfr.gov/cgi-bin/text-idx?SID=48f64e166fe3561666f871e521996e13&mc=true&node=se10.3.430_132&rgn=div8

⁴¹⁰ Approximately 10 percent more efficient than baseline, as specified in the ENERGY STAR Appliance Savings Calculator (updated September 2015).

http://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx.

⁴¹¹ AV is calculated as a simple average per selected freezer product type in the corresponding Product Class utilizing data provided by <https://www.energystar.gov/productfinder/product/certified-residential-freezers/results>

8.4.2 Energy and Demand Savings Methodology

8.4.2.1 Savings Algorithms and Input Variables

New Construction or Replace-on-Burnout

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{\text{baseline}} - kWh_{ES}$$

Equation 8.4-2

Where:

kWh_{baseline} = Federal standard baseline energy usage; see Table 8.4-2.

kWh_{ES} = ENERGY STAR average energy usage; see Table 8.4-2.

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{\text{savings}}}{8,760 \text{ hrs}} \times DF$$

Equation 8.4-3

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.4-3.

Table 8.4-3: [Freezers] Demand Factors⁴¹²

| Peak Type | DF |
|-----------|-------|
| NCP | 1.325 |
| CP | 1.134 |
| 4CP | 1.155 |

Early Retirement

Annual energy (kWh) and peak demand (kW) savings must be calculated separately for two time periods:

1. The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
2. The remaining time in the EUL period (EUL – RUL)

⁴¹² See Volume 1, Section 4.

Annual energy and peak demand savings are calculated by weighting the early retirement and replacement-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

Where:

RUL = Remaining useful life (see Table 8.4-4); if unknown, assume the age of the replaced unit is equal to the EUL resulting in a default RUL of 5.0 years.

EUL = Estimated useful life = 22 years.

Table 8.4-4: [Freezers] Remaining Useful Life (RUL) of Replaced Freezer⁴¹³

| Age of replaced freezer (years) | RUL (years) | Age of replaced Freezer (years) | RUL (years) | Age of replaced Freezer (years) | RUL (years) |
|---------------------------------|-------------|---------------------------------|-------------|---------------------------------|-------------|
| 1 | 20.7 | 10 | 12.1 | 19 | 6.6 |
| 2 | 19.7 | 11 | 11.3 | 20 | 6.2 |
| 3 | 18.7 | 12 | 10.6 | 21 | 5.9 |
| 4 | 17.7 | 13 | 9.9 | 22 | 5.0 |
| 5 | 16.7 | 14 | 9.2 | 23 | 4.0 |
| 6 | 15.7 | 15 | 8.6 | 24 | 3.0 |
| 7 | 14.8 | 16 | 8.1 | 25 | 2.0 |
| 8 | 13.8 | 17 | 7.5 | 26 | 1.0 |
| 9 | 13.0 | 18 | 7.1 | 27 ^{414,415} | 0.0 |

Derivation of RULs

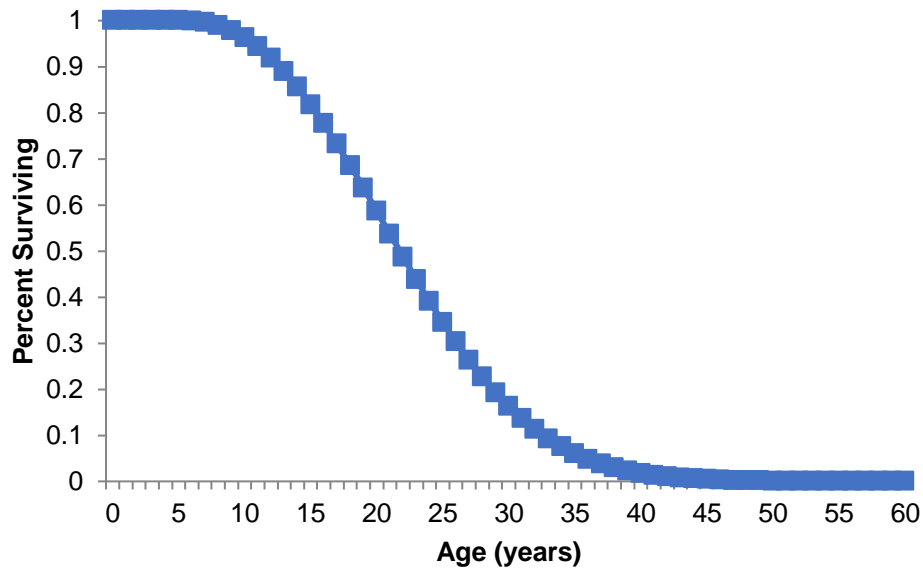
ENERGY STAR freezers have an estimated useful life of 22 years. This estimate is consistent with the age at which approximately 50 percent of the freezers installed in a given year will no longer be in service, as described by the survival function in Figure 8.4-1.

⁴¹³ Current federal standard effective date is 9/15/2014. Since the federal standard effective date occurred in late 2014, existing units manufactured as of 2015 are not eligible to use the early retirement baseline and should use the ROB baseline instead.

⁴¹⁴ RULs are capped at the 75th percentile of equipment age, 27 years, as determined based on DOE survival curves. Systems older than 27 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

⁴¹⁵ Ward, B., Bodington, N., Farah, H., Reeves, S., and Lee, L. "Considerations for early replacement of residential equipment." Prepared by the Evaluation, Measurement, and Verification (EM&V) team for the Electric Utility Marketing Managers of Texas (EUMMOT). January 2015. This document has been made available to all Texas investor-owned utilities through the EM&V team's SharePoint.

Figure 8.4-1: [Freezers] Survival Function⁴¹⁶



The method for estimating the remaining useful life (RUL) of a replaced system uses the age of the existing system to re-estimate the projected unit lifetime based on the survival function shown in Figure 8.4-1. The age of the freezer being replaced is found on the horizontal axis, and the corresponding percentage of surviving freezers is determined from the chart. The surviving percentage value is then divided in half, creating a new estimated useful lifetime applicable to the current unit age. Then, the age (year) that corresponds to this new percentage is read from the chart. RUL is estimated as the difference between that age and the current age of the system being replaced.

For example, assume a freezer being replaced is 22 years old (the estimated useful life). The corresponding percent surviving value is approximately 50 percent. Half of 50 percent is 25 percent. The age corresponding to 25 percent on the chart is approximately 27 years. Therefore, the RUL of the freezer being replaced is 27-22 = 5 years.

Energy Savings

For the RUL period:

$$kWh_{savings,ER} = kWh_{manf} - kWh_{ES}$$

Equation 8.4-4

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

⁴¹⁶ Department of Energy, Federal Register, 76 Final Rule 57516, Technical Support Document: 8.2.3.1 Estimated Survival Function. September 15, 2011. http://www1.eere.energy.gov/buildings/appliance_standards/pdfs/refrig_finalrule_tsd.pdf.

$$kWh_{savings,ROB} = kWh_{baseline} - kWh_{ES}$$

Equation 8.4-5

Where:

$$kWh_{manf} = \text{Baseline annual energy consumption of existing refrigerator} = 805 \text{ kWh}^{417}$$

Demand Savings

To calculate demand savings for the early retirement of a freezer, a similar methodology is used as for replace-on-burnout installations, with separate savings calculated for the remaining useful life of the unit, and the remainder of the EUL as outlined in the section above.

For the RUL period:

$$kW_{savings,ER} = \frac{kWh_{savings,ER}}{8,760 \text{ hrs}} \times DF$$

Equation 8.4-6

For The remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

$$kW_{savings,ROB} = \frac{kWh_{savings,ROB}}{8,760 \text{ hrs}} \times DF$$

Equation 8.4-7

Annual deemed peak demand savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

8.4.2.2 Deemed Energy Savings Tables

Table 8.4-5: [Freezers] Energy Savings (kWh) by Freezer Type

| Freezer type | Product Class | ROB savings (kWh/year) | ER savings (kWh/year) |
|--------------|---------------------------------------|------------------------|-----------------------|
| Chest | Standard ($\geq 7.75 \text{ ft}^3$) | 29 | 146 |
| | Compact ($< 7.75 \text{ ft}^3$) | 22 | 155 |

⁴¹⁷ Existing unit consumption is derived from the MwEPA Refrigerator and Freezer Database. Consumption is weighted using appliance characteristics from the 2020 Residential Energy Consumption Survey (RECS) for units greater than 15 years old. Data was only available for units manufactured on or after 1979.

<https://www.energy.gov/scep/wap/articles/refrigerator-and-freezer-energy-rating-online-search-tool>.
<https://www.eia.gov/consumption/residential/data/2020/hc/pdf/HC%203.8.pdf>.

| Freezer type | Product Class | ROB savings (kWh/year) | ER savings (kWh/year) |
|--------------|--|------------------------|-----------------------|
| Upright | Standard (≥ 7.75 ft ³) | 48 | 122 |
| | Compact (< 7.75 ft ³) | 32 | 143 |

8.4.2.3 Deemed Demand Savings Tables

Table 8.4-6: [Freezers] Replace-on-Burnout Demand Savings (kW) by Freezer Type

| Freezer type | Product Class | NCP kW | 4CP kW | CP kW |
|--------------|--|--------|--------|-------|
| Chest | Standard (≥ 7.75 ft ³) | 0.004 | 0.004 | 0.004 |
| | Compact (< 7.75 ft ³) | 0.003 | 0.003 | 0.003 |
| Upright | Standard (≥ 7.75 ft ³) | 0.007 | 0.006 | 0.006 |
| | Compact (< 7.75 ft ³) | 0.005 | 0.004 | 0.004 |

Table 8.4-7: [Freezers] Early Retirement Demand Savings (kW) by Freezer Type

| Freezer type | Product Class | NCP kW | 4CP kW | CP kW |
|--------------|--|--------|--------|-------|
| Chest | Standard (≥ 7.75 ft ³) | 0.022 | 0.019 | 0.019 |
| | Compact (< 7.75 ft ³) | 0.023 | 0.020 | 0.020 |
| Upright | Standard (≥ 7.75 ft ³) | 0.018 | 0.016 | 0.016 |
| | Compact (< 7.75 ft ³) | 0.022 | 0.018 | 0.019 |

1.1.1.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 22 years based on the current DOE Final Rule standards for residential freezers.⁴¹⁸

8.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- ENERGY STAR certificate matching new unit model number

⁴¹⁸ Final Rule: Standards, Federal Register, 76 FR 57516 (Sept. 15, 2011) and associated Technical Support Document. https://www.ecfr.gov/cgi-bin/text-idx?SID=48f64e166fe3561666f871e521996e13&mc=true&node=se10.3.430_132&rgn=div8. Download TSD at: <http://www.regulations.gov/#!documentDetail;D=EERE-2008-BT-STD-0012-0128>.

- Unit quantity
- Baseline type (new construction, replace-on-burnout, or early retirement)
- Freezer type (upright or chest)
- Freezer size (standard or compact)
- Photograph demonstrating functionality of existing equipment and/or customer responses to survey questionnaire documenting the condition of the replaced unit and their motivation for measure replacement for early retirement eligibility determination (early retirement only)
- The installer will provide documentation of proper disposal of freezers in accordance with applicable federal, state, and local regulations (early retirement only)
- Proof of purchase – with date of purchase and quantity
 - Alternative: photo of unit installed or another pre-approved method of installation verification

Document Revision History

Table 8.4-8: [Freezers] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated early retirement age eligibility. |
| FY 2026 | Updated early retirement age eligibility and weighting using latest RECS data. Updated resulting early retirement savings tables. Clarified upcoming federal standard. |

8.5 REFRIGERATOR/FREEZER RECYCLING

8.5.1 Measure Description

This measure involves the early retirement and recycling of an existing, full-size (7.75 ft³ or greater) refrigerator and/or freezer in a residential application. Savings represent the estimated energy consumption of the existing unit over its remaining life.

8.5.1.1 Eligibility Criteria

This measure applies to operable primary and secondary retired refrigerators/freezers. Recycling savings for this measure are limited to the removal and recycling of a working refrigerator/freezer from the electrical grid and differ from the savings for a new ENERGY STAR refrigerator/freezer. To qualify, the customer must release the existing unit to the utility or utility representative to ensure proper disposal in accordance with applicable federal, state, and local regulations.

8.5.1.2 Baseline Condition

Without program intervention, the recycled refrigerator/freezer would have remained operable on the electrical grid. As a result, the baseline condition is continued operation of the existing refrigerator.

8.5.1.3 High-Efficiency Condition

There is no efficiency standard for a recycling measure because the energy efficient action is the removal of an operable appliance, not—as with most demand-side management programs—the installation of a higher efficiency model.

8.5.2 Energy and Demand Savings Methodology

Savings for this measure are based on the assumed annual energy consumption of the refrigerator/freezer being retired.

8.5.2.1 Savings Algorithms and Input Variables

Energy Savings

Demand savings can be derived by using the following:

$$\text{Energy Savings } [\Delta kWh] = kWh_{existing} - ISAF \times PUF$$

Equation 8.5-1

Where:

$kWh_{existing}$ = Average annual energy consumption⁴¹⁹; see Table 8.5-1.

$ISAF$ = In Situ Adjustment Factor⁴²⁰ = 0.942.

⁴¹⁹ ENERGY STAR Flip Your Fridge Calculator. <https://www.energystar.gov/index.cfm?fuseaction=refrig.calculator>.

⁴²⁰ The Cadmus Group, Inc. "Residential Retrofit High Impact Measure Evaluation Report." Prepared for California Public Utilities Commission Energy Division. February 8, 2010. Factor to account for variation between site conditions and controlled DOE testing conditions (90°F test chamber, empty refrigerator and freezer cabinets, and no door openings). Appliances in warmer climate zones use more energy than those in cooler climate zones; utilized Southern California Edison data (highest percentage of warm climate projects) to best approximate Texas climate, p. 139-140.

$$PUF = \text{Part Use Factor}^{421} = 0.915.$$

Table 8.5-1: [Refrigerator/Freezer Recycling] Average Annual Energy Consumption

| Total Capacity (ft ³) | Year Manufactured | kWh _{existing} by Freezer Configuration | | | | |
|-----------------------------------|-------------------|--|--------|-------|---------|-------|
| | | Top | Bottom | Side | Upright | Chest |
| < 16.5 | ≤ 2000 | 861 | 962 | 1,139 | 937 | 532 |
| | 2001-2010 | 556 | 724 | 747 | 713 | 435 |
| | ≥ 2011 | 374 | 483 | 592 | 449 | 292 |
| 16.5-18.9 | ≤ 2000 | 962 | 1,051 | 1,266 | 1,058 | 621 |
| | 2001-2010 | 613 | 747 | 818 | 805 | 508 |
| | ≥ 2011 | 412 | 517 | 640 | 507 | 341 |
| 19.0-21.4 | ≤ 2000 | 1,031 | 1,110 | 1,329 | 1,138 | 680 |
| | 2001-2010 | 651 | 762 | 854 | 866 | 557 |
| | ≥ 2011 | 438 | 539 | 664 | 545 | 373 |
| 21.5-24.4 | ≤ 2000 | 1,090 | 1,172 | 1,368 | 1,194 | 721 |
| | 2001-2010 | 683 | 777 | 876 | 909 | 591 |
| | ≥ 2011 | 459 | 562 | 679 | 572 | 396 |
| ≥ 24.5 | ≤ 2000 | 1,223 | 1,347 | 1,528 | 1,355 | 840 |
| | 2001-2010 | 758 | 822 | 966 | 1,031 | 688 |
| | ≥ 2011 | 508 | 627 | 740 | 648 | 461 |

⁴²¹ Ibid. Factor to account for the number of refrigerators that were running, running part time, or not running at the time of recycling, p. 142-143 (weighted by representative utility survey participation, p. 117).

Demand Savings

Demand savings can be derived by using the following:

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{\text{savings}}}{AOH} \times DF$$

Equation 8.5-2

Where:

AOH = Annual operating hours = 8,760 hours.

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.5-2.

Table 8.5-2: [Refrigerator/Freezer Recycling] Demand Factors⁴²²

| Peak Type | DF |
|-----------|-------|
| NCP | 1.325 |
| CP | 1.134 |
| 4CP | 1.155 |

8.5.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

8.5.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

1.1.1.5 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 8 years for refrigerator and freezer recycling, representing the assumed remaining useful life of the retired unit.⁴²³

8.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Unit quantity

⁴²² US Department of Energy's Building America B10 Benchmark load profiles for refrigerators.

⁴²³ KEMA, Inc. "Residential Refrigerator Recycling Ninth Year Retention Study." Prepared for Southern California Edison. July 22, 2004.

- Manufacture year for removed unit(s)
- Total unit capacity (ft³)
- Freezer configuration (top, bottom, side-by-side, upright, chest)

Document Revision History

Table 8.5-3: [Refrigerator/Freezer Recycling] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

8.6 ENERGY STAR® AIR PURIFIERS

8.6.1 Measure Description

This measure applies to the installation of an ENERGY STAR air purifier. This measure applies to existing homes and new construction.

8.6.1.1 Eligibility Criteria

This measure applies to ENERGY STAR-certified floor, tabletop, and wall-mounted air purifiers/room air cleaners.

8.6.1.2 Baseline Condition

The baseline condition is the current federal standard Tier 1 requirements, effective August 9, 2023, with compliance enforced as of December 31, 2023. The standard will increase to Tier 2 requirements on December 31, 2025.⁴²⁴

Table 8.6-1: [Air Purifiers] Federal Standard

| Smoke CADR | Tier 1 CADR/W | Tier 2 CADR/W |
|------------|---------------|---------------|
| 30-99 | 1.7 | 1.9 |
| 100-149 | 1.9 | 2.4 |
| 150+ | 2.0 | 2.9 |

8.6.1.3 High-Efficiency Condition

The table below displays the ENERGY STAR Final Version 2.0 specification for eligible air cleaners, effective October 17, 2020 and revised May 2022.⁴²⁵ Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

Table 8.6-2: [Air Purifiers] ENERGY STAR Specification

| Smoke CADR | Minimum CADR/W |
|------------|----------------|
| 10-99 | 1.9 |
| 100-149 | 2.4 |

⁴²⁴ DOE minimum efficiency standard for residential air cleaners.
https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=77.
<https://www.energy.gov/sites/default/files/2023-03/air-cleaners-ecs-dfr.pdf>.

⁴²⁵ ENERGY STAR® Program Requirements for Room Air Cleaners.
https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%202.0%20Room%20Air%20Cleaners%20Specification%20%28Rev.%20May%202022%29_0.pdf.

| Smoke CADR | Minimum CADR/W |
|------------|----------------|
| 150+ | 2.9 |

8.6.2 Energy and Demand Savings Methodology

Energy savings for this measure were derived using the ENERGY STAR® Appliance Savings Calculator and the revised ENERGY STAR specification in Table 8.6-2.⁴²⁶ Default baseline standby power and clean air delivery rate (CADR) efficiency (CADR/W) values were taken from the ENERGY STAR calculator. ENERGY STAR standby power, CADR, and CADR/W are averages from the ENERGY STAR qualified product listing. Baseline CADR is assumed to be equivalent to ENERGY STAR® CADR.

This measure will be updated to comply with the latest available ENERGY STAR specification and appliance calculator. It will also periodically be updated to comply with the latest updates to the ENERGY STAR qualified product listing.

8.6.2.1 Savings Algorithms and Input Variables

Energy Savings

Energy savings can be derived by using the following:

$$\text{Energy Savings } [\Delta kWh] = (kWh_{conv,OP} + kWh_{conv,SB}) - (kWh_{ES,OP} + kWh_{ES,SB})$$

Equation 8.6-1

$$kWh_{baseline,OP} = \frac{\left(\frac{CADR_{conv}}{Eff_{conv}}\right)}{1,000} \times \text{hours} \times \text{days}$$

Equation 8.6-2

$$kWh_{baseline,SB} = (8,760 - \text{hours} \times \text{days}) \times \frac{W_{conv,SB}}{1,000}$$

Equation 8.6-3

$$kWh_{ES,OP} = \frac{\left(\frac{CADR_{ES}}{Eff_{ES}}\right)}{1,000} \times \text{hours} \times \text{days}$$

Equation 8.6-4

$$kWh_{ES,SB} = \frac{8,760 - \text{hours} \times \text{days} \times W_{ES,SB}}{1,000}$$

Equation 8.6-5

⁴²⁶ ENERGY STAR® Appliance Savings Calculator (updated October 2016). <https://www.energystar.gov/buildings/facility-owners-and-managers/existing-buildings/save-energy/purchase-energy-saving-products>.

Where:

| | | |
|-----------------|---|--|
| $kWh_{conv,OP}$ | = | Conventional operating energy usage. |
| $kWh_{conv,SB}$ | = | Conventional standby energy usage. |
| $kWh_{ES,OP}$ | = | ENERGY STAR operating energy usage. |
| $kWh_{ES,SB}$ | = | ENERGY STAR standby energy usage. |
| $CADR_{conv}$ | = | Conventional unit clean air delivery rate [ft^3/min], assume equivalent to $CADR_{ES}$. |
| $CADR_{ES}$ | = | ENERGY STAR unit clean air delivery rate [ft^3/min], see Table 8.6-2. |
| Eff_{conv} | = | Conventional clean air delivery efficiency = 1.0 CFM/W. |
| Eff_{ES} | = | ENERGY STAR clean air delivery efficiency, see Table 8.6-2. |
| hours | = | Average operating hours per day = 16. |
| days | = | Average days per year = 365. |
| $W_{conv,SB}$ | = | Conventional model standby power = 1.0 W. |
| $W_{ES,SB}$ | = | ENERGY STAR model standby power = 0.6 W. |
| 1,000 | = | Constant to convert from watts to kilowatts. |
| 8,760 | = | Total hours per year. |

Demand Savings

Demand savings can be derived by using the following:

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{savings}}{\text{hours} \times \text{days}} \times DF$$

Equation 8.6-6

Where:

| | | |
|------|---|---|
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.6-3. |
|------|---|---|

Table 8.6-3: [Pool Pumps] Demand Factors⁴²⁷

| Peak Type | DF |
|-----------|-------|
| NCP | 1.078 |
| CP | 0.644 |

⁴²⁷ US Department of Energy's Building America B10 Benchmark load profiles for pool pumps. The profile used to determine demand factors is calculated as the difference of single speed and variable speed profiles. Summer profiles include April through September.

| Peak Type | DF |
|-----------|-------|
| 4CP | 0.702 |

8.6.2.2 Deemed Energy Savings Tables

Table 8.6-4: [Air Purifiers] Energy Savings

| Smoke CADR Range (CFM) | Representative CADR | ENERGY STAR QPL Average Smoke CADR/W | Energy Savings (kWh) |
|------------------------|---------------------|--------------------------------------|----------------------|
| 10-99 | 75 | 3.0 | 115 |
| 100-149 | 129 | 4.3 | 222 |
| 150-199 | 171 | 4.6 | 284 |
| 200-249 | 225 | 4.4 | 363 |
| 250-299 | 275 | 5.7 | 522 |
| 300+ | 375 | 5.5 | 699 |

8.6.2.3 Deemed Demand Savings Tables

Table 8.6-5: [Air Purifiers] Demand Savings

| CADR Range (CFM) | NCP | CP | 4CP |
|------------------|-------|-------|-------|
| 10-99 | 0.021 | 0.013 | 0.014 |
| 100-149 | 0.041 | 0.024 | 0.027 |
| 150-199 | 0.053 | 0.031 | 0.034 |
| 200-249 | 0.067 | 0.040 | 0.044 |
| 250-299 | 0.096 | 0.058 | 0.063 |
| 300+ | 0.129 | 0.077 | 0.084 |

1.1.1.6 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 9 years for air purifiers, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID RES-AirCleaner.⁴²⁸

⁴²⁸ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

8.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- ENERGY STAR certificate matching new unit model number
- Unit quantity
- Smoke clean air delivery rate (CADR) in ft³/min (CFM)
- Proof of purchase with date of purchase, quantity, and model
 - Alternative: photo of unit installed or other pre-approved method of installation verification

Document Revision History

Table 8.6-6: [Air Purifiers] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated baseline to Tier 1 federal standard. |
| FY 2026 | No revision. |

8.7 ENERGY STAR® POOL PUMPS

8.7.1 Measure Description

This measure involves the replacement of a single-speed pool pump with an ENERGY STAR-certified variable-speed or multi-speed pool pump.

8.7.1.1 Eligibility Criteria

This measure applies to all residential applications of in-ground pools or above-ground pools. Pools that serve multiple tenants in a common area are not eligible for this measure. Ineligible pump products include waterfall, integral cartridge filter, integral sand filter, storable electric spa, and rigid electric spa.⁴²⁹

Multi-speed pool pumps are an alternative to variable speed pumps. The multi-speed pump uses an induction motor that functions as two motors in one, with full-speed and half-speed options. Multi-speed pumps may enable significant energy savings. However, if the half-speed motor is unable to complete the required water circulation task, the larger motor will operate exclusively. Having only two speed-choices limits the ability of the pump motor to fine-tune the flow rates required for maximum energy savings.⁴³⁰ Therefore, multi-speed pumps must have a high-speed override capability to revert to low speed after a period not to exceed 24 hours.

8.7.1.2 Baseline Condition

The baseline is assumed to be a new pool pump that is compliant with the current federal standard, effective July 19, 2021.⁴³¹ Weighted energy factor (WEF) requirements are based on rated hydraulic horsepower (hhp).

Table 8.7-1: [Pool Pumps] Baseline Condition

| Pump subtype | Size class | WEF |
|--|-------------------------------|------------------------------|
| Self-priming (inground) pool pumps | Extra Small (hhp ≤ 0.13) | WEF = 5.55 |
| | Small (hhp > 0.13 to < 0.711) | WEF = -1.30 x ln(hhp) + 2.90 |
| | Standard (hhp ≥ 0.711) | WEF = -2.30 x ln(hhp) + 6.59 |
| Non-self-priming (above ground) pool pumps | Extra Small (hhp ≤ 0.13) | WEF = 4.60 |
| | Standard size (hhp > 0.13) | WEF = -0.85 x ln(hhp) + 2.87 |

⁴²⁹ These product types are excluded by the ENERGY STAR specification.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.1%20Pool%20Pumps%20Final%20Specification_0.pdf.

⁴³⁰ Hunt, A. & Easley, S., 2012, "Measure Guideline: Replacing Single-Speed Pool Pumps with Variable Speed Pumps for Energy Savings." Building America Retrofit Alliance (BARA), U.S. DOE. May 2012. <http://www.nrel.gov/docs/fy12osti/54242.pdf>.

⁴³¹ Federal standard for dedicated-purpose pool pumps. https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=67.

8.7.1.3 High-Efficiency Condition

The high-efficiency condition is a 1 to 5 hp variable speed pump (VSP) or multi-speed pool pump that is compliant with the ENERGY STAR Final Version 3.1 Requirements for pool pumps effective July 19, 2021.⁴³² Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

Additional optional efficiency standards are available, aligning with recommendations from the Consortium for Energy Efficiency (CEE) residential swimming pool pump specification, effective October 21, 2020.⁴³³ For all in-ground pumps, CEE Tier 1 matches the current federal standard, and CEE Tier 2 matches the current ENERGY STAR specification for in-ground standard size pumps. Additional savings are only specified for CEE tiers where there is an incremental efficiency improvement above the ENERGY STAR specification.

Compliance only needs to be verified against the CEE specification when claiming CEE savings that exceed the corresponding ENERGY STAR savings values. ENERGY STAR savings should be claimed for all pumps where CEE compliance is not verified and where there are no CEE savings specified.

⁴³² ENERGY STAR Pool Pumps Final Version 3.1 Program Requirements.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.1%20Pool%20Pumps%20Final%20Specification_0.pdf.

⁴³³ CEE Residential Swimming Pool Pump Specification.

https://cee1.org/images/pdf/CEE_ResSwimmingPoolPump_Specification_21Oct2020.pdf.

Table 8.7-2: [Pool Pumps] High-Efficiency Condition

| Pump Subtype | Size Class | ENERGY STAR | CEE Tier 1 | CEE Tier 2 |
|--|-------------------------------|------------------------------|------------------------------|------------------------------|
| Self-priming (inground) pool pumps | Extra Small (hhp ≤ 0.13) | WEF ≥ 13.40 | — | — |
| | Small (hhp > 0.13 to < 0.711) | WEF ≥ -2.45 x ln(hhp) + 8.40 | WEF ≥ -1.30 x ln(hhp) + 4.95 | WEF ≥ -2.83 x ln(hhp) + 8.84 |
| | Standard (hhp ≥ 0.711) | | WEF ≥ -2.30 x ln(hhp) + 6.59 | WEF ≥ -2.45 x ln(hhp) + 8.40 |
| Non-self-priming (above ground) pool pumps | Extra Small (hhp ≤ 0.13) | WEF ≥ 4.92 | — | — |
| | Standard size (hhp > 0.13) | WEF ≥ -1.00 x ln(hhp) + 3.85 | WEF ≥ -1.60 x ln(hhp) + 9.10 | — |

8.7.2 Energy and Demand Savings Methodology

Savings for this measure are based on methods and input assumptions from the ENERGY STAR Pool Pump Savings Calculator.

8.7.2.1 Savings Algorithms and Input Variables

Energy Savings

Energy savings for this measure were derived using the ENERGY STAR Pool Pump Savings Calculator with Texas selected as the applicable location, so Texas-specific assumptions were used.⁴³⁴

$$\text{Energy Savings } [\Delta kWh] = kWh_{base} - kWh_{ES}$$

Equation 8.7-1

Where:

kWh_{base} = Baseline pool pump energy [kWh].

kWh_{ES} = ENERGY STAR variable speed pool pump energy [kWh].

Algorithms to calculate the above parameters are defined as:

$$kWh_{base} = \frac{PFR_{base} \times 60 \times \text{hours} \times \text{days}}{WEF_{base} \times 1,000}$$

Equation 8.7-2

$$kWh_{ES} = \frac{V \times TO \times \text{days}}{WEF_{ES} \times 1,000}$$

Equation 8.7-3

Where:

PFR_{base} = Baseline pump flow rate [gal/min]; see Table 8.7-3.

WEF_{base} = Baseline pump energy factor [gal/W·hr]; see Table 8.7-3.

WEF_{ES} = ENERGY STAR pump energy factor [gal/W·hr]; see Table 8.7-3.

hours = Pump daily operating hours; see Table 8.7-3.

days = Total days per year.

V = Pool Volume = 22,000 gal (default).

TO = Number of turnovers per day; see Table 8.7-4.

⁴³⁴ The ENERGY STAR Pool Pump Savings Calculator, updated February 2013, can be found on the ENERGY STAR website at: <https://www.energystar.gov/productfinder/product/certified-poolpumps/results>.

60 = Constant to convert between minutes and hours.

1,000 = Constant to convert from watts to kilowatts.

Table 8.7-3: [Pool Pumps] Conventional Assumptions

| New Pump (hp) | Reference hhp ⁴³⁵ | hours ⁴³⁶ | PFR _{conv} (gal/min) |
|------------------|------------------------------|----------------------|-------------------------------|
| ≤ 1.25 | 1.0 | 4.9 | 75.5000 |
| 1.25 < hp ≤ 1.75 | 1.5 | 4.7 | 78.1429 |
| 1.75 < hp ≤ 2.25 | 2.0 | 4.1 | 88.6667 |
| 2.25 < hp ≤ 2.75 | 2.5 | 4.0 | 93.0910 |
| 2.75 < hp ≤ 5 | 3.0 | 4.0 | 101.6667 |

Table 8.7-4: [Pool Pumps] ENERGY STAR Assumptions

| New Pump (hp) | V | TO ⁴³⁷ |
|------------------|--------|-------------------|
| ≤ 1.25 | 22,000 | 1.0 |
| 1.25 < hp ≤ 1.75 | | |
| 1.75 < hp ≤ 2.25 | | |
| 2.25 < hp ≤ 2.75 | | |
| 2.75 < hp ≤ 5 | | |

Demand Savings

Demand savings can be derived by using the following:

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{base} - kWh_{ES}}{\text{hours}} \times \frac{DF}{\text{days}}$$

Equation 8.7-4

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.7-5.

⁴³⁵ Hhp not available in ENERGY STAR calculator. Assumed hhp calculated as follows: Ref. horsepower x AF. AF = 0.533 based on ratio of hhp to hp from ENERGY STAR qualified product listing. Accessed 8/11/2023.

⁴³⁶ The daily average operating hours for conventional single-speed pumps, based on 2014 residential pool pump program survey results from CenterPoint Energy.

⁴³⁷ Calculated as TO = hours x 60 x PFR_{base} ÷ V.

Table 8.7-5: [Pool Pumps] Demand Factors⁴³⁸

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.246 |
| 4CP | 0.118 |

8.7.2.2 Deemed Energy Savings Tables

Table 8.7-6: [Pool Pumps] Energy Savings⁴³⁹

| New pump hp | Inground | Above ground |
|--------------------|----------|--------------|
| ENERGY STAR | | |
| ≤ 1.25 | 1,371 | 587 |
| 1.25 < hp ≤ 1.75 | 235 | 657 |
| 1.75 < hp ≤ 2.25 | 262 | 707 |
| 2.25 < hp ≤ 2.75 | 332 | 852 |
| 2.75 < hp ≤ 5 | 509 | 1,229 |
| CEE Tier 1 | | |
| ≤ 1.25 | — | 1,585 |
| 1.25 < hp ≤ 1.75 | — | 1,779 |
| 1.75 < hp ≤ 2.25 | — | 1,935 |
| 2.25 < hp ≤ 2.75 | — | 2,176 |
| 2.75 < hp ≤ 5 | — | 2,642 |
| CEE Tier 2 | | |
| ≤ 1.25 | 1,423 | — |
| 1.25 < hp ≤ 5 | — | — |

⁴³⁸ US Department of Energy's Building America B10 Benchmark load profiles for pool pumps. The profile used to determine demand factors is calculated as the difference of single speed and variable speed profiles. Summer profiles include April through September.

⁴³⁹ The results in this table may vary slightly from results produced by the ENERGY STAR calculator because of rounding of default savings coefficients throughout the measure.

8.7.2.3 Deemed Demand Savings Tables

Table 8.7-7: [Pool Pumps] Demand Savings – Inground Pools⁴⁴⁰

| Rated Pump (hp) | NCP | CP | 4CP |
|--------------------|-------|-------|-------|
| ENERGY STAR | | | |
| ≤ 1.25 | 0.767 | 0.189 | 0.090 |
| 1.25 < hp ≤ 1.75 | 0.137 | 0.034 | 0.016 |
| 1.75 < hp ≤ 2.25 | 0.175 | 0.043 | 0.021 |
| 2.25 < hp ≤ 2.75 | 0.227 | 0.056 | 0.027 |
| 2.75 < hp ≤ 5 | 0.348 | 0.086 | 0.041 |
| CEE Tier 1 | | | |
| All sizes | – | – | – |
| CEE Tier 2 | | | |
| ≤ 1.25 | 0.796 | 0.196 | 0.094 |
| 1.25 < hp ≤ 5 | – | – | – |

Table 8.7-8: [Pool Pumps] Demand Savings – Above Ground Pools⁴⁴¹

| Rated Pump (hp) | NCP | CP | 4CP |
|--------------------|-------|-------|-------|
| ENERGY STAR | | | |
| ≤ 1.25 | 0.328 | 0.081 | 0.039 |
| 1.25 < hp ≤ 1.75 | 0.383 | 0.094 | 0.045 |
| 1.75 < hp ≤ 2.25 | 0.472 | 0.116 | 0.056 |
| 2.25 < hp ≤ 2.75 | 0.583 | 0.143 | 0.069 |
| 2.75 < hp ≤ 5 | 0.842 | 0.207 | 0.099 |
| CEE Tier 1 | | | |
| ≤ 1.25 | 0.886 | 0.218 | 0.105 |
| 1.25 < hp ≤ 1.75 | 1.037 | 0.255 | 0.122 |
| 1.75 < hp ≤ 2.25 | 1.293 | 0.318 | 0.153 |
| 2.25 < hp ≤ 2.75 | 1.490 | 0.367 | 0.176 |
| 2.75 < hp ≤ 5 | 1.810 | 0.445 | 0.214 |
| CEE Tier 2 | | | |
| All sizes | – | – | – |

⁴⁴⁰ Ibid.

⁴⁴¹ Ibid.

1.1.1.7 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for pool pumps, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID OutD-PoolPump.⁴⁴²

8.7.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

For all projects collect:

- Unit quantity
- Manufacturer and model number of new pool pump
- ENERGY STAR certificate matching model number
- Rated pool pump horsepower
- Weighted energy factor of new pool pump
- Rated hydraulic horsepower of new pool pump
- Rated horsepower of new pool pump
- Proof of purchase with date of purchase, quantity, and model
 - Alternative: photo of unit installed or other pre-approved method of installation verification

For a significant sample of projects where attainable (e.g., those projects that are selected for inspection, not midstream or retail programs):

- Items listed for all projects above
- Installation type: ER, ROB, NC
- Rated horsepower of existing pool pump
- Existing and new pool pump operating hours

⁴⁴² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 8.7-9: [Pool Pumps] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated baseline to current federal standard. Added new savings tiers. Updated documentation requirements. |
| FY 2026 | No revision. |

8.8 ADVANCED POWER STRIPS

8.8.1 Measure Description

This measure involves the installation of a multi-plug Advanced Power Strip (APS) that can automatically disconnect specific loads depending on the power draw of a specified or “master” load.

In the case of Tier 1 APS, a load sensor in the strip disconnects power from the control outlets when the master power draw is below a certain threshold. This feature allows for a reduction of power draw from peripheral consumer electronics, which usually maintain some load even when in the off or standby position. Thus, when the master device (e.g., television) is turned off, power supply is cut to other related equipment (e.g., set top boxes, speakers, video game consoles, etc.).

Tier 2 APS use an external sensor paired with a configurable countdown timer to manage both active and standby power loads for controlled devices in a complete system. Tier 2 APS may operate either with or without a master control socket. Those without a master control socket sense power of all devices connected to the controlled sockets; those with a master control socket sense power for the device connected to the control socket. The external sensor of a Tier 2 APS may utilize an infrared-only sensor, or it may utilize a “multi-sensor” which detects both infrared (IR) remote control signals and motion to determine device inactivity and deliver additional savings as compared to a Tier 1 APS device. Both versions of external sensor use IR filtering to prevent inappropriate switching events that may have otherwise resulted from natural interference such as sunlight or CFL light bulbs.

8.8.1.1 Eligibility Criteria

This measure applies to all residential applications. For Tier 2 applications, the APS must control at least two audiovisual devices.

8.8.1.2 Baseline Condition

The baseline condition is assumed to be uncontrolled peripheral loads, each plugged into a traditional surge protector or wall outlet.

8.8.1.3 High-Efficiency Condition

The high-efficiency condition is peripheral loads controlled by a Tier 1 or Tier 2 APS.

8.8.2 Energy and Demand Savings Methodology

8.8.2.1 Savings Algorithms and Input Variables

Savings were developed based on reported plug load electricity consumption and hourly use data. A set of home entertainment and home office peripheral equipment and related performance data are

presented in the following table. “Daily Standby Hours” and “Daily Off Hours” represent the average number of hours the device is left in standby or off mode. For each device, a weighted watt per hour value is calculated based on projected watts consumed in either mode.

There are two savings paths available for Tier 1. Savings can be estimated by:

1. Complete system type (home entertainment or home office)
2. Per APS for an average complete system if the type is unknown

Tier 2 savings are determined using the average component uses for a complete system and an energy reduction percentage.

Table 8.8-1: [APS] Audio Equipment Watt Consumption Breakdown⁴⁴³

| System Type | Peripheral Device | Daily Standby Hours | Daily Off Hours | Standby Power (W) | Off Power (W) | Weighted W/hr | Annual APS Hours |
|--------------------|----------------------------------|---------------------|-----------------|-------------------|---------------|---------------|------------------|
| Home Entertainment | Audio Equipment: AV Receiver | 0.0 | 18.0 | 19.2 | 3.1 | 3.1 | 6,570 |
| | Audio Equipment: Speakers | 0.0 | 18.0 | 3.0 | 0.0 | 0.0 | 6,570 |
| | Audio Equipment: Subwoofer | 0.0 | 18.0 | 7.8 | 0.6 | 0.6 | 6,570 |
| | Media Player: Blu-ray | 2.5 | 20.8 | 7.0 | 0.1 | 0.8 | 8,505 |
| | Media Player: DVD | 2.5 | 20.8 | 5.0 | 2.0 | 2.3 | 8,505 |
| | Media Player: DVD-R | 2.5 | 20.8 | 7.0 | 3.0 | 3.4 | 8,505 |
| | Media Player: DVD/VCR | 2.5 | 20.4 | 8.0 | 4.0 | 4.4 | 8,359 |
| | Media Player: VCR | 2.2 | 21.4 | 6.0 | 3.0 | 3.3 | 8,614 |
| | Set-Top Box: Cable | 0.0 | 16.5 | 25.0 | 16.0 | 16.0 | 6,023 |
| | Set-Top Box: Cable with DVR | 0.0 | 16.5 | 45.0 | 43.0 | 43.0 | 6,023 |
| | Set-Top Box: Satellite | 0.0 | 15.1 | 10.0 | 15.0 | 15.0 | 5,512 |
| | Set-Top Box: Satellite with DVR | 0.0 | 15.1 | 27.0 | 28.0 | 28.0 | 5,512 |
| | Set-Top Box: Stand Alone DVR | 0.0 | 18.3 | 27.0 | 27.0 | 27.0 | 6,680 |
| | Television: CRT | 0.0 | 18.7 | 5.3 | 1.6 | 1.6 | 6,826 |
| | Television: LCD | 0.0 | 18.7 | 2.2 | 0.5 | 0.5 | 6,826 |
| | Television: Plasma | 0.0 | 18.7 | 0.9 | 0.6 | 0.6 | 6,826 |
| | Television: Projection | 0.0 | 18.7 | 4.4 | 7.0 | 7.0 | 6,826 |
| | Video Game Console: Nintendo Wii | 1.5 | 21.4 | 10.5 | 1.9 | 2.5 | 8,359 |
| | Video Game Console: Wii U | 1.5 | 21.4 | 34.0 | 0.4 | 2.6 | 8,359 |

⁴⁴³ Derived from New York State Energy Research and Development Authority (NYSERDA), "Advanced Power Strip Research Report." August 2011.

| System Type | Peripheral Device | Daily Standby Hours | Daily Off Hours | Standby Power (W) | Off Power (W) | Weighted W/hr | Annual APS Hours |
|-------------|-----------------------------------|---------------------|-----------------|-------------------|---------------|---------------|------------------|
| | Video Game Console: PlayStation 2 | 1.5 | 21.4 | 17.0 | 0.2 | 1.3 | 8,359 |
| | Video Game Console: PlayStation 3 | 1.5 | 21.4 | 152.9 | 1.1 | 11.0 | 8,359 |
| | Video Game Console: PlayStation 4 | 1.5 | 21.4 | 137.0 | 6.4 | 14.9 | 8,359 |
| | Video Game Console: XBOX | 1.5 | 21.4 | 68.0 | 2.0 | 6.3 | 8,359 |
| | Video Game Console: XBOX 360 | 1.5 | 21.4 | 117.5 | 3.1 | 10.6 | 8,359 |
| | Video Game Console: XBOX One | 1.5 | 21.4 | 112.0 | 11.9 | 18.4 | 8,359 |

Table 8.8-2: [APS] Home Office Peripheral Watt Consumption Breakdown

| System Type | Peripheral Device | Daily Standby Hours | Daily Off Hours | Standby Power (W) | Off Power (W) | Weighted W/hr | Annual APS Hours |
|-------------|-----------------------|---------------------|-----------------|-------------------|---------------|---------------|------------------|
| Home Office | Computer: Desktop | 4.1 | 16.7 | 11.6 | 3.3 | 4.9 | 7,592 |
| | Computer: Laptop | 4.1 | 16.7 | 7.6 | 4.4 | 5.0 | 7,592 |
| | Computer Monitor: CRT | 2.4 | 16.5 | 7.6 | 1.5 | 2.3 | 6,899 |
| | Computer Monitor: LCD | 2.4 | 16.5 | 1.9 | 1.1 | 1.2 | 6,899 |
| | Computer Speakers | 0.0 | 18.7 | 3.7 | 2.3 | 2.3 | 6,826 |
| | Copier | 0.0 | 23.5 | 2.8 | 1.5 | 1.5 | 8,578 |
| | Fax Machine: Inkjet | 0.5 | 23.3 | 6.0 | 5.3 | 5.3 | 8,687 |
| | Fax Machine: Laser | 0.5 | 23.3 | 5.3 | 2.2 | 2.3 | 8,687 |
| | Printer: Inkjet | 4.4 | 19.5 | 2.5 | 1.3 | 1.5 | 8,724 |
| | Printer: Laser | 4.4 | 19.5 | 9.0 | 3.3 | 4.3 | 8,724 |
| | Scanner | 0.0 | 23.5 | 3.6 | 2.1 | 2.1 | 8,578 |

Energy Savings

Tier 1

Energy and demand savings for a Tier 1 APS in use in a home office or for a home entertainment system are calculated using the following algorithm, where kWh saved are calculated and summed for all peripheral devices:

$$\text{Energy Savings } [\Delta kWh] = \sum \frac{(W_i \times H_i)}{1,000} \times ISR$$

Equation 8.8-1

Where:

| | | |
|-------|---|---|
| W_i | = | Weighted watts per hour consumed in standby/off mode for each peripheral device; see Table 8.8-1. |
| H_i | = | Annual hours per year controlled by the APS; see Table 8.8-1. |
| 1,000 | = | Constant to convert from watts to kilowatts. |
| ISR | = | In-service rate or the percentage of units rebated that are installed, see Table 8.8-3 |

Table 8.8-3: [APS] In-Service Rate

| Program Type | ISR |
|--------------------|------|
| All ⁴⁴⁴ | 0.83 |

Tier 2

The energy and demand savings for Tier 2 APS are obtained using the average household entertainment center and home office component usages, multiplied by an energy reduction percentage.

$$\Delta kWh_{\text{Entertainment Center}} = kWh_{TV} \times ERP \times ISR$$

Equation 8.8-2

$$\Delta kWh_{\text{Computer System}} = kWh_{Comp} \times ERP \times ISR$$

Equation 8.8-3

$$\Delta kWh_{\text{Unspecified Use}} = \frac{kWh_{TV} + kWh_{Comp}}{2} \times ERP \times ISR$$

Equation 8.8-4

⁴⁴⁴ MidAmerican Energy Company & Tetra Tech "Residential Assessment Impact and Process Evaluation FINAL". December 22, 2020, APPENDIX B: IN-SERVICE RATES ANALYSIS, p. 47.

Where:

| | | |
|--------------|---|---|
| kWh_{TV} | = | Average annualized energy consumption of Tier 2 qualifying TV systems, default value of 602.8. ⁴⁴⁵ |
| kWh_{Comp} | = | Average annualized energy consumption of Tier 2 qualifying computer systems, default value of 197.9. ⁴⁴⁶ |
| ERP | = | Energy Reduction Percentage of qualifying Tier 2 APS product range, (default = 47.5%). ⁴⁴⁷ |

Demand Savings

Tier 1 and Tier 2 APS

Demand savings for a Tier 1 APS in use for a home entertainment system or home office are calculated using the following algorithm, where kWh saved is calculated and summed for all peripheral devices. Demand savings for a Tier 2 APS are calculated using the average household home office and home entertainment center usages, multiplied by an assumed energy reduction percentage.

$$\text{Demand Savings } [\Delta kWh] = \sum \frac{\Delta kWh}{H} \times DF$$

Equation 8.8-5

Where:

| | | |
|--------------|---|---|
| ΔkWh | = | Annual energy savings (kWh) for each peripheral device; savings must be adjusted by applying the program specific ISR specified in Table 8.8-3. |
| H | = | Hours per year controlled by the Tier 1 APS; see Table 8.8-1. |
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 8.8-4. |

Table 8.8-4: [APS] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.363 |
| 4CP | 0.202 |

8.8.2.2 Deemed Energy Savings Tables

The savings presented in these tables must be adjusted by applying the program specific ISR values

⁴⁴⁵ New York State Energy Research and Development Authority (NYSERDA) 2011, Advanced Power Strip Research Report, p. 30. August.

⁴⁴⁶ Ibid.

⁴⁴⁷ Average of ERP from Northeast Energy Efficiency Partnerships (NEEP), "Case Study: Tier 2 Advanced Power Strips and Efficiency Programs." April 2015.

specified in Table 8.8-3.

Table 8.8-5: [APS] Unadjusted Tier 1 Energy Savings before applying ISR

| System Type | kWh Savings |
|-----------------------------------|-------------|
| Home Entertainment ⁴⁴⁸ | 269.9 |
| Home Office ⁴⁴⁹ | 87.1 |
| Unspecified System ⁴⁵⁰ | 178.5 |

Table 8.8-6: [APS] Unadjusted Tier 2 Energy Savings before applying ISR

| System Type | kWh Savings |
|--------------------|-------------|
| Home Entertainment | 286.3 |
| Home Office | 94.0 |
| Unspecified System | 190.2 |

8.8.2.3 Deemed Demand Savings Tables

The savings presented in these tables must be adjusted by applying the program specific ISR values specified in Table 8.8-3.

Table 8.8-7: [APS] Unadjusted Tier 1 Demand Savings before applying ISR

| System Type | NCP | CP | 4CP |
|-----------------------------------|-------|-------|-------|
| Home Entertainment ⁴⁵¹ | 0.040 | 0.015 | 0.008 |
| Home Office ⁴⁵² | 0.011 | 0.004 | 0.002 |
| Unspecified System ⁴⁵³ | 0.026 | 0.009 | 0.005 |

Table 8.8-8: [APS] Unadjusted Tier 2 Demand Savings before applying ISR

| System Type | NCP | CP | 4CP |
|----------------------|-------|-------|-------|
| Entertainment Center | 0.065 | 0.024 | 0.013 |
| Computer System | 0.021 | 0.008 | 0.004 |
| Unspecified Usage | 0.043 | 0.016 | 0.009 |

8.8.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for a Tier 1 APS, according to the 2011 NYSEDA Advanced

⁴⁴⁸ Assuming Audio Equipment: AV Receiver, Media Player: Average, Set-Top Box: Average, and Video Game Console: Average.

⁴⁴⁹ Assuming Computer: Desktop, Computer Monitor: LCD, Computer Speakers, Printer: Average.

⁴⁵⁰ Average of Home Entertainment System and Home Office system averages.

⁴⁵¹ Assuming Audio Equipment: AV Receiver, Media Player: Average, Set-Top Box: Average, and Video Game Console: Average.

⁴⁵² Assuming Computer: Desktop, Computer Monitor: LCD, Computer Speakers, Printer: Average.

⁴⁵³ Average of Home Entertainment System and Home Office system averages.

Power Strip Research Report.⁴⁵⁴ While Tier 2 APS is not covered by the NYSERDA report, assume the same 10-year EUL for Tier 2 APS.

8.8.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Unit quantity
- Manufacturer and model number
- APS type (Tier 1 or Tier 2)
- System type (home entertainment, home office, unspecified)
- Proof of purchase - including date of purchase and quantity
 - Alternative: photo of unit installed or another pre-approved method of installation verification.

Document Revision History

Table 8.8-9: [APS] Revision History

| Guidebook version | Description of change |
|-------------------|-------------------------|
| FY 2025 | Added in-service rates. |
| FY 2026 | No revision. |

⁴⁵⁴ New York State Energy Research and Development Authority (NYSERDA), “Advanced Power Strip Research Report”. August 2011. Page 30.

8.9 ENERGY STAR® ELECTRIC VEHICLE SUPPLY EQUIPMENT (EVSE)

8.9.1 Measure Description

This measure applies to the installation of a Level 2 electric vehicle supply equipment (EVSE) at a residential site. EVSE is the infrastructure that enables plug-in electric vehicles (PEV) to charge onboard batteries. Level 2 EVSE require 240-volt electrical service. This measure provides deemed savings for the energy efficiency improvement of an ENERGY STAR EVSE compared to a standard Level 1 EVSE.

8.9.1.1 Eligibility Criteria

Eligible equipment includes ENERGY STAR-qualified⁴⁵⁵ Level 2 EVSE installed at a residence. The EVSE may be installed for use on either an all-battery electric vehicle (BEV) or a plug-in hybrid electric vehicle (PHEV). Multifamily buildings should use the commercial EVSE measure.

8.9.1.2 Baseline Condition

The baseline condition is assumed to be a blend of 49%⁴⁵⁶ Level 1 EVSEs (ENERGY STAR or non-ENERGY STAR) and 51% Level 2 EVSEs. Energy savings are available for the 49% market share of Level 1 EVSEs.

8.9.1.3 High-Efficiency Condition

The high efficiency condition is a Level 2 EVSE compliant with the ENERGY STAR Final Version 1.1 specification for eligible EVSE, effective March 31, 2021.⁴⁵⁷ Energy efficiency service providers are expected to comply with the latest ENERGY STAR requirements.

8.9.2 Energy and Demand Savings Methodology

Savings for this measure are based on efficiency gains of the ENERGY STAR equipment during operating modes when the vehicle is plugged in and charging. Following a study conducted by Frontier Energy, energy savings are established by estimating annual miles driven, average EV fuel economy, and approximate percent (%) of energy savings attributed to charging with ENERGY STAR Level 2 EVSE as opposed to Level 1 EVSE.

⁴⁵⁵ ENERGY STAR EVSE qualified product listing: <https://www.energystar.gov/productfinder/product/certified-evse/results>.

⁴⁵⁶ Calculated as the number of normal power outlets divided by the total number of sampled EV owners for the home category. "Exploring consumer sentiment on electric-vehicle charging", McKinsey & Company. January 9, 2024. Exhibit 2. <https://www.mckinsey.com/features/mckinsey-center-for-future-mobility/our-insights/exploring-consumer-sentiment-on-electric-vehicle-charging>.

⁴⁵⁷ ENERGY STAR Electric Vehicle Supply Equipment Final Version 1.1 Program Requirements. https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20V1.1%20DC%20EVSE%20Final%20Specification_0.pdf.

8.9.2.1 Savings Algorithms and Input Variables

Energy Savings

Table 8.9-1 presents the most common registered EVs in Texas and their corresponding fuel economy to establish an average annual energy per individual affected by this measure.

Table 8.9-1: [RES EVSE] EV Registration by Model – Fuel Economy for EVs in Texas ⁴⁵⁸

| Make | Model | % of Market ⁴⁵⁹ | EPA Fuel Economy [kWh/100mi] ⁴⁶⁰ | Weighted Avg. [kWh/100mi] |
|--------------|----------------|----------------------------|---|---------------------------|
| Tesla | Model 3 | 24.6% | 25 | 6.2 |
| Tesla | Model Y | 22.5% | 27 | 6.1 |
| Tesla | Model S | 6.5% | 28 | 1.8 |
| Tesla | Model X | 4.1% | 32 | 1.3 |
| Chevrolet | Bolt EV/EUV | 3.3% | 29 | 0.8 |
| Ford | Mustang Mach-E | 2.4% | 34 | 1.0 |
| Nissan | Leaf | 2.0% | 31 | 0.6 |
| Volkswagen | ID.4 | 1.3% | 31 | 0.4 |
| Ford | F150 Lightning | 1.1% | 50 | 0.5 |
| Multiple | Multiple | 32.2% | 32 ⁴⁶¹ | 10.3 |
| Total | | 100.0% | – | 29.0 |

$$\text{Annual Energy Consumption [kWh}_c\text{]} = \text{miles} \times \text{WAFE}$$

Equation 8.9-1

$$\text{Annual Energy Savings } [\Delta \text{kWh}] = \text{kWh}_c \times \text{L2\%} \times \text{BAF}$$

Equation 8.9-2

Where:

$$\text{miles} = \text{Average distance driven per year in the U.S.}^{462} [\text{miles}] = 13,476$$

$$\text{WAFE} = \text{Weighted Average Fuel Economy [kWh/mi]} = 0.29 \text{ (see Table 8.9-1: [RES EVSE] EV Registration by Model – Fuel Economy for EVs in Texas)}$$

⁴⁵⁸ EVs in Texas, DFW Clean Cities. <https://www.dfwcleancities.org/evsintexas>.

⁴⁵⁹ All models with less than 1 percent of market share were combined.

⁴⁶⁰ U.S. Department of Energy. <https://www.fueleconomy.gov/>.

⁴⁶¹ Average of EPA fuel economy for models with a higher market share.

⁴⁶² Average Annual Miles per Driver by Age Group, U.S. Department of Transportation Federal Highway Administration. <https://www.fhwa.dot.gov/ohim/ohh00/bar8.htm>.

L2% = *Percent savings achieved by Level 2 EVSE compared to Level 1 EVSE*⁴⁶³ = 10%

BAF = *Baseline Adjustment Factor [%] = 49% (representation of market charging with Level 1 EVSE)*

Demand Savings

8.9.2.2 Demand (kW) savings are not estimated for this measure. Deemed Energy Savings Tables

Table 8.9-2 presents the deemed energy savings per EVSE.

Table 8.9-2: [RES EVSE] Energy Savings⁴⁶⁴

| kWh Savings |
|-------------|
| 191 |

8.9.2.3 Deemed Demand Savings Tables

Not applicable.

8.9.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) for an EVSE is assumed to be 10 years.⁴⁶⁵

8.9.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- ENERGY STAR certificate matching EVSE model number
- EVSE quantity
- Vehicle year, make, and model (if available)

⁴⁶³ "Texas Residential R&D Electrical Vehicle Study", Frontier Energy for AEP Texas. March 2024.

⁴⁶⁴ ENERGY STAR Market and Industry Scoping Report EVSE, September 2013.

https://www.energystar.gov/sites/default/files/asset/document/Electric_Vehicle_Scoping_Report.pdf.

⁴⁶⁵ US Department of Energy Vehicle Technologies Office, November 2015, "Costs Associated with NonResidential Electric Vehicle Supply Equipment" p. 21. https://afdc.energy.gov/files/u/publication/evse_cost_report_2015.pdf.

- Estimated number of miles driven per day (if available)

Document Revision History

Table 8.9-3: [RES EVSE] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated algorithm with days coefficient. Updated documentation requirements. |
| FY 2026 | Updated savings methodology to use a weighted Level 1 and Level 2 baseline. |

9. RESIDENTIAL: NEW CONSTRUCTION

9.1 RESIDENTIAL NEW CONSTRUCTION

9.1.1 Measure Description

This measure involves the inclusion of energy efficient design features in new home construction.

9.1.1.1 Eligibility Criteria

New homes are eligible in the program year in which they are completed. Eligibility is established by building a home whose total source energy use is estimated to be less than that of a home built to International Energy Conservation Code 2021 (IECC 2021) specifications by at least 15 percent.

Builders and homeowners can establish that participating homes meet this target by obtaining a Level 1 certification or higher from Build San Antonio Green. Alternatively, participating homes can document expected savings with simulation software that provides a code compliance report, such as REM/Rate or the International Code Compliance Calculator (IC3) developed and maintained by Texas A&M University's Energy Systems Lab.

9.1.1.2 Baseline Condition

The baseline is established as a home with the same footprint as the as built home but built to the current code in San Antonio according to the requirements of the standard's prescriptive approach to compliance. Effective February 1, 2023, San Antonio adopted IECC 2021 as its current energy code. Efficiency of installed equipment in the baseline home meets the minimum requirements of the federal standards in place in a given program year.

For estimating program savings through building simulation modeling, a reference home model is specified according to the provisions for creating a standard reference design in Section R405 of IECC 2021. Where neither code nor federal manufacturing standards dictate settings for model parameters specified in the reference home, Building America House Simulation Protocols and general knowledge of typical residential sector construction practices are relied upon.

9.1.1.3 High-Efficiency Condition

The high-efficiency condition is the new home as built. CPS Energy's Residential New Construction program promotes a holistic approach to achieving energy efficient homes, including a combination of envelope and equipment-based improvements to reduce home energy use. The energy savings estimations process is designed to efficiently estimate electric energy and demand savings attributable to each participating home.

9.1.2 Energy and Demand Savings Methodology

Savings are achieved by introducing improvements in participating new homes in the following components:

- Building Envelope
- Space Conditioning Equipment
- Domestic Hot Water
- Lighting
- Appliances

Interactions between these various elements confound application of engineering algorithms: therefore, energy and demand savings for the residential new construction measure are estimated by using building simulation modeling.

9.1.2.1 Savings Algorithms and Input Variables

A set of representative models are used: individual participating homes are not modeled for evaluation purposes. These models are built to represent the population of participating homes based on what is known about the techniques being used by participating builders to achieve the program's goals. Builders earning Tier 1 incentives through Build San Antonio Green certification can follow a prescriptive path or a performance path to Level 1 or higher certification. Modeling the prescriptive path is straightforward: the specific requirements for achieving the tiers are specified in the model of the as built home. Builders taking advantage of the performance path also generally apply a standard set of measures. These measures can be simulated: for evaluation of homes submitted via the performance path, evaluation requires development of representative models for each builder.

In addition to variables that are exactly repeated across large numbers of homes, there are some variables for which multiple models will need to be developed to capture the range of possible outcomes:

- Layout: one-story and two-story homes are modeled separately.
- Square Footage: participant homes are binned in 500-square-foot blocks (1,500-2,000 sq. ft., 2,000-2,500, etc.). Achieved Leakage Rate: As this is an outcome, it cannot be pre-determined. Most participating builders are achieving leakage rates between 2 and 4 ACH₅₀. Multiple leakage rates will be applied to representative models to accurately capture the range of savings impacts from the different leakage rates.

Savings are estimated by using load shapes created by simulating the hourly savings for each representative model. Representative model savings are then aggregated to total program savings by

multiplying each load shape's values by the number of homes represented by that model and summing these values across all representative models.

Energy Savings

Energy savings is the difference between the expected annual energy use of the as built participating homes and the simulated energy use of homes built with the same footprints as the participating homes but built strictly to the minimum requirements of current code (IECC 2021), modeled as specified above (see Baseline Condition).

Demand Savings

As with energy savings, demand savings is the difference between simulation results for the as built and the reference home models, except that difference is taken only for the specific hours necessary to identify demand savings according to the definitions of the different demand periods (non-coincident peak, coincident peak, and ERCOT 4CP).

9.1.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy savings.

9.1.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating demand savings.

9.1.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 23 years for residential new construction when reporting whole home savings. Prescriptive savings reported for individual energy efficiency measures should refer to the EUL for each respective measure.

9.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Builder
- Number of stories
- Conditioned floor area (square feet)
- Incentive achieved (Tier 1)

- Participation path
 - BSAG prescriptive path
 - BSAG performance path
 - Other
- Measured air infiltration rate
- Space conditioning equipment type (CAC with gas furnace or heat pump)
 - Capacity (tons)
 - Cooling efficiency (SEER)
 - Heating efficiency (AFUE/HSPF depending on type)
- Water heater:
 - Fuel type (gas/electric)
 - Storage volume (0 if tankless)
 - EF
- High efficacy lighting installed
 - High efficacy lighting as percent of total
 - CFL/LFL as percent of high efficacy lighting
 - LED as percent of high efficacy lighting
- ENERGY STAR appliances installed
- Additional/unusual features (e.g., solar water heater, rooftop solar PV system, etc.)

10. RESIDENTIAL: RENEWABLE ENERGY

10.1 SOLAR PHOTOVOLTAIC

10.1.1 Measure Description

This measure involves the installation of a new or expanded residential grid-connected solar photovoltaic (PV) system.

10.1.1.1 Eligibility Criteria

Only PV systems that result in reductions of the customer's purchased energy and/or peak demand qualify for savings. Off-grid systems are not eligible. CPS Energy maintains additional eligibility criteria for participating in the incentive program.

10.1.1.2 Baseline Condition

PV system not currently installed (typical), or an existing system is present but additional generating capacity is added.

10.1.1.3 High-Efficiency Condition

PV system (or additional capacity on an existing system) is installed and operational.

10.1.2 Energy and Demand Savings Methodology

10.1.2.1 Savings Algorithms and Input Variables

Energy and demand savings are derived from meter-based savings validation of CPS Energy's fleet of residential solar energy systems conducted by Frontier Energy in 2021.

Energy Savings

Based on Frontier's 2021 analysis of CPS Energy's residential solar fleet, CPS Energy uses an average annual performance factor of 1,324 kWh per kW_{DC} per year for residential solar energy systems.⁴⁶⁶ Thus,

$$\text{Energy Savings } [\Delta kWh] = 1,324 \times kW_{DC} \text{ installed}$$

Equation 10.1-1

⁴⁶⁶ Evaluation, Measurement and Verification of CPS Energy's FY 2015 DSM Programs, June 11, 2015, Frontier Associates.

Where:

$$kW_{DC} = \text{Sum of the DC capacity at standard test conditions (STC) of all PV modules installed (or additional capacity installed on existing system). This factor may be reassessed periodically and updated if the composition of installed projects is determined to vary substantially from the assumed fleet-wide average.}$$

The annual energy savings performance factor was derived from solar AMI data for residential systems installed from 2017 through 2020. The table below lists the percentage of annual kWh applied to each avoided cost period.

Table 10.1-1: [RES Solar PV] Solar Initiative Allocation of Annual kWh Savings into Avoided Cost Periods

| Load Shape Category | Summer On Peak | Summer Mid Peak | Summer Off Peak | Non-Summer Mid Peak | Non-Summer Off Peak |
|---------------------|----------------|-----------------|-----------------|---------------------|---------------------|
| Residential Solar | 12.21% | 25.95% | 0.23% | 42.72% | 18.89% |

10.1.2.2 Deemed Energy Savings Tables

This section is not applicable for this measure.

10.1.2.3 Deemed Demand Savings Tables

Frontier’s 2021 analysis of CPS Energy’s residential solar fleet produced estimated average performance factors for non-coincident peak (NCP), coincident peak (NCP), and ERCOT TCOS 4CP demand savings. These performance factors were determined by subjecting the residential fleet-wide 8,760 hourly load shape to methods for determining each demand metric:

- Non-Coincident Peak (NCP): CPS Energy uses a non-coincident peak factor of 104.6% (or 1.046) of the total array DC capacity at standard test conditions (STC). This factor represents the maximum hourly kW_{AC} value over the 8,760-hour TMY period, regardless of when it occurred.

$$\text{Non-Coincident Peak (NCP) savings} = 1.046 \times kW_{DC}$$

Equation 10.1-2

- Coincident Peak (CP): CPS Energy uses a coincident peak factor of 43.3% (or 0.433) of the total array DC capacity at standard test conditions (STC). This factor is calculated as the probability-weighted average kW_{AC} output of a one (1) kW_{DC} “fleet average” residential array over the top 20 hours in a blended TMY weather file determined to be the most likely to coincide with CPS Energy’s peak.

$$\text{Coincident Peak (CP) savings} = 0.433 \times kW_{DC}$$

Equation 10.1-3

- ERCOT TCOS 4CP: CPS Energy uses an ERCOT TCOS 4CP factor of 36.4% (or 0.364) of the total array DC capacity at standard test conditions (STC). This factor is calculated as the average demand savings of a one (1) kW_{DC} “fleet average” residential array during 20 recent 4CP intervals.

$$ERCOT\ TCOS\ 4CP\ savings = 0.364 \times kW_{DC}$$

Equation 10.1-4

10.1.2.4 Claimed Peak Demand Savings

This section is not applicable for this measure.

10.1.2.5 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 30 years for solar PV. This value is consistent with engineering estimates based on manufacturers' warranties and historical data, and with the EUL reported in the Texas Technical Reference Manual (TRM).

10.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Project location (city) and zip code
- Module type: Standard, premium, or thin film
- Array Type: Fixed (open rack), fixed (roof mount), 1-axis tracking, 1-axis backtracking, 2-axis tracking, etc.
- Tilt, azimuth, and DC system size rating at standard test conditions for each array
- Date of PVWatts® run, and PVWatts® report (retained with project documentation) for each array

10.1.4 Document Revision History

Table 10.1-2 [RES Solar PV] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

11. RESIDENTIAL: DEMAND RESPONSE/LOAD CONTROL

11.1 RESIDENTIAL DEMAND RESPONSE

11.1.1 Measure Description

Residential demand response (DR) measures include technologies or programs that enable CPS Energy to reduce aggregate residential customer demand to respond to an electric system need. Most commonly, these technologies include controlling thermostats, but may also include controllers for water heaters, pool pumps, room air conditioners, EVs, or other residential loads at the end-user level. There is also a behavioral demand response program covering residential houses that are not in direct load control residential programs. Instead of controlling thermostats or other devices, email and phone call notifications are sent to participants in advance of each event. Participants can also receive a utility bill credit for avoiding EV charging during on-peak time.

11.1.1.1 Eligibility Criteria

Any residential customer with an eligible control technology who is actively enrolled in one of CPS Energy's residential demand response programs. These programs and eligible control technologies/program included the following:

Table 11.1-1: [RES DR] Programs and Eligible Control Technologies

| Program | Eligible Control Technology/Program |
|---|---|
| Smart Thermostat | Any of several eligible Honeywell thermostats provided and installed by CPS Energy |
| Wi-Fi Thermostat Rewards (or: Bring Your Own Thermostat (BYOT)) | <p>Any of several eligible thermostats directly purchased by the customer and installed by the customer</p> <ul style="list-style-type: none">• Nest 1st, 2nd, 3rd generation or Nest Thermostat E• Honeywell D6 Pro, FocusPro® (WiFi 6000), VisionPro (WiFi 8000), WiFi 9000, Lyric Round, T5 or T6, Honeywell Home T9, Honeywell Home T10• ecobee Smart, ecobee3, ecobee 3 lite, ecobee 4• Emerson Sensi Wi-Fi Thermostat, Emerson Sensi Touch Wi-Fi Thermostat• Alarm.com Radio Thermostat CT-30, CT-80, CT-100, Trane ComfortLink Control, Alarm.com Smart Thermostat• Building36 Intelligent Thermostat• Radio Thermostat CT-30 (WiFi), CT-50 (WiFi), CT-80 (WiFi)• Filtrete™ 3M-50 (WiFi)• Lux Products GEO• Vivint Radio Thermostat CT100 with Vivint Go!Control Panel |
| Direct Install Thermostats | Currently offering 3 rd generation Google Nest, Emerson Sensi, and ecobee thermostats. |

| Program | Eligible Control Technology/Program |
|--|--|
| Reduce My Use/Behavioral Demand Response (BDR) | No device needed; an opt-out randomized control trial (RCT) for residential homes |
| FlexEV OffPeak Rewards | All participating level 2 EV chargers. Currently, eligible level 2 EV chargers only include Chargepoint and Enel X chargers. |
| FlexEV Smart Rewards | All participating level 2 EV chargers. Currently, eligible level 2 EV chargers only include Chargepoint and Enel X chargers. |

11.1.1.2 Baseline Condition

Customer not enrolled in a residential demand response program.

11.1.1.3 High-Efficiency Condition

Customer enrolled in a residential demand response program.

11.1.2 Energy and Demand Savings Methodology

11.1.2.1 Savings Algorithms and Input Variables

Demand and Energy Savings

Energy (kWh) and demand (kW) savings for FY 2022 and forward residential DR programs will be estimated using actual AMI or device-level 15-minute interval consumption data. Specifically, for each residential DR program, savings will be estimated as described in the following sections.

My Thermostat Rewards Bring Your Own Thermostat (BYOT) Program

Nest, Honeywell, ecobee, Emerson, and Other Thermostats on EnergyHub and Resideo Platforms

Actual aggregated 15-minute interval device-level data stratified by thermostat type from June to September will be used for quantifying thermostat device-level kW demand reduction for residential DR events.

Savings analyses are conducted in the following steps:

Step 1: convert CPS residential DR dashboard interval consumption data into average per device basis and convert AMI raw interval data into average per account basis by each category. Specifically, for each category on residential DR dashboard, divide aggregated interval kW by the corresponding device count, yielding average per device kW. Take the mean kWh of each interval and multiply by 4 for each category, yielding average per account kW for small commercial AMI data customers.

Step 2: for each event, utilize two methodologies - temperature-based regression and CPS “top 3 of 10”

analysis, and select the methodology with the lowest RMSE during “test period”.

Specifically, for each event, use the event day with the previous 10 eligible days, and use the 11 total days to conduct the following procedures:

- (1) Regression: Average per device/account kW is modeled as a function of an event dummy variable indicating whether a time period is within the event period, a precool dummy variable indicating whether a time period is within the 1-hour precool period before each event⁴⁶⁷, a snapback dummy variable indicating whether a time period is within the 2-hour snapback period right after each event, a cdh (cooling degree hours, with balance point set as 65 °F) variable, a cdh-squared (cooling degree hours squared, to account for non-linear relationship between temperature and load to some extent) variable, and three time-of-day dummy variables indicating time of day – 0:00-6:00, 6:00-12:00, 12:00-18:00 or 18:00-24:00. The model equation can be expressed as follows:

$$kW_t = \beta_0 + \beta_1 \times event_t + \beta_2 \times precool_t + \beta_3 \times snapback_t + \beta_4 \times cdh_t + \beta_5 \times cdh_t^2 + \sum_{i=6}^8 \beta_i \times time - of - day_t$$

$-\beta_1$ is the estimated kW load reduction per device/account during a certain event with regression method. Similarly, β_2 is the estimated kW precool, and β_3 is the estimated kW snapback per device during a certain event. Net energy savings (kWh) per device/account is calculated as $-\beta_1 \times \text{event duration} - \beta_2 - \beta_3 \times 2 \text{ hours}$.

- (2) CPS Energy’s high 3-of-10 baseline analysis: This methodology ranks the last ten eligible days based on total kWh during the event period. The three days with the highest kWh during the event period are selected. These three days are then averaged for each interval to create a calculated baseline. An adjustment ratio to the calculated baseline is applied to factor in weather effects and customer operation levels on the event day. In this case, adjustment ratio is calculated as the ratio between the average kW of the event day and the three baseline days during the 1-hour adjustment window immediately preceding the precool period or event period (if there is no precool period). The average kW difference during the event period is the estimated kW savings. The kWh difference during the combination of 1-hour precool period, event period, and 2-hour snapback period is the estimated net kWh savings.
- (3) Compare the RMSE (root mean square error) of these two analyses during test period, and select the results generated by the methodology with the lower RMSE. Here, “test period” consists of four separate periods. The first three periods are the event time periods during the “top previous 3 days” (i.e., the three baseline days illustrated in the “high 3-of-10 baseline analysis” section above); the last period is 10:00 am – 2:00 pm during event day. Multiplying per device kW savings by number of end-of-year (EOY) enrolled devices yields EOY kW savings.

Meanwhile, the previous time temperature matrix developed by Frontier will still be used for

⁴⁶⁷ Precool dummy variable only existed in the regression model for Resideo platform WiFi thermostats. There was no obvious precooling consumption pattern for traditional cycling thermostats and this dummy variable was therefore not included.

calculations, simply as a reference and for comparison.

To estimate year-round energy conservation savings attributable to the installation of Nest and ecobee thermostats, Frontier will refer to the deemed savings estimate in Guidebook section 5.7, since Nest thermostat is one of the ENERGY STAR-certified thermostat brands.

Smart Thermostat Program

In FY 2024, all thermostats in the Smart Thermostat program are categorized by dwelling type and cycling strategy as follows:

Table 11.1-2: [RES DR] Smart Thermostat Dwelling Thermostat Type

| Thermostat type | Dwelling type | Cycling strategy |
|-----------------|---------------|------------------|
| Pager | Residential | 33% |
| | | 50% |
| | Commercial | 33% |
| | | 50% |
| Wi-Fi | Residential | Resideo |
| | Commercial | Resideo |

Like the kW savings estimation process for BYOT thermostats, actual aggregated 15-minute interval device-level or AMI data stratified by dwelling type and cycling strategy from June to September will be used for quantifying per-device or per-AMI account level kW demand reduction for Smart Thermostat residential DR events. For each event day, the savings analysis is conducted in the same manner as those thermostats in the BYOT program. Multiplying per device kW savings by number of EOY enrollment devices yields EOY kW savings.

Multiplying kW savings by DR event duration (unit: hours) yields gross energy savings. Subtracting potential over-consumption during the pre-cooling or snapback period (if any) from gross energy savings yields net energy savings.

Like some of the thermostats in the BYOT program, previously developed temperature bins for the Smart Thermostat program will be used for reference or comparison calculation.

Direct Install Thermostats Program

Because these thermostats operate in an equivalent manner to those thermostats of the same brand employed in the BYOT program, demand and energy savings attributable to thermostats deployed within the Direct Install Thermostats Program used the same methodology described for the BYOT program.

Reduce My Use/Behavioral Demand Response (BDR)

CPS Energy partnered with Opower to implement a pilot behavioral demand response (BDR) program for residential customers beginning in summer 2017. This program was implemented as an opt-out randomized controlled trial (RCT). These participated households were all equipped with AMI meters and did not participate in other CPS Energy DR programs.

Every year, some residential customers are recruited into either treatment group or control group. Each year of new recruitment is called a “wave.” To this point, there are seven waves – 2017 - 2023 wave, one wave for each year. Treatment group participants receive a welcome letter in May before the program starts each summer. One day before each event day or on the same day before each event, participants receive a notification message through email and phone call. This notification also contains information explaining what a peak day is and personalized energy conservation tips. After each event, customers receive a follow up call. Two weeks later, personalized customer performance feedback is also provided to participants.

A simple difference method is employed for each of the four waves, i.e., savings are estimated as the simple difference between control group and treatment group for each event for this wave:

$$\begin{aligned} kW \text{ savings per participant} \\ = \text{control group } kW \text{ per participant} - \text{treatment group } kW \text{ per participant} \end{aligned}$$

FlexEV Rewards Programs

CPS Energy launched two pilot EV charging demand response programs starting June 2021: the FlexEV Smart Rewards program and the FlexEV Off-Peak Rewards program. Customers with an eligible⁴⁶⁸ level 2 EV charger can choose to sign up for either program.

FlexEV Smart Rewards Program

For the FlexEV Smart Rewards program, CPS Energy can make remote adjustments to participating EV chargers during the event period. EV chargers can either be turned off or reduced to level 1 charging (charging rate no higher than 1.8 kW). Events can be called from 2-9 pm during weekdays throughout the year. In return, customers receive a \$250 utility bill credit and a \$5 monthly credit while they remain enrolled in the program.⁴⁶⁹ The FlexEV Smart Rewards program events can help soften snap-back from thermostat events (usually around 3-6 pm), as EV charging tends to begin coincidentally with the end of thermostat DR events (usually around 6-7 pm).

Savings analyses are conducted in the following steps:

Step 1: Plot aggregated average non-event day device-level load profile by month to have a brief visual inspection on whether there were any significant EV charging behavioral changes throughout the program throughout the whole fiscal year. We then assume all non-event weekdays can serve as eligible

⁴⁶⁸ Currently, eligible level 2 EV chargers only include Chargepoint and Enel X chargers. The full list of eligible model numbers can be found here: <https://www.chargingrewards.com/faqs/cpsenergy/>.

⁴⁶⁹ <https://www.cpsenergy.com/en/about-us/programs-services/electric-vehicles/ev-charging-solutions.html>.

days, and we adopt “10 previous + 10 post eligible days” analysis, which is illustrated in the following steps.

Step 2: Using device-level interval data, calculate baseline device-level load profile by aggregating load for 20 days – 10 eligible days prior to event day and 10 eligible days after event day. The baseline load profile is the average load profile for these 20 days.

Step 3: kW savings is the average kW difference during event-day load profile vs baseline-day load profile.

Program level achieved, EOY, and incremental CP kW, NCP kW, 4CP kW, and energy (kWh) savings will be estimated in the following manner:

Table 11.1-3: [RES DR] FlexEV Smart Rewards Program Savings

| Savings Type | NCP kW | CP kW | 4CP kW | kWh ⁴⁷⁰ |
|---------------------|--|--|--|--------------------|
| Achieved savings | Maximum kW savings during any event throughout the year | Average kW savings for events coincided with “peak probability table” | Average kW savings during ERCOT 4CP events, multiplied by success rate | - |
| EOY savings | Maximum kW savings during any event throughout the year, scaled by EOY participation | Average kW savings during June – September events, scaled by EOY participation | Average kW savings during ERCOT 4CP events, multiplied by success rate and scaled by EOY participation | - |
| Incremental savings | Maximum kW savings during any event throughout the year, scaled by newly added participation | Average kW savings during June – September events, scaled by newly added participation | Average kW savings during ERCOT 4CP events, multiplied by success rate and scaled by newly added participation | - |

FlexEV Off-Peak Rewards Program

The FlexEV Off-Peak Rewards program incentivizes customers to voluntarily charge during off-peak hours (between 9pm and 4pm), without any direct intervention from CPS Energy. In return, customers receive a one-time \$125 credit on their utility bill and can earn a \$10 monthly credit if charging is limited to no more than twice monthly during peak hours.

FlexEV Smart Rewards non-event days were the best option for a “control group” because we have not

⁴⁷⁰ The general assumption of EV programs is to shift load instead of saving energy.

detected significant charging behavior change for these days. Savings analysis is described in detail by the following steps:

Step 1: For both FlexEV Smart Rewards and FlexEV Off-Peak Rewards datasets, aggregate non-event, non-holiday weekdays to generate two separate average load profiles.

Step 2: Calculate the adjusting ratio between FlexEV Off-Peak Rewards and FlexEV Smart Rewards.

Step 3: Apply adjusting ratio to FlexEV Smart Rewards interval EV load to force the average load profile to be the same with that of FlexEV Off-Peak Rewards and therefore create a comparable “baseline.”

Step 4: For both adjusted FlexEV Smart Rewards and FlexEV Off-Peak Rewards datasets, calculate daily average kW level during 4pm to 9pm for every non-event, non-holiday weekday. The differences between 4pm to 9pm kW level for these two datasets are the estimated kW savings for each non-event, non-holiday weekday.

Step 5: For the days which fall on event days of the FlexEV Smart Rewards program, kW savings per device were assumed as the average kW savings level throughout entire fiscal year.

Program level achieved, EOY and incremental CP kW, NCP kW, 4CP kW and energy (kWh) savings will be estimated in the following manner:

Table 11.1-4: [RES DR] FlexEV Off-Peak Rewards Program Savings

| Savings Type | NCP kW | CP kW | 4CP kW | kWh ⁴⁷¹ |
|---------------------|--|--|---|--------------------|
| Achieved savings | Maximum kW savings during any peak period throughout the year | Average kW savings for non-holiday weekdays | Average kW savings during ERCOT 4CP events | - |
| EOY savings | Maximum kW savings during any peak period throughout the year, scaled by EOY participation | Average kW savings for non-holiday weekdays, scaled by EOY participation | Average kW savings during ERCOT 4CP events, scaled by EOY participation | - |
| Incremental savings | Maximum kW savings during any peak period throughout the year, scaled by newly added participation | Average kW savings for non-holiday weekdays, scaled by newly added participation | Average kW savings during ERCOT 4CP events, scaled by newly added participation | - |

⁴⁷¹ The general assumption of EV programs is to shift load instead of saving energy.

11.1.2.2 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 1 year for behavioral DR, and for all the other residential demand response measures the EUL is 10 years.

11.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- For each event, the starting and ending time, ambient temperature, and reason for deployment.
- Program enrollment at the beginning and end of the program year, and during each demand response event, by participant class.
- Aggregated fifteen-minute interval meter data by dwelling type or cycling strategy category.

12. COMMERCIAL: LIGHTING

12.1 LIGHTING EFFICIENCY

12.1.1 Guidance For Combination Lighting Fixture & Controls Projects

For Lighting retrofits installed in combination with existing controls or controls upgrade, fixture and control savings should be allocated as follows

- 1) Calculate total savings, adjusting pre and post operating hours and coincidence factors to account for applicable controls
- 2) Determine if project is eligible to claim controls savings:
 - a. Scenario 1: Retrofit project with no baseline controls
 - b. Scenario 2: New construction project with controls other than occupancy sensors
- 3) If controls savings are eligible, calculate controls savings using the lighting controls measure section. Otherwise, set control savings equal to zero
- 4) Deduct controls savings from total savings
- 5) Claim controls savings using controls EUL. Claim difference of the total savings and controls savings using applicable fixture EUL.

12.1.2 Measure Description

This section provides estimates of the energy and peak savings resulting from the installation of energy efficient lamps and/or ballasts. The installation can be the result of new construction or the replacement of existing lamps and/or ballasts. This TRM Measure ID covers the following lighting technologies:

- Linear Fluorescent T5s and High-Performance or Reduced Watt T8s. Linear fluorescent measures may also involve delamping⁴⁷² with or without the use of reflectors.
- Fluorescent Electrodeless Induction lamps and fixtures.
- Compact Fluorescent Lamp (CFL) screw-based lamps and hard-wired pin-based fixtures.
- Pulse-start Metal Halide (PSMH), Ceramic Metal Halide (CMH), and other High Intensity Discharge (HID) lamps.
- Light Emitting Diode (LED) screw-based lamps and hard-wired LED fixtures.

Energy and demand savings are based on operating hours, demand factors, and changes in pre-existing

⁴⁷² Delamping energy savings are eligible if done in conjunction with T-8 lamp and electronic ballast retrofits.

and post-installation lighting loads, as determined by using an approved lighting Standard Fixture Wattage table, available for download from the Texas Efficiency website.⁴⁷³

12.1.2.1 Eligibility Criteria

This section describes the system information and certified wattage values that must be used to estimate energy and peak savings from lighting systems installed as part of CPS Energy's energy efficiency programs. The Standard Fixture Wattage table lists the fixture codes and the demand values for use in calculating energy and demand savings for lighting efficiency projects.

Existing lighting fixtures must be removed or demolished in place after retrofit to count toward reduced pre-install wattage. Existing lighting fixtures that remain operable after retrofit should be listed in both the pre- and post-retrofit lighting inventory.

In addition, LED and linear fluorescent T8s need to be qualified as follows:

- High-performance (HP) and reduced watt (RW) T8 linear fluorescent lamps need to be qualified by the *Consortium for Energy Efficiency* (CEE). Their respective ballasts need to be qualified by NEMA⁴⁷⁴. See High Efficiency Condition section for additional details.
- LED lamps and fixtures must have their input power (wattage) and an L⁷⁰ rated life (hours) verified through some combination of the following references: DesignLights ConsortiumTM (DLC), ENERGY STAR, or independent lab testing⁴⁷⁵ (e.g., LM-79, LM-80, TM-21, ISTMT). Rated life for LED fixtures should be greater than or equal to 50,000 hours, which can be demonstrated by compliance with DLC v3.0 or later⁴⁷⁶ or through independent lab testing. Similarly, rated life for integral LED lamps should be greater than or equal to 10,000 hours, which can be demonstrated by compliance with ENERGY STAR Version 2.1 Specification or later⁴⁷⁷ or through independent lab testing. These values represent the point at which the minimum L70 was raised to levels consistent with current deemed measure life assumptions.
 - DLC and ENERGY STAR certified model numbers should closely align with the installed model number. However, small variances are allowed for portions of the model number that may refer to aspects of the fixture that do not affect energy performance (e.g., color temperature, fixture housing). Reported model numbers should always default to the closest match available.
 - DLC and ENERGY STAR specifications are periodically updated. Projects may report

⁴⁷³ Maintained by Frontier Energy on behalf of the Electric Utility Marketing Managers of Texas (EUMMOT): <http://texasefficiency.com/index.php/regulatory-filings/lighting>.

⁴⁷⁴ While CEE stopped qualifying ballasts in January 2015, the NEMA Premium Electronic Ballast Program has continued to be maintained and is consistent with the prior CEE specifications for high performance lamps and ballasts, tested in accordance with ANSI C82 Standards.

⁴⁷⁵ DLC test lab requirements: <https://www.designlights.org/solid-state-lighting/qualification-requirements/testing-lab-requirements/>.

⁴⁷⁶ Equivalent to the L⁷⁰ rated life requirement for all categories as specified in DesignLights ConsortiumTM (DLC) technical requirements v3.0, representing the point at which the minimum L⁷⁰ was raised to 50,000 hours for all product categories. https://www.designlights.org/wp-content/uploads/2021/01/DLC_Technical-Requirements-Table_V3-0.pdf.

⁴⁷⁷ Equivalent to the rated life requirement for all lamps as specified in the ENERGY STAR lamps specification v2.1. <https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Lamps%20V2.1%20Final%20Specification.pdf>.

fixture wattage from older versions of product certifications according to the following certification date guidelines if a copy of the original certification is preserved.

- New construction: permit date
 - Small business: date of customer acceptance or project proposal
 - All other: installation date
- DLC currently tracks delisted products. DLC-delisted products are eligible as long as they were rated for compliance with DLC v3.0 or later. ENERGY STAR does not track delisted products. However, any delisted product may be eligible if prior compliance is documented using a downloaded copy of the prior rating certificate.
 - If a product is available in various length increments but is DLC certified for a specific fixture length, the specified DLC power may be converted to a watts per square foot value to be multiplied against the installed fixture length instead of reporting as a non-qualified fixture.
 - **Field adjustable light output (FALO):** If a product is available with field-adjustable light output (or wattage setpoints) that can be adjusted by an installation contractor to utilize some or all LED nodes on the fixture, this will be noted in the Product Capabilities section of the DLC certification. DLC will typically specify the maximum input wattage. These fixtures should be reported based on the following scenarios:
 - If the fixture is installed at a reduced setpoint, it should be reported at the rated wattage for the reduced setpoint in combination with the “None” control code. Because DLC only reports the maximum wattage, report reduced wattage setpoint as documented in the manufacturer specification sheet.
 - If the fixture is installed with additional controls (e.g., occupancy sensor, daylighting, etc.), then it should be reported using the above guidance in combination with the applicable control code.
 - If the fixture is installed at the maximum setpoint without adjustment, it should be reported at the maximum DLC input wattage.
 - Project documentation for FALO should include a screenshot of the DLC certificate and photos of the field-adjustable setpoints for a sample of the installed lighting.
 - The same guidance applies to FALO fixtures installed in exterior applications, except that the fixture should always be installed in combination with photocell or timeclock controls

Exempt Lighting for New Construction. Some types of new construction lighting fixtures are exempt from inclusion in the interior lighting demand savings calculation. Exempt fixtures are those that do not provide general/ambient/area lighting, have separate control devices, and are installed in one of the following applications⁴⁷⁸:

1. The connected power associated with the following lighting equipment is not included in calculating total connected lighting power.
 - a. Professional sports arena playing-field lighting
 - b. Sleeping-unit lighting in hotels, motels, boarding houses, or similar buildings
 - c. Emergency lighting automatically off during normal building operation.
 - d. Lighting in spaces specifically designed for use by occupants with special lighting needs including visual impairment and other medical and age-related issues.
 - e. Lighting in interior spaces that have been specifically designated as a registered interior historic landmark
 - f. Casino gaming areas.
 - g. Mirror lighting in dressing rooms.
2. Lighting equipment used for the following shall be exempt provided that it is in addition to general lighting and is controlled by an independent control device.
 - a. Task lighting for medical and dental purposes
 - b. Display lighting for exhibits in galleries, museums, and monuments
3. Lighting for theatrical purposes, including performance, stage, film production, and video production.
4. Lighting for photographic processes.
5. Lighting integral to equipment or instrumentation and installed by the manufacturer.
6. Task lighting for plant growth or maintenance.
7. Advertising signage or directional signage.
8. in restaurant building and areas, lighting for food warming or integral to food preparation equipment.
9. Lighting equipment that is for sale.

⁴⁷⁸ IECC 2018, Section C405.3.1.

10. Lighting demonstration equipment in lighting education facilities.
11. Lighting approved because of safety considerations, inclusive of exit lights.
12. Lighting integral to both open and glass-enclosed refrigerator and freezer cases
13. Lighting in retail display windows, provided the display area is enclosed by ceiling-height partitions.
14. Furniture-mounted supplemental task lighting that is controlled by automatic shut off.
15. Exit signs.

Non-Qualifying LEDs

This section provides guidance on assessing and calculating nonresidential lighting project savings that include non-qualifying LEDs.

Savings Process

Figure 12.1-1 summarizes the recommended protocol for lighting system projects with non-qualifying LEDs when square footage cannot be isolated. Additional explanation and criteria for use follows.

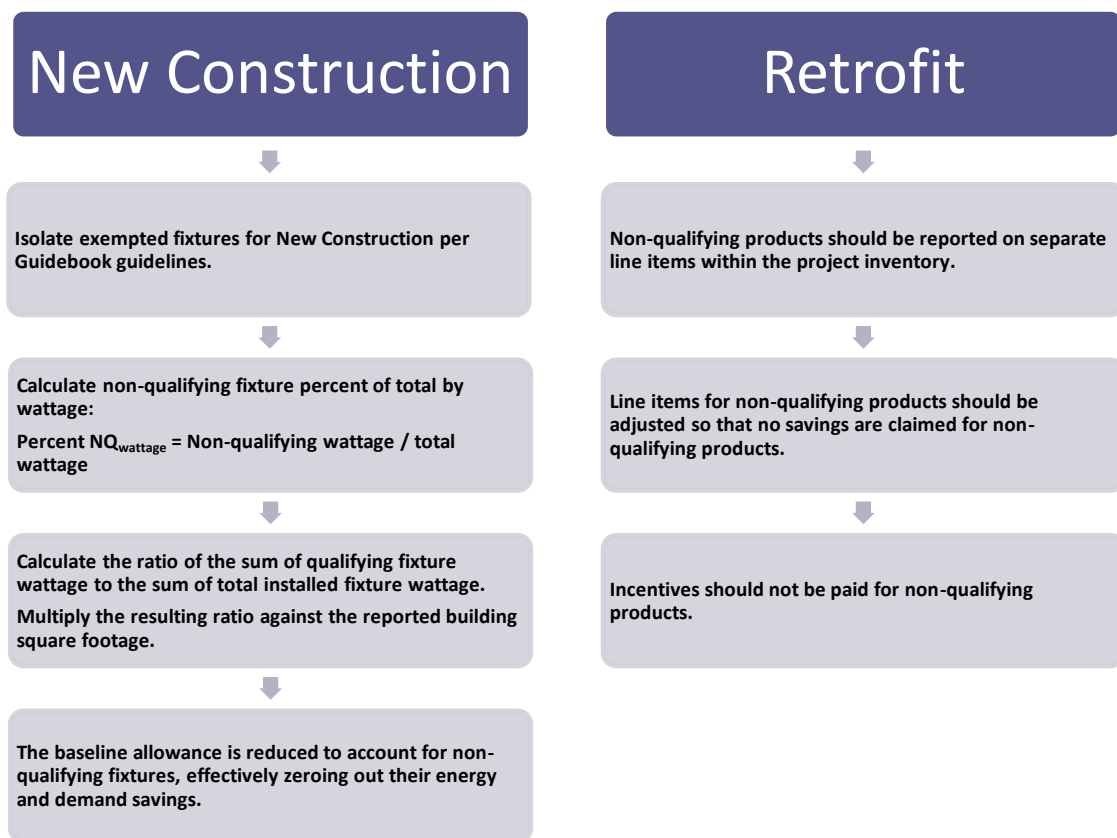


Figure 12.1-1: [COM Lgt] Non-Qualifying LED Process for Lighting Projects

Step 1: Qualify New Construction Projects

Calculate non-qualifying LED project percentage:

- Based as a percentage of demand ($\text{Percent NQ}_{\text{wattage}} = \text{wattage of non-qualifying fixtures} / \text{wattage of total fixtures}$)

Step 2: New Construction Projects

Adjust baseline wattage to account for non-qualifying fixtures.

- List non-qualifying LEDs on separate lines (e.g., separate on lighting inventory worksheet of deemed savings tool). Non-qualifying fixtures are identified by a unique fixture code.
- Adjust code allowable baseline wattage so that non-qualifying fixture wattage is not included as part of the lighting power density (LPD) code limit requirements. To do so, calculate the sum of the qualifying fixture wattage and the sum of the total installed fixture wattage. Take the ratio of qualifying fixture wattage to total fixture wattage and multiply the resulting ratio against the total treated square footage for the space. The adjusted square footage is included as part of the overall LPD calculation and will decrease the total allowable baseline wattage for the project.
- **Fixture Isolation Method.** If non-qualifying fixtures are isolated to a section of the building whose square footage can be easily segmented from the total building square footage, the non-qualifying fixtures and affected square footage can be excluded from the lighting inventory. Excluded fixtures must be documented when using the fixture isolation method.

Step 3: Retrofit Projects

List non-qualifying LEDs on separate lines (e.g., separate on lighting inventory worksheet of deemed savings tool).

- Include a unique identifier/marker for the non-qualifying LED within the inventory (e.g., fixture code, description, or another designator within deemed savings tool).
- Adjust non-qualifying LED wattage so their demand and energy savings are not included as part of the project savings. Demand and energy savings for non-qualifying LEDs shall result in zero project savings.
- Adjust non-qualifying LED quantities so they are not included as part of the project incentive. Incentives shall not be paid on non-qualifying LEDs.
- Provide clear visibility for all changes within the savings calculation (e.g., deemed savings

tool), including changes to all input assumptions and calculation methodologies to implement the above procedure.

- All other savings procedures and requirements as specified within the Guidebook for lighting measures apply to all fixtures of a lighting project.

12.1.2.2 Baseline Condition

The baseline condition or assumed baseline efficiency used in the savings calculations depends on the decision type used for the measure. For new construction, the baseline will be based on an LPD in watts per square foot by building/space type, as specified by the relevant energy code/standard applied to a specific project. For retrofit applications, the baseline efficiency would typically reflect the in-situ, pre-existing equipment, except for linear fluorescent T12s and first generation T8s as explained below. Eligible baseline fixture types and wattages are specified in the Standard Fixture Wattages table.

Major renovation projects should use a new construction baseline (for the building type after the improvement) if either of the following conditions are met:

- Building type changes in combination with the renovation.
- Renovation scope includes removing drywall and gutting existing building to the studs.

Linear Fluorescent T12 Special Conditions

The U.S. Energy Policy Act of 1992 (EPACT) set energy efficiency standards that preclude certain lamps and ballasts from being manufactured in or imported into the U.S. The latest standards covering general service linear fluorescents went into full effect July 2014. Under this provision, almost all 4-foot and some 8-foot T12 lamps, as well as first-generation 4-foot, 700 series T8 lamps were prohibited from manufacture. Because all lighting equipment for CPS Energy’s energy efficiency programs must be EPACT compliant, including existing or baseline equipment, adjustments were made to the T12 fixture values in the Standard Fixture Wattage table.

As such, 4-foot and 8-foot T12s are no longer an approved baseline technology for CPS Energy’s efficiency programs. While 4-foot and 8-foot T12s are still eligible for lighting retrofit projects, an assumed electronic T8 baseline will be used for estimating the energy and demand savings instead of the actual baseline of the existing T12 equipment. T12 fixtures remain in the Standard Fixture Wattage table, but the label for these records now reads “T12 (T8 baseline)” and the fixture wattage for these records reflects the adjusted fixture wattages shown in Table 12.1-1.

Table 12.1-1: [COM Lgt] Adjusted Baseline Wattages for T12 Equipment

| T12 Length ⁴⁷⁹ | Lamp Count | Revised Lamp Wattage | Revised System Wattage |
|---|------------|----------------------|------------------------|
| 48 inch – Std, HO, and VHO (4-foot bulbs) | 1 | 32 | 31 |
| | 2 | 32 | 58 |
| | 3 | 32 | 85 |
| | 4 | 32 | 112 |
| | 6 | 32 | 170 |
| | 8 | 32 | 224 |
| 96 inch – Std (8-foot bulbs) 60/75W | 1 | 59 | 69 |
| | 2 | 59 | 110 |
| | 3 | 59 | 179 |
| | 4 | 59 | 219 |
| | 6 | 59 | 330 |
| | 8 | 59 | 438 |
| 96 inch - HO and VHO (8-foot bulbs) 95/110W | 1 | 86 | 101 |
| | 2 | 86 | 160 |
| | 3 | 86 | 261 |
| | 4 | 86 | 319 |
| | 6 | 86 | 481 |
| | 8 | 86 | 638 |
| 2-foot U-Tube | 1 | 32 | 32 |
| | 2 | 32 | 60 |
| | 3 | 32 | 89 |

General Service Lamps

On May 8, 2022, the Department of Energy (DOE) issued two final rules relating to general service lamps:

- Energy Conservation Program: Definitions for General Service Lamps, effective July 8, 2022, which expanded the definition of general service lamp.⁴⁸⁰
- Energy Conservation Program: Energy Conservation Standards for General Service Lamps,

⁴⁷⁹ Key: HO = high output; VHO = very high output.

⁴⁸⁰ DOE Final Rule: Definitions for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0012-0022>.

effective July 25, 2022, which shifted the baseline to 45 lumens per watt efficacy.⁴⁸¹

The baseline is assumed to be the second-tier Energy Independence and Security Act of 2007 (EISA)-mandated efficiency for a general service lamp (see Table 12.1-2). The EISA regulations dictate that general service lamps must comply with a 45 lumen per watt efficacy standard at time of sale beginning January 1, 2023.⁴⁸²

Table 12.1-2: [COM Lgt] EISA 2007 Baseline Adjustment for GSLs^{483 484}

| Minimum Lumens | Maximum Lumens | Incandescent Equivalent Wattage | 2 nd Tier EISA 2007 Baseline Wattage |
|----------------|----------------|---------------------------------|---|
| 250 | 309 | 25 | Exempt |
| 310 | 749 | 40 | 12 |
| 750 | 1,049 | 60 | 20 |
| 1,050 | 1,489 | 75 | 28 |
| 1,490 | 2,600 | 100 | 45 |
| 2,601 | 3,300 | 150 | 66 |

12.1.2.3 High-Efficiency Condition

Eligible efficient fixture types and wattages are specified in the Standard Fixture Wattages table. Some technologies, such as LEDs, must meet the additional requirements specified under Eligibility Criteria.

High-Efficiency/Performance Linear Fluorescent T8s

All 4-foot post-retrofit technologies and new construction projects must use electronic ballasts manufactured after November 2014,⁴⁸⁵ and high performance T8 lamps that are on the T8 Replacement Lamp products list developed by the Consortium for Energy Efficiency (CEE) as published on its website.

If CEE does not have efficiency guidelines for a T8 system (such as for 8-foot, 3-foot, 2-foot, and U-bend T8 products), the product must have higher light output or reduced wattage than its standard equivalent product (minimum efficacy of 75 mean lumens per watt), a color rendering index (CRI) greater than 80, and an average rated life of 24,000 hours at 3 hours per start. In addition, 2-foot and 3-foot systems must also use electronic ballasts manufactured after November 2014.

⁴⁸¹ DOE Final Rule: Energy Conservation Standards for GSLs. <https://www.regulations.gov/document/EERE-2021-BT-STD-0005-0070>.

⁴⁸³ Federal standard for General Service Incandescent Lamps (GSILs): https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=20.

⁴⁸⁴ If exempt, refer to incandescent equivalent wattage.

⁴⁸⁵ Changes to the DOE Federal standards for electronic ballasts effective November 2014 met both the CEE performance specification and the NEMA Premium requirements, so CEE discontinued their specification and qualifying product lists. A legacy ballast list from January 2015 is still available.

Solar LEDs

Solar-powered LEDs are common in several commercial applications, primarily associated with pole-mounted fixtures. Solar lighting uses photovoltaic (PV) cells, which absorb solar energy to charge a battery and power the fixture. By default, solar fixtures should use an efficient wattage of 0 W. Because fixture performance relies on battery performance, the measure life for solar fixtures is capped at the expected battery life.

12.1.3 Energy and Demand Savings Methodology

12.1.3.1 Savings Algorithms and Input Variables

This section describes the deemed savings methodology for both energy and demand savings for all lighting projects. Savings are calculated using separate methods for retrofit and new construction projects.

Retrofit⁴⁸⁶

$$\begin{aligned} \text{Energy Savings } [\Delta kWh] &= (kW_{pre} \times hours_{pre} \times (1 - CAF_{pre}) - kW_{post} \times hours_{post} \times (1 - CAF_{post})) \times IEF_E \\ &\times ISR \end{aligned}$$

Equation 12.1-1

$$\begin{aligned} \text{Demand Savings } [\Delta kW] &= (kW_{pre} \times DF_{pre} \times (1 - CAF_{pre}) - kW_{post} \times DF_{post} \times (1 - CAF_{post})) \times IEF_D \times ISR \end{aligned}$$

Equation 12.1-2

New Construction

$$\text{Energy Savings } [\Delta kWh] = \left(\frac{LPD \times FA}{1,000} - kW_{post} \right) \times hours \times (1 - CAF_{post}) \times IEF_E$$

Equation 12.1-3

$$\text{Demand Savings } [\Delta kW] = \left(\frac{LPD \times FA}{1,000} - kW_{post} \right) \times DF \times (1 - CAF_{post}) \times IEF_D$$

Equation 12.1-4

⁴⁸⁶ The energy and demand savings calculations should also account for lighting controls that are present on existing lighting systems. The CAF in the Lighting Controls measure section should be used for these calculations to adjust the deemed hours and peak demand factors on the pre side of the equations. Savings for controls installed on new fixtures are accounted for in the Lighting Controls measure.

Where:

kW_{pre} = Total kW of existing measure(s) (Approved baseline fixture code wattage from deemed savings tool divided by 1,000 and multiplied by fixture/lamp quantity).

kW_{post} = Total kW of retrofit measure(s) (Verified installed fixture code wattage from deemed savings tool divided by 1,000 and multiplied by fixture/lamp quantity).

Note: wattage for installed LED fixtures may be rounded up or down to the nearest half watt; all other wattages should be rounded to the nearest watt.

LPD = Acceptable Lighting Power Density based on building type from efficiency codes from Table 12.1-3 [W/ft²].

FA = Floor area of the treated space where the lights were installed.

$hours$ = Hours by building type; see Table 12.1-8.

CAF = Control adjustment factor from Lighting Controls measure (set equal to 0 if no controls are installed on the existing fixture)

DF = Demand factor by building type for NCP, CP, or 4CP; see Table 12.1-8.

IEF_E = Energy HVAC interactive effect factor by space conditioning type; see Table 12.1-9.

IEF_D = Demand HVAC interactive effects factor by space conditioning type; see Table 12.1-9.

$1,000$ = Constant to convert from watts to kilowatts.

ISR = In-Service Rate, the percentage of incentivized units that are installed and in use (rather than removed, stored, or burnt out) to account for units incentivized but not operating = 1.0 unless otherwise specified for upstream/midstream applications; see Table 12.1-10.

Each of the parameters in these equations, and the approach or their stipulated values, is discussed in detail below.

Note: Using the savings coefficients defined below may result in NCP savings that are lower than CP or 4CP savings for some building types. In those cases, NCP savings should be set to the highest resulting demand savings when comparing NCP, CP, and 4CP demand savings.

Lamp and Fixture Wattages (kW_{pre} , $kW_{installed}$)

Existing Construction: Standard Fixture Wattage Table.⁴⁸⁷ Another example of the Standard Fixture Wattages can be found in the Fixtures Codes tab of the latest version of the Lighting Survey Form. This table contains identification codes and demand values (watts) to common fixture types (fluorescent, incandescent, HID, LED, etc.) used in commercial applications. The table is subdivided into lamp types such as linear fluorescent, compact fluorescent, mercury vapor, etc., with each subdivision sorted by fixture code. Each record, or row, in the Table contains a fixture code, which serves as a unique identifier. A legend explains the rules behind the fixture codes.

Each record also includes a description of the fixture, the number of lamps, the number of ballasts if applicable, and the fixture wattage. The table wattage values for each fixture type are averages of various manufacturers' laboratory tests performed to ANSI test standards. By using standardized demand values for each fixture type, the table simplifies the accounting procedures for lighting equipment retrofits. The table is updated periodically as new fixtures are added.

The fixture codes and the demand values listed in the watt/fixture column in the Table of Standard Fixture Wattages are used to calculate energy and demand savings for any lighting efficiency project.

New Construction: LPD table. Installed lighting wattages for new construction are determined in the same way as for retrofit or replacement projects (by using the Standard Fixture Wattage table). However, the baseline wattage is determined from the treated floor area and the applicable LPD value, the allowable watts per square foot of lit floor area as specified by the relevant energy code. The applicable baseline is determined by the energy code that was in effect at the time of building permit issuance. The code selected for energy savings calculations should match the code shown in the permit drawings. The current commercial code for the city of San Antonio is IECC 2021. These values are presented in Table 12.1-3 for interior spaces and in Table 12.1-5 for exterior spaces.

In Table 12.1-5 , exterior space types are grouped into four zones:

- Zone 1: Developed areas of national parks, state parks, forest lands, and rural areas.
- Zone 2: Areas predominantly consisting of residential zoning, neighborhood business districts, light industrial with limited night-time use, and residential mixed-use areas.
- Zone 3: All other areas.
- Zone 4: High-activity commercial districts in major metropolitan areas as designated by the local land use planning authority.

Note: Projects should default to Zone 2. Other Zones can be selected with documentation of the adjustment. Documentation includes a site aerial with a review of the neighboring properties to validate alternate selection. City zoning drawings may be used to validate a Zone 4 selection.

⁴⁸⁷ Maintained by Frontier Energy on behalf of EUMMOT: <http://texasefficiency.com/index.php/regulatory-filings/lighting>.

Table 12.1-3: [COM Lgt] New Construction LPDs for Interior Space Types by Building Type⁴⁸⁸

| Facility Type | LPD (W/ft ²) | Facility Type | LPD (W/ft ²) |
|-----------------------------|--------------------------|-------------------------|--------------------------|
| Automotive Facility | 0.75 | Multifamily | 0.45 |
| Convention Center | 0.64 | Museum | 0.55 |
| Courthouse | 0.79 | Office | 0.64 |
| Dining: Bar/Lounge/Leisure | 0.80 | Parking Garage | 0.18 |
| Dining: Cafeteria/Fast Food | 0.76 | Penitentiary | 0.69 |
| Dining: Family | 0.71 | Performing Arts Theater | 0.84 |
| Dormitory | 0.53 | Police Station | 0.66 |
| Exercise Center | 0.72 | Post Office | 0.65 |
| Fire Station | 0.56 | Religious Building | 0.67 |
| Gymnasium | 0.76 | Retail | 0.84 |
| Health Care/Clinic | 0.81 | School/University | 0.72 |
| Hospital | 0.96 | Sports Arena | 0.76 |
| Hotel/Motel | 0.56 | Town Hall | 0.69 |
| Library | 0.83 | Transportation | 0.50 |
| Manufacturing Facility | 0.82 | Warehouse | 0.45 |
| Motion Picture Theater | 0.44 | Workshop | 0.91 |

In addition to the interior building types specified in IECC, the following LPDs have been established for agricultural greenhouses. Greenhouse types are defined as follows:

- High intensity sole-source greenhouse: All plant lighting is provided by ceiling-mounted high intensity artificial electric lighting.
- Supplemented greenhouse: Most plant lighting is provided by natural sunlight with supplemented artificial electric lighting used to extend daylight hours during winter seasons with short periods of sunlight or on inclement weather days when sunlight levels are suboptimal.
- Vertical farming: Plants are sacked along vertical shelving from floor to ceiling to increase grow area.

⁴⁸⁸ IECC 2021 Table C405.3.2(1).

Table 12.1-4: [COM Lgt] New Construction LPDs for Agricultural Greenhouses⁴⁸⁹

| Facility Type ⁴⁹⁰ | LPD (W/ft ²) |
|---|--------------------------|
| Agricultural: high intensity sole-source greenhouse | 52.16 |
| Agricultural: supplemented greenhouse | 10.92 |
| Agricultural: vertical farming ⁴⁹¹ | - |

The total exterior lighting power allowance for all exterior building applications is the sum of the base site allowance plus the individual allowances for areas that are to be illuminated and are permitted in Table 12.1-5.

The reported square footage should represent the illuminated area. Each unique outdoor area should report a unique illuminated area specific to that application and should not be combined under a single space type. For example, a new construction convenience store project should have separate areas for fuel canopy, parking and drives, building facades, and any other applicable space types. Fuel canopies should reflect the area under the canopy rather than the entire exterior lot area. Building facades should reflect the total wall area where wall-mounted fixtures are installed rather than the floor area for any space type surrounding the illuminated wall.

Table 12.1-5: [COM Lgt] New Construction LPDs for Exterior Space Types by Building Type⁴⁹²

| Space Type | LPD (W/ft ²) | | | |
|---|--------------------------|--------|--------|--------|
| | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
| Base Site Allowance | 350 W | 400 W | 500 W | 900 W |
| Uncovered Parking: Parking Areas and Drives | 0.03 | 0.04 | 0.06 | 0.08 |
| Building Grounds: Walkways ≥ 10 ft wide, Plaza Areas, and Special Feature Areas | 0.10 | 0.10 | 0.11 | 0.14 |
| Building Grounds: Dining Areas | 0.65 | 0.65 | 0.75 | 0.95 |
| Building Grounds: Stairways | 0.60 | 0.70 | 0.70 | 0.70 |
| Building Grounds: Pedestrian Tunnels | 0.12 | 0.12 | 0.14 | 0.21 |
| Building Grounds: Landscaping | 0.03 | 0.04 | 0.04 | 0.04 |
| Building Entrances and Exits: Entry Canopies | 0.20 | 0.25 | 0.40 | 0.40 |
| Building Entrances, Exits, and Loading Docks: Loading Docks | 0.35 | 0.35 | 0.35 | 0.35 |
| Sales Canopies: Free-standing and Attached | 0.40 | 0.40 | 0.60 | 0.70 |
| Outdoor Sales: Open Areas | 0.20 | 0.20 | 0.35 | 0.50 |

⁴⁸⁹ "Energy Savings Potential of SSL in Agricultural Applications," US Department of Energy. June 2020. Table E-1.

<https://www.energy.gov/sites/prod/files/2020/07/f76/ssl-agriculture-jun2020.pdf>.

⁴⁹⁰ Weighted average of LPDs specified for LED, HPS/MH, and Fluorescent lighting type categories based on 2019 technology mix from Table E-1.

⁴⁹¹ Vertical farming was excluded due to 100% LED adoption in the 2019 technology mix from Table E-1.

⁴⁹² Ibid.

| Space Type | LPD (W/ft ²) | | | |
|---|--------------------------|--------|--------|--------|
| | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
| Building Facades ⁴⁹³ | - | 0.075 | 0.113 | 0.150 |
| Entrances and Gatehouse Inspection Stations | 0.50 | 0.50 | 0.50 | 0.50 |
| Loading Areas for Emergency Vehicles | 0.35 | 0.35 | 0.35 | 0.35 |

The following default metal halide baseline wattage assumptions have been approved for exterior athletic fields and courts, which are not included in the above LPD table. These baseline wattages were derived based on a review of reported lumen range for available LED products and their reported equivalent metal halide (MH) wattage.

Table 12.1-6: [COM Lgt] New Construction Baseline Wattages for Athletic Field/Court LEDs⁴⁹⁴

| Equivalent MH Wattage | # Lamps | LED Lumen Range |
|-----------------------|-------------------------|-----------------|
| 175 | 1 | < 7,500 |
| 250 | 1 | 7,500-12,499 |
| 400 | 1 | 12,500-19,999 |
| 400 | 2 | 20,000-39,999 |
| 1,000 | 1 | 40,000-59,999 |
| 1,500 | 1 | 60,000-74,999 |
| 1,000 | 2 | 75,000-99,999 |
| 1,000 | 3 | 100,000-124,999 |
| 1,000 | 4 | 125,000-149,999 |
| 1,000 | 5 | 150,000-199,999 |
| 1,000 | Variable ⁴⁹⁵ | ≥ 200,000 |

Operating Hours (Hours) and Demand Factors (DFs)

Operating hours and demand factors vary by building type, as shown in Table 12.1-8. The building types used in this table are based on the Commercial Buildings Energy Consumption Survey (CBECS)⁴⁹⁶ building types but have been modified for Texas.

The operating hours and peak demand factors specified in this section have been calculated at the facility level and should be applied to the entire facility. Outdoor fixtures that are not associated with

⁴⁹³ ASHRAE 90.1-2013 reflects a higher baseline. The Guidebook specifies the higher, more conservative, baseline in order to allow the same LPD to apply to all buildings, regardless of whether they are state funded.

⁴⁹⁴ Based on product review of LED replacement high-bay and corn lamp equivalent wattages.

⁴⁹⁵ Six plus one additional lamp for every 50,000 lumens above 200,00 (rounded down).

⁴⁹⁶ DOE-EIA Commercial Building Energy Consumption Survey. <https://www.eia.gov/consumption/commercial/>

the typical building lighting schedule may be claimed separately. These can include parking lot, walkway, wallpack, or other lighting, while building-mounted lighting with an operating schedule that more closely approximates the interior lighting schedule typically should not be claimed separately.

Table 12.1-7: [COM Lgt] Building Type Descriptions and Examples

| Building Type Code | Principal Building Activity | Definition | Operating Hours |
|--------------------|---------------------------------|---|--|
| Agriculture | Dairy Buildings | Buildings used to house dairy livestock and collect milk from dairy cows. | 1) Dairy Buildings |
| | Grow House | Buildings used to grow herbs, fruits, or vegetables under artificial lighting. | 1) 24-Hour Grow House 2) Non 24-Hour Grow House |
| Data Center | Data Center | Buildings used to house computer systems and associated components. | 1) Data Center |
| Education | College/University | Buildings used for academic or technical classroom instruction, such as elementary, middle, or high schools, and classroom buildings on college or university campuses. Buildings on education campuses for which the main use is not classroom are included in the category relating to their use. For example, administration buildings are part of "Office," dormitories are "Lodging," and libraries are "Public Assembly." | 1) College or University 2) Career or Vocational Training 3) Adult Education |
| | Primary School | | 1) Elementary or Middle School (grade 8 or lower) 2) Preschool or Daycare |
| | Secondary School ⁴⁹⁷ | | 1) High School (grade 9 or greater) 2) Religious Education |
| Food Sales | Convenience | Buildings used for retail or wholesale of food. | 1) Gas Station with a Convenience Store 2) Convenience Store |
| | Supermarket | | 1) Grocery Store or Food Market |
| Food Service | Full-Service Restaurant | Buildings used for preparation and sale of food and beverages for consumption. | 1) Restaurant or Cafeteria |
| | Quick-Service Restaurant | | 1) Fast Food |

⁴⁹⁷ Individual middle and junior high schools may have a campus size and building activities that better align with secondary schools. The use of secondary school assumptions in lieu of primary school assumptions is subject to pre-approval. Otherwise, Education subcategory should be determined by lowest grade.

| Building Type Code | Principal Building Activity | Definition | Operating Hours |
|--------------------|-----------------------------|---|---|
| Healthcare | Hospital | Buildings used as diagnostic and treatment facilities for inpatient care. | 1) Hospital 2) Inpatient Rehabilitation |
| | Outpatient Healthcare | Buildings used as diagnostic and treatment facilities for outpatient care. Medical offices are included here if they use any type of diagnostic medical equipment (if they do not, they are categorized as an office building). | 1) Medical Office 2) Clinic or Outpatient Health Care 3) Veterinarian |
| Multifamily | Common Area | Buildings containing Multifamily dwelling units, having multiple stories, and equipped with elevators. | 1) Common Area |
| Lodging | Large Hotel | Buildings used to offer multiple accommodations for short-term or long-term residents. | 1) Motel or Inn 2) Hotel 3) Dormitory, Fraternity, or Sorority 4) Retirement Home, Nursing Home, Assisted Living, or other Residential Care 5) Convent or Monastery |
| | Nursing Home | | |
| | Small Hotel/Motel | | |

| Building Type Code | Principal Building Activity | Definition | Operating Hours |
|--------------------|-----------------------------|--|--|
| Manufacturing | 1 Shift (<70 hr/week) | Buildings used for manufacturing/industrial applications. | 1) Apparel 2) Beverage, Food, and Tobacco Products 3) Chemicals 4) Computer and Electronic Products 5) Appliances and Components 6) Fabricated Metal Products 7) Furniture 8) Leather and Allied Products 9) Machinery 10) Nonmetallic Mineral Products 11) Paper 12) Petroleum and Coal Products 13) Plastics and Rubber Products 14) Primary Metals 15) Printing and Related Support 16) Textile Mills 17) Transportation Equipment 18) Wood Products |
| | 2 Shift (70-120 hr/week) | | |
| | 3 Shift (>120 hr/week) | | |
| Mercantile | Stand-Alone Retail | Buildings used for the sale and display of goods other than food. Shopping malls comprised of multiple connected establishments. | 1) Retail Store 2) Beer, Wine, or Liquor Store 3) Rental Center 4) Dealership or Showroom for Vehicles or Boats 5) Studio or Gallery |
| | Strip Mall/Enclosed Mall | | 1) Strip Shopping Center 2) Enclosed Malls |

| Building Type Code | Principal Building Activity | Definition | Operating Hours |
|--------------------|-----------------------------|--|--|
| Office | Large Office | Buildings used for general office space, professional office, or administrative offices. Medical offices are included here if they do not use any type of diagnostic medical equipment (if they do, they are categorized as an outpatient health care building). | 1) Administrative or Professional Office 2) Government Office 3) Mixed-Use Office 4) Bank or Other Financial Institution 5) Medical Office 6) Sales Office 7) Contractor's Office (e.g., Construction, Plumbing, HVAC) 8) Non-Profit or Social Services 9) Research and Development 10) City Hall or City Center 11) Religious Office 12) Call Center |
| | Medium Office | | |
| | Small Office | | |
| Parking | Parking Garage | Buildings used for parking applications. | No sub-categories collected. |

| Building Type Code | Principal Building Activity | Definition | Operating Hours |
|-------------------------|-----------------------------|---|---|
| Public Assembly | Public Assembly | Buildings in which people gather for social or recreational activities, whether in private or non-private meeting halls. | 1) Social or Meeting (e.g., Community Center, Lodge, Meeting Hall, Convention Center, Senior Center) 2) Recreation (e.g., Gymnasium, Health Club, Bowling Alley, Ice Rink, Field House, Indoor Racquet Sports) 3) Entertainment or Culture (e.g., Museum, Theater, Cinema, Sports Arena, Casino, Night Club) 4) Library 5) Funeral Home 6) Student Activities Center 7) Armory 8) Exhibition Hall 9) Broadcasting Studio 10) Transportation Terminal |
| Public Order and Safety | Jail and Prison | Government establishments engaged in justice, public order, and safety. | 1) Correctional Institutions 2) Prison Administration and Operation |
| | Other | | 1) Police Protection 2) Legal Counsel and Prosecution 3) Fire Protection 4) Public Order and Safety, Not Elsewhere Classified |
| Religious Worship | Religious Worship | Buildings in which people gather for religious activities, (such as chapels, churches, mosques, synagogues, and temples). | No sub-categories collected. |

| Building Type Code | Principal Building Activity | Definition | Operating Hours |
|--------------------|-----------------------------|--|---|
| Service | Service | Buildings in which some type of service is provided, other than food service or retail sales of goods. | 1) Vehicle Service or Vehicle Repair Shop 2) Vehicle Storage/Maintenance 3) Repair Shop 4) Dry Cleaner or Laundromat 5) Post Office or Postal Center 6) Car Wash 7) Gas Station with no Convenience Store 8) Photo Processing Shop 9) Beauty Parlor or Barber Shop 10) Tanning Salon 11) Copy Center or Printing Shop 12) Kennel |
| Warehouse | Warehouse | Buildings used to store goods, manufactured products, merchandise, raw materials, or personal belongings (such as self-storage). | 1) Refrigerated Warehouse 2) Non-refrigerated warehouse 3) Distribution or Shipping Center |
| Other | Other | For building types not explicitly listed. | Values used for Other are the most conservative values from the explicitly listed building types. |

Table 12.1-8: [COM Lgt] Operating Hours and Demand Factors by Building Type⁴⁹⁸

| Building Type | Operating Hours | Peak Type ⁴⁹⁹ | | |
|--|-----------------|--------------------------|------|------|
| | | NCP | CP | 4CP |
| Agriculture: Long-Day Lighting ⁵⁰⁰ | 6,209 | 1.00 | 1.00 | 1.00 |
| Agriculture: Non-24 Hour Sole-Source Greenhouse ⁵⁰¹ | 5,479 | 1.00 | 1.00 | 1.00 |
| Agriculture: Non-24 Hour Supplemented Greenhouse ⁵⁰² | 2,000 | 1.00 | 0.00 | 0.00 |
| Data Centers | 4,008 | 0.85 | 0.85 | 0.85 |
| Education: K-12 with Summer Session, College, University, Vocational, and Day Care | 3,577 | 0.90 | 0.90 | 0.90 |
| Education: K-12 with Partial Summer Session ⁵⁰³ | 3,177 | 0.90 | 0.84 | 0.72 |
| Education: K-12 without Summer Session | 2,777 | 0.90 | 0.32 | 0.54 |
| Food Sales: Non-24 Hour Supermarket or Convenience Store | 4,706 | 0.90 | 0.90 | 0.90 |
| Food Service: Full-Service Restaurant | 4,368 | 0.90 | 0.90 | 0.90 |
| Food Service: Quick-Service Restaurant | 6,188 | 0.90 | 0.90 | 0.90 |
| Food Service: 24 Hour Restaurant | 7,311 | 0.90 | 0.90 | 0.90 |
| Health Care: Inpatient | 5,730 | 0.90 | 0.81 | 0.70 |
| Health Care: Outpatient | 3,386 | 0.90 | 0.71 | 0.50 |
| Health Care: Resident Care and Nursing Home | 4,271 | 0.90 | 0.71 | 0.50 |
| Lodging: Hotel/Motel/Dorm, Common Area | 6,630 | 0.90 | 0.90 | 0.90 |
| Lodging: Hotel/Motel/Dorm, Room | 3,055 | 0.90 | 0.30 | 0.30 |
| Manufacturing: 1 Shift (<70 hr/week) | 2,786 | 0.85 | 0.83 | 0.85 |
| Manufacturing: 2 Shift (70-120 hr/week) | 5,188 | 0.85 | 0.85 | 0.85 |
| Manufacturing: 3 Shift (>120 hr/week) | 6,414 | 0.85 | 0.85 | 0.85 |
| Mercantile: Non-24 Hour Stand-Alone Retail | 3,668 | 0.90 | 0.90 | 0.90 |
| Mercantile: Enclosed Mall | 4,813 | 0.90 | 0.90 | 0.90 |
| Mercantile: Strip Center and Non-Enclosed Mall | 3,965 | 0.90 | 0.90 | 0.90 |

⁴⁹⁸ The operating hours and peak demand factors listed in this table have been calculated at the facility level and should be applied to the entire facility. Outdoor fixtures that are not associated with the typical building schedule may be claimed separately.

⁴⁹⁹ Building type operating schedules are adapted from COMNET Appendix C – Schedules (Rev. 3). <https://comnet.org/appendix-c-schedules>. Updated 7/25/2016.

⁵⁰⁰ Daily operating hours are 17 hours/day, 365.25 days/year, for dairy cow housing that implements long daylighting practices. Deemed operating hours are based on assumptions from the MN and WI TRMs and market research indicating 16-18 hours of daily operation.

⁵⁰¹ Daily operating hours are 15 hours/day, 365.25 days/year. Deemed operating hours are based on market research indicating 14-16 hours of daily operation.

⁵⁰² Daily operating hours are 15 hours/day, 365.25 days/year. Deemed operating hours are based on market research indicating 14-16 hours of daily operation.

⁵⁰³ Assuming a partial summer session in June with no summer session in July.

| Building Type | Operating Hours | Peak Type ⁴⁹⁹ | | |
|--|-----------------|--------------------------|------|------|
| | | NCP | CP | 4CP |
| Mercantile/Food Sales: 24 Hour Stand-Alone Retail, Supermarket, or Convenience Store | 6,900 | 0.90 | 0.90 | 0.90 |
| Multifamily: Common Area | 4,772 | 0.90 | 0.90 | 0.90 |
| Office | 3,737 | 0.90 | 0.86 | 0.90 |
| Outdoor: Athletic Field and Court ⁵⁰⁴ | 767 | 1.00 | 0.00 | 0.00 |
| Outdoor: Billboard ⁵⁰⁵ | 3,470 | 1.00 | 0.00 | 0.00 |
| Outdoor: Dusk-to-Dawn ⁵⁰⁶ | 4,161 | 1.00 | 0.00 | 0.00 |
| Outdoor: Less than Dusk-to-Dawn ⁵⁰⁷ | 1,998 | 1.00 | 0.00 | 0.00 |
| Parking Garage | 7,884 | 1.00 | 1.00 | 1.00 |
| Public Assembly | 2,638 | 0.65 | 0.65 | 0.65 |
| Public Order and Safety: Jail and Prison | 7,264 | 0.90 | 0.90 | 0.90 |
| Public Order and Safety: Other | 3,472 | 0.90 | 0.71 | 0.50 |
| Religious Worship | 1,824 | 0.65 | 0.65 | 0.65 |
| Service: Excluding Food | 3,406 | 0.90 | 0.90 | 0.90 |
| Warehouse: Non-Refrigerated | 3,501 | 0.85 | 0.79 | 0.75 |
| Warehouse: Refrigerated | 3,798 | 0.85 | 0.79 | 0.75 |
| Other | 2,638 | 0.65 | 0.65 | 0.50 |

Building Type Selection

The deemed lighting hours of use (HOU) and peak demand factors (DF) for the utility to use in calculating savings associated with lighting are broken down by building type and use. If the building type changes in combination with the retrofit, the selected building type should be consistent with the space condition after improvement. These values are provided in Table 12.1-8. For most building types listed in this table, the HOU and CFs were created based on weighted averages of lighting usage across all activity areas of the building.⁵⁰⁸ Therefore, the deemed HOU and CFs are representative of an entire building type, across all activity areas that are in a “typical” building for this type.

The following flow chart has been provided to assist the utility in understanding how to use the deemed

⁵⁰⁴ “2015 U.S. Lighting Market Characterization,” U.S. Department of Energy. November 2017. Value derived by multiplying average daily operating hours (2) by 365.25 hours/year.

⁵⁰⁵ Ibid.

⁵⁰⁶ This space type refers to fixtures controlled either by photocells or by timers operating on a dusk-to-dawn schedule. Calculated based on average dark hours for Amarillo (northernmost) and Corpus Christi (southernmost) climate zones from sunrise to sunset excluding ½ of civil twilight period. <https://www.timeanddate.com/sun/>. Note: pending update to US Naval Observatory annual data once website maintenance has completed. http://aa.usno.navy.mil/data/docs/RS_OneYear.php.

⁵⁰⁷ This space type refers to fixtures controlled by timers operating on a less than dusk-to-dawn schedule.

⁵⁰⁸ More information on how these values were created can be found in PUCT Docket #39146.

methods for calculating lighting savings based on HOU and CF provided in the Guidebook. Additionally, it provides guidance on how to treat lodging facilities and outdoor lighting projects as well as unique building types.

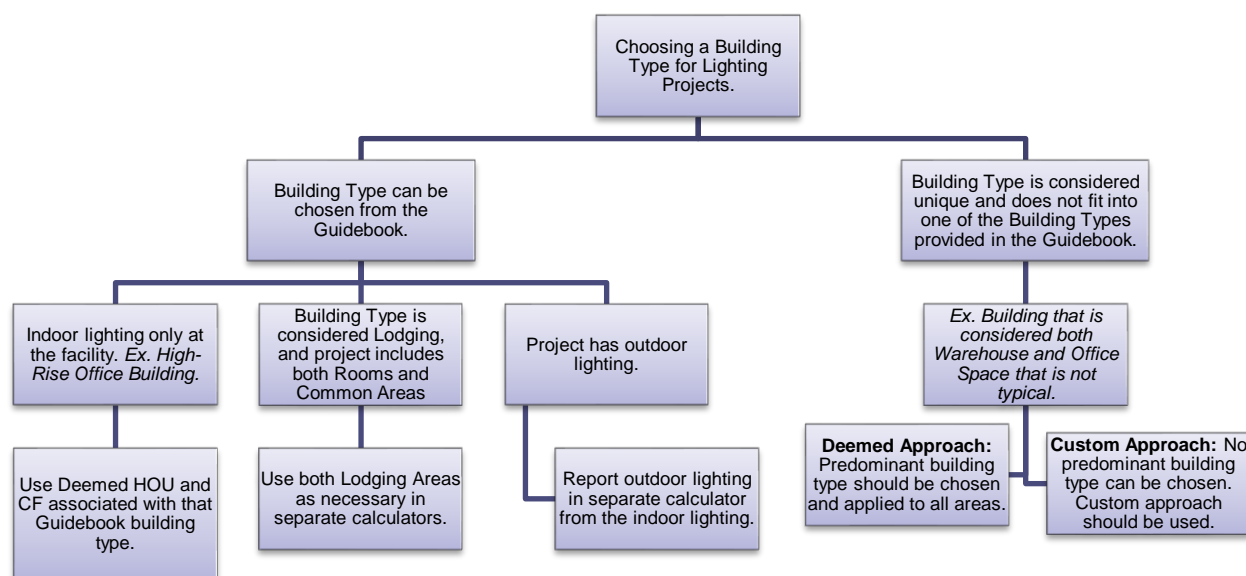


Figure 12.1-2: [COM Lgt] Building Type Decision Making

Lodging sites. Lodging facilities (Hotel/Motel/Dormitories) have been identified in the Guidebook by *Common* and *Rooms*, both with different HOU and CF. As two different values have been provided for these areas, it is acceptable for the utility to use either or both building types for a single project.

Outdoor Lighting Projects that involve outdoor lighting should be claimed in a separate calculator or separate inventory within the same calculator. The exception to this is walkway lighting that is more consistent with building operation. In this application, the utility should use the primary building type as its HOU, and CFs have been rolled up into the overall building type calculations (e.g., walkway lighting between two buildings that operates during business hours).

Building Type Selection. In most cases, buildings (except greenhouses and parking structures) should be classified based on the building type that represents the majority of the square footage. Greenhouses and parking garages should be treated separately from other indoor spaces intended for human occupancy. In other situations where multiple Guidebook building types seem plausible, or a predominant building type is unclear, the utility has two choices:

- **Deemed approach.** The deemed approach is a simplified method where the utility should choose a building type based on the “best fit” for the facility. For interior spaces, this is determined by the largest interior area for the potential building areas. Although, if that is not the best fit, the utility will use its best judgment in making this decision and provide sufficient, defensible documentation for its decision-making process.

The “Manufacturing” building type is specified with 1, 2, and 3 shift options:

- 1 Shift: typical operation of 9.5-11.5 hours per day and 4-6 days per week (< 70 hours per week)
- 2 Shift: typical operation of 18-20 hours per day and 5-6 days per week (70-120 hours per week)
- 3 Shift: typical operation of 24 hours per day and 5-6 days per week (> 120 hours per week)

The following building type combinations are pre-authorized exceptions to this rule. For these combinations, individual fixtures can be reported as either specified building type based on location. All other interior space combinations should reference a single deemed building type unless authorized by the evaluator.

- Office – Warehouse (refrigerated or non-refrigerated)
- Office – Manufacturing (any shift number)
- Manufacturing (buildings with different shift designations by area)
- Inpatient healthcare – Outpatient healthcare
- Lodging, common areas – Lodging, rooms

The “Other” building type can be used for business types that are not explicitly listed. The Hours and CF values used for Other are the most conservative values from the explicitly listed building types (except for the CF values specified for “Education: K-12 without Summer Session” and “Lodging: Hotel/Motel/Dorm, Common Areas,” which are associated with a very specific operating schedules that experience low coincidence with the summer peak period). When the Other building type is used, a description of the actual building type, the primary business activity, the business hours, and the lighting schedule must be collected for the project site and stored in the utility tracking data system.

“Outdoor Dusk-to-Dawn” applies to outdoor fixtures controlled by a photocell or timer with dusk-to-dawn operation throughout the entire year. Outdoor fixtures controlled by timers with less than dusk-to-dawn operation (excluding for athletic fields and courts) may be claimed separately using the “Outdoor Less than Dusk-to-Dawn” building type or using a custom timer schedule.

Exterior spaces may reference multiple outdoor “building” types differentiated based on typical operating schedules (Outdoor dusk-to-dawn, less than dusk-to-dawn, athletic, or billboard).

- **Custom approach.** In more unique situations where the deemed building types in the Guidebook may not be representative of the project’s facility type, or where the facility may represent multiple building types without a clear predominant building type (or the use of a

predominant building type may be too conservative in the estimate of savings), the utility should consider these projects “custom.” The deemed methods only apply to specific scenarios and cannot be developed for all unique situations. Defensible documentation for HOU and CF assumptions should be provided.

HVAC Interactive Effects Factors

Basic lighting savings are adjusted to account for the lighting system interaction with HVAC systems in conditioned or refrigerated spaces. A reduced lighting load reduces the internal heat gain to the building, which reduces the air conditioning/cooling load, but it also increases the heating load. This measure only considers the additional cooling savings, and the heating penalty or increase in usage is ignored.

As Table 12.1-9 shows, four conditioned space types are used. There is a single air-conditioned space type and two options for commercial refrigeration type spaces like walk-in coolers and refrigerated warehouses: medium and low temperature. If the temperature of the actual application falls between these values, then the higher temperature value should be used. The final space type is unconditioned (or more explicitly uncooled as the focus is on cooling). In the lighting calculators, these values are typically assigned at the line-item level based on the conditioning type for the space in which the fixtures are located.

Table 12.1-9: [COM Lgt] Deemed Energy and Demand Interactive HVAC Factors⁵⁰⁹

| Space Conditioning Type | Energy Interactive HVAC Factor | NCP Demand Interactive HVAC Factor | CP/4CP Demand Interactive HVAC Factor |
|---------------------------------------|--------------------------------|------------------------------------|---------------------------------------|
| Air Conditioned | 1.05 | 1.05 | 1.10 |
| Med. Temp. Refrigeration (33 to 41°F) | 1.25 | 1.25 | 1.25 |
| Low Temp. Refrigeration (-10 to 10°F) | 1.30 | 1.30 | 1.30 |
| None (Unconditioned/Uncooled) | 1.00 | 1.00 | 1.00 |

Upstream/Midstream Program Assumptions

For upstream/midstream program delivery, use the following AOH and CF assumptions specified by lamp type. Assumed AOH and CF values have been weighted based on building type survey data from 2018 CBECS⁵¹⁰ and 2018 MECS⁵¹¹ as well as lamp density and lamp type distribution survey data from the DOE 2020 U.S. Lighting Market Characterization (LMC).⁵¹²

All general service and reflector lamps with an equivalent wattage of 100 W or lower distributed

⁵⁰⁹ Petition of Electric Utility Marketing Managers of Texas to Revise Existing M&V Guidelines for Lighting Measures, PUCT Docket No. 39146, from the Petition, Table 7 (page 17) and Table 12 (page 24).

⁵¹⁰ 2018 Commercial Building Energy Consumption Survey (CBECS). <https://www.eia.gov/consumption/commercial/>.

⁵¹¹ 2018 Manufacturing Energy Consumption Survey (MECS). <https://www.eia.gov/consumption/manufacturing/>.

⁵¹² 2020 U.S. Lighting Market Characterization, Department of Energy. April 2017. . https://www.energy.gov/sites/default/files/2024-08/ssl-lmc2020_apr24.pdf

through upstream or midstream programs should calculate savings using a combination of residential and non-residential savings methodologies with 95 percent of savings allocated to the residential sector and the remaining 5 percent of savings allocated to the commercial sector.⁵¹³

Table 12.1-10: [COM Lgt] Midstream Assumptions by Lamp Type⁵¹⁴

| Lamp Type | AOH | Demand Factors | | | ISR |
|------------------|-------|----------------|------|------|------|
| | | NCP | CP | 4CP | |
| GSL/reflector | 3,745 | 0.85 | 0.71 | 0.73 | 0.98 |
| LED Tube | 3,542 | 0.86 | 0.73 | 0.77 | 1.00 |
| High Bay Fixture | 3,987 | 0.85 | 0.84 | 0.85 | 1.00 |
| Garage | 7,884 | 1.00 | 1.00 | 1.00 | 1.00 |
| Outdoor | 4,161 | 1.00 | 0.00 | 0.00 | 1.00 |

Baseline wattage for GSLs is 45 Lumens per watt. For non-GSLs, the baseline wattage for ENERGY STAR qualified products is assumed to be equal to the equivalent wattage from the ENERGY STAR certification. Baseline wattage assumptions for DLC and third-party qualified products should be determined based on product technical specifications and/or delivered light output (lumens) and detailed in the program qualified product listing.

12.1.3.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

12.1.3.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

12.1.3.4 Measure Life and Lifetime Savings

Estimated useful life (EUL) values are defined for the following lamp/fixture types.⁵¹⁵ A separate new construction EUL has been established to account for the whole-building baseline.

- Halogen Lamps: 1.5 years

⁵¹³ Weighting assumptions based on evaluator review of LED purchasing behavior for similar program designs.

⁵¹⁴ 2018 CBECS and 2018 MECS. <https://www.eia.gov/consumption/commercial/data/2018/>, <https://www.eia.gov/consumption/manufacturing/data/2018/>

⁵¹⁵ Petition of AEP Texas Central Company, AEP Texas North Company, CenterPoint Energy Houston Electric, LLC, El Paso Electric Company, Entergy Texas, Inc., Oncor Electric Delivery Company LLC, Southwestern Electric Power Company, Texas-New Mexico Power Company, and Southwestern Public Service Company to Revise Existing Estimated Useful Life Values, PUCT Docket No. 36779, (August 27, 2009).

- High Intensity Discharge Lamps: 15 years
- Integrated-ballast CCFL Lamps: 4.5 years
- Integrated-ballast CFL Lamps: 2.5 years
- Integral LED Lamps (general service): 9 years⁵¹⁶
- LED Fixtures: 15 years
- LED Corn Cob Lamps: 15 years
- LED Tubes: 15 years
- Solar LEDs⁵¹⁷: 10 years
- Modular CFL and CCFL Fixtures: 15 years
- T8 and T5 Linear Fluorescents: 15 years
- New Construction Interior Fixtures/Controls: 14 years⁵¹⁸
- New Construction Exterior Fixtures: 15 years⁵¹⁹

12.1.4 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline: retrofit or new construction
- Building or space type
- Optional: building or space funding source (state or private)
- For new construction projects ONLY:
 - LPD factor
 - Interior and/or exterior lighting schedules and plans
 - Interior and/or exterior space areas and distances

⁵¹⁶ Petition of Electric Utility Marketing Managers of Texas to Establish Installation and Efficiency Standards for Non-Residential LED Technologies, PUCT Docket No. 38023, (June 14, 2010).

⁵¹⁷ The typical solar battery life is approximately 5-15 years. A typical product warranty for a solar LED fixture is 10 years. This deemed EUL aligns with the average product life expectancy and typical warranty period.

⁵¹⁸ Based on review of new construction EULs claimed by Texas investor-owned utilities during PY 2019 and 2020, weighted by energy savings.

⁵¹⁹ Ibid.

- If applicable, verify if SECO compliance certification forms were filed⁵²⁰
- Conditioned space type: cooling equipment type, refrigerated space temperature range, heating fuel type, and % heated/cooled
- Baseline fixture configuration
- Baseline lamp wattage
- Baseline ballast type
- Baseline lighting controls
- Baseline quantity of operating fixtures
- Baseline quantity of inoperable fixtures
- Post-retrofit manufacturer and model number⁵²¹
- Post-retrofit fixture configuration
- Post-retrofit lamp wattage⁵²²
- Post-retrofit lamp specification sheets: Post retrofit lamp product qualification information from DLC, ENERGY STAR®, or independent lab testing
- Post-retrofit ballast type
- Post-retrofit lighting controls
- Post-retrofit quantity of operating fixtures
- For FALO fixtures ONLY:
 - Isolate these fixtures by setting type and location within reported project inventories and track field adjustment settings; photos of the field-adjusted setpoints for a sample of fixtures
 - Post-retrofit lumen readings for inspection sample
- Equipment operating hours
- Lighting measure life category

⁵²⁰ State-funded buildings are required to submit SECO compliance forms as part of the NC/renovation process. Buildings that submit SECO compliance forms are considered state-funded and must meet the provisions of ASHRAE 90.1-2013 rather than IECC 2015. Previous tables in this section present the alternative compliance values where they are encountered in the codes.

⁵²¹ See Eligibility Criteria section for additional information and exceptions related to reporting post-retrofit model number.

⁵²² See Eligibility Criteria section for additional information and exceptions related to reporting post-retrofit fixture wattage.

- For retrofit only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging and installed fixture; OR an evaluator pre-approved inspection approach
- For new construction only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging and installed fixture; as-built design drawings; lighting specifications package that provides detailed make and model information on installed lighting; OR an evaluator pre-approved inspection approach
- For upstream/midstream only: Qualified product list mapping efficient lighting products to baseline wattage assumptions.

Document Revision History

Table 12.1-11: [COM Lgt] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Added guidance for delisted lighting products and for new construction exterior lighting zone selection. Aligned building type names across all commercial measures. |
| FY 2026 | Clarified exterior new construction code zone selection guidance, adjusted new construction savings algorithm, updated “multiple” control type, removed non-operational fixture penalty, in-service rate incorporated into retrofit savings algorithm, clarified building type section guidance, and updated midstream building type weighting assumptions. |

12.2 LIGHTING CONTROLS

12.2.1 Measure Description

This measure promotes the installation of lighting controls in both new construction and retrofit applications. For retrofit applications, lighting controls would typically be installed where there is no control other than a manual switch (wall or circuit panel). For new construction lighting systems, they would be added where they are not already required by existing energy or building codes. Promoted technologies include occupancy sensors and daylight dimming controls. Energy and peak demand savings are calculated for these technologies with a controls adjustment factor (CAF) Eligibility Criteria

Measures installed through utility programs must be one of the occupancy sensor, daylighting, and tuning controls that are described in Table 12.2-1. Savings may be claimed for control types that exceed the minimum code required controls, mainly occupancy sensors for interior spaces.

New construction (NC) buildings designed after November 1, 2016 must be equipped with lighting controls unless specifically designated in the below exceptions. Most interior building spaces must have occupancy sensor controls or time-switch controls. Daylight responsive controls must be present in daylight zones. Exterior lighting must be installed with daylight sensors. Therefore, NC lighting controls savings can only be claimed in instances where the installed controls exceed energy code. Refer to IECC 2015, Section C405 for more information.

Networked lighting control (NLC): An NLC system uses software control based on the outputs of the sensor equipment. The system requires commissioning to ensure proper operation. A plan detailing the inspection and recalibration frequency that identifies the actions necessary through the end of the EUL period is required to ensure continued operation in accordance with design conditions.

12.2.1.1 Baseline Condition

The retrofit baseline condition assumes no existing or code-required automatic lighting controls are installed on the existing lighting fixtures (i.e., they are only manually switched).

For control types that exceed the minimum required control types (usually occupancy sensors or time switch controls), savings can be claimed with the minimum required controls as the baseline efficiency. In these cases, the applicable baseline control adjustment factors (CAF) are specified for occupancy sensors in Table 12.2-2.

For new construction projects, the baseline should be occupancy sensors in most cases unless a specific exception is allowed by code.⁵²³

⁵²³ Per IECC 2015, C405.2 lighting controls are mandatory.

12.2.1.2 High-Efficiency Condition

The energy-efficient condition is properly installed (not bypassed or overridden) and calibrated lighting controls that control overhead lighting in a facility based on occupancy, day-lighting, or tuning sensors.

12.2.2 Energy and Demand Savings Methodology

12.2.2.1 Savings Algorithms and Input Variables

The equations for lighting controls resemble those used in Section 12.1 for Lighting Efficiency, with the addition of the control adjustment factor (CAF) multipliers, as shown below. Additionally, the pre/post kW difference is replaced by a single kW value (the total fixture wattage controlled by the device).

$$\text{Energy Savings } [\Delta kWh] = kW_{\text{controlled}} \times CAF \times \text{Hours} \times IEF_E$$

Equation 12.2-1

$$\text{Demand Savings } [\Delta kW] = kW_{\text{controlled}} \times CAF \times DF \times IEF_D$$

Equation 12.2-2

Where:

$kW_{\text{controlled}}$ = Total kW of controlled fixtures (Fixture wattage from Standard wattage table multiplied by quantity of fixtures).

Hours = Hours by building type from Table 12.1-8.

CAF = Controls adjustment Factor; see Table 12.2-2.

DF = Demand Factor for NCP, CP, or 4CP peak demand by building type; see Table 12.1-8.

IEF_E = Energy HVAC interactive effects factor by building type; see Table 12.1-9.

IEF_D = Demand HVAC interactive effects factor by building type; see Table 12.1-9.

See Section 12.1, the Lighting Efficiency, for a full explanation of the non-control variables and their corresponding values. The lighting controls CAF for different building types are presented in Table 12.2-2. The CAF represent the reduction in energy and demand usage. For example, a factor of 0.24 would equate to 24% energy and demand savings. The same values from the referenced Lawrence Berkeley National Laboratory (LBNL) study are used for both energy and demand factors because of the lack of published data for demand factors.

Table 12.2-1: [Lgt Controls] Lighting Control Definitions

| Control Type | Description |
|----------------------------|---|
| None | No control |
| Occupancy | Adjustment of light levels according to the presence of occupants -Wall or Ceiling-Mounted Occupancy Sensors -Integrated Fixture Occupancy Sensors -Time Clocks -Energy Management Systems |
| Daylighting (Indoor) | Adjustment of light levels automatically in response to the presence of natural light -Photosensors |
| Outdoor | Outdoor on/off photosensor/time clock controls; no savings attributed because already required by code |
| Personal Tuning | Adjustment of individual light levels by occupants according to their personal preference; applies to private offices, workstation-specific lighting in open-plan offices, and classrooms -Dimmers -Wireless ON/OFF switches -Personal computer-based controls -Pre-set scene selection |
| Institutional Tuning | Adjustment of light levels through commissioning or provision of switches or controls for areas or groups of occupants -Dimmable ballasts -On/Off or dimmer switches for non-personal tuning |
| Networked Lighting Control | Lighting systems with a combination of sensors, networked interfaces, software, and controllers that affect lighting changes in luminaires, retrofit kits, or lamps. NLC systems can be installed with or without luminaire level lighting control (LLLC), referring to the capability to have a networked occupancy sensor and ambient light sensor installed for each luminaire or kit. |

Table 12.2-2: [Lgt Controls] Energy and Power Adjustment Factors⁵²⁴

| Control Type | Control Codes | CAF | |
|---------------------------------|---------------|----------|-------------------|
| | | Retrofit | NC ⁵²⁵ |
| None | None | 0.00 | 0.00 |
| Occupancy | OS | 0.24 | 0.00 |
| Continuous daylighting (Indoor) | DL | 0.28 | 0.04 |

⁵²⁴ Williams, A., Atkinson, B., Garbesi, K., & Rubinstein, F., "A Meta-Analysis of Energy Savings from Lighting Controls in Commercial Buildings." Lawrence Berkeley National Laboratory. September 2011. Table 6, p. 14. Weighted average by number of "reviewed" and "non reviewed" papers.

⁵²⁵ NC CAFs are derived by deducting the OS CAF from the equivalent retrofit CAF value.

| Control Type | Control Codes | CAF | |
|----------------------------|--------------------|----------|-------------------|
| | | Retrofit | NC ⁵²⁵ |
| Outdoor ⁵²⁶ | Outdoor | 0.00 | 0.00 |
| Personal Tuning | PT | 0.31 | 0.07 |
| Institutional Tuning | IT | 0.36 | 0.12 |
| Networked Lighting Control | NLC ⁵²⁷ | 0.49 | 0.25 |

12.2.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

12.2.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

12.2.2.4 Measure Life and Lifetime Savings

Lighting controls savings for interior new construction projects should be claimed at the project level (combined fixture and controls savings) using the estimated useful life (EUL) matching the lighting equipment.⁵²⁸

For retrofit applications, the EUL for lighting controls is provided by the 2007 GDS Associates Report.⁵²⁹

- Retrofit sensors and controls: 10 years
- New construction interior fixtures/control⁵³⁰: 14 years

⁵²⁶ No control savings are allowed for outdoor controls because they are already required by code. ASHRAE 90.1-1989, Section 6.4.2.8 specifies that exterior lighting not intended for 24-hour continuous use shall be automatically switched by timer, photocell, or a combination of timer and photocell. This is consistent with current specifications in ASHRAE 90.1-2010, Section 9.4.1.3, which specifies that lighting for all exterior applications shall have automatic controls capable of turning off exterior lighting when sufficient daylight is available or when the lighting is not required during nighttime hours.

⁵²⁷ "Energy Savings from Networked Lighting Control (NLC) Systems with and without LLLC," Prepared by DesignLights Consortium for Northwest Energy Efficiency Alliance (NEEA). September 24, 2020. <https://www.designlights.org/resources/reports/report-energy-savings-from-networked-lighting-controlnlc-systems-with-and-without-lllc/>. Savings range from 0.35 without LLLC to 0.63 with LLLC, with an overall average of 0.49. Average is selected because report concludes that additional study is needed to verify the impact of LLLC.

⁵²⁸ Based on review of new construction EULs claimed by Oncor and CenterPoint during the PY 2019 and 2020 weighted by energy savings.

⁵²⁹ GDS Associates. Measure Life Report—Residential and Commercial/Industrial Lighting and HVAC Measures. Prepared for the New England State Program Working Group (SPWG). June 2007. This report only specifies an EUL for Occupancy Sensors and Photocells, so it is assumed that the same EUL was applied to time clocks. <http://library.cee1.org/content/measure-life-report-residential-andCommercialindustrial-lighting-and-hvac-measures>

⁵³⁰ Based on review of new construction EULs claimed by Oncor and CenterPoint during the PY 2019 and 2020 weighted by energy savings.

12.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- Baseline type: retrofit or new construction
- Conditioned space type: cooling equipment type, refrigerated space temperature range (specified per control)
- Location of controlled lighting: interior or exterior (specified per control)
- Baseline & post-retrofit lighting control type code⁵³¹
- Lighting control mount type: wall, ceiling, integrated fixture, etc.
- Lighting control equipment specification sheets
- Quantity of controlled fixtures/lamps
- Controlled fixture/lamp type
- Controlled fixture/lamp wattage
- For NLC systems:
 - Lighting control network specification sheets,
 - Lighting control commissioning report,
 - Lighting control network inspection and recalibration plan, or
 - Other evaluator pre-approved documentation
- **For retrofit only:** Proof of purchase: invoice showing model number; a photo of the model number on product packaging and installed fixture; OR an evaluator pre-approved inspection approach
- **For new construction only:** invoice showing model number; a photo of the model number on product packaging and installed fixture; as-built design drawings; lighting specifications package that provides detailed make and model information on installed lighting; OR an evaluator pre-approved inspection approach

⁵³¹ For a control type that combines multiple features (e.g., occupancy + daylighting), specify the installed control types by combining the control codes for the individual control types.

Document Revision History

Table 12.2-3: [Lgt Controls] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Clarified new construction controls eligibility. Updated control types. Consolidated EAF and PAF into CAF and added column for new construction CAF. Added documentation requirements for NLC systems. |
| FY 2026 | Consolidated “EAF” and PAF” coefficient label to “CAF” |

13. COMMERCIAL: HEATING, VENTILATION & AIR CONDITIONING

13.1 AIR CONDITIONER AND HEAT PUMP TUNE-UPS

13.1.1 Measure Description

This measure applies to direct expansion central air conditioners (AC) and heat pumps (HP) of any configuration where all applicable actions from the checklist below are completed. An AC tune-up involves checking, cleaning, adjusting, and resetting the equipment to factory conditions to restore operating efficiencies closer to as-new performance. This measure applies to all commercial applications.

For this measure, the service technician must complete the following tasks according to industry best practices. To properly assess and adjust the refrigerant charge level, the unit must be operating under significant (normal) cooling load conditions. Therefore, this measure may only be performed for energy savings reporting purposes when the outdoor ambient dry bulb temperature is above 75°F, and the indoor return air dry bulb temperature is above 70°F.

HVAC Inspection and Tune-Up Checklist⁵³²

- Check thermostat settings
- Tighten all electrical connections and measure motor voltage and current.
- Lubricate all moving parts, including motor and fan bearings.
- Inspect and clean the condensate drain.
- Inspect controls of the system to ensure proper and safe operation. Check the startup/shutdown cycle of the equipment to ensure the system starts, operates, and shuts off properly.
- Clean evaporator and condenser coils.
- Check refrigerant level and adjust to manufacturer specifications
- Clean indoor blower fan components and adjust to provide proper system airflow
- Inspect and clean or change air filters; replacement preferred best practice.
- Measure airflow via static pressure across the cooling coil and adjust to manufacturer

⁵³² Based on ENERGY STAR HVAC Maintenance Checklist. <https://www.energystar.gov/saveathome/heating-cooling/maintenance-checklist>.

specifications.

- Check capacitor functionality and capacitance and compare to original equipment manufacturer (OEM) specifications.

13.1.1.1 Eligibility Criteria

HVAC systems must be manufactured before January 1, 2023, to be eligible for this measure.⁵³³ All commercial customers are eligible for this measure if they have direct expansion refrigerated air conditioning that has not been serviced in the last 5 years.

This measure also applies to packaged terminal air conditioners and heat pumps (PTAC/PTHP), but chillers are ineligible.

13.1.1.2 Baseline Condition

The baseline is a system with some or all the following issues:

- Dirty condenser coil
- Dirty evaporator coil
- Dirty blower wheel
- Dirty filter
- Improper airflow
- Incorrect refrigerant charge

The baseline system efficiency should be calculated using the following formulas:

$$EER_{pre} = (1 - EL) \times EER_{post}$$

Equation 13.1-1

$$HSPF_{pre} = (1 - EL) \times HSPF_{post}$$

Equation 13.1-2

Where:

EER_{pre} = Efficiency of the cooling equipment before tune-up.

EL = Efficiency loss because of dirty coils, blower, filter, improper airflow, and/or incorrect refrigerant charge = 0.05.

⁵³³ The current federal standard became effective on January 1, 2023, with full manufacturing compliance of the new SEER2 testing procedure being enforced as of April 24, 2023. This measure will be updated in the future to address the new efficiency ratings.
<https://www.regulations.gov/document/EERE-2021-BT-TP-0030-0027>.

| | | |
|---------------|---|---|
| EER_{post} | = | Deemed cooling efficiency of the equipment after tune-up; see Table 13.1-1. |
| $HSPF_{pre}$ | = | Heating efficiency of the air source heat pump before tune-up. |
| $HSPF_{post}$ | = | Deemed heating efficiency of air source heat pumps after tune-up; see Table 13.1-1. |

Note: The efficiency loss factor specified above may be replaced with program specific values if an M&V plan and efficiency loss factor derivation are provided to the evaluation team. These factors will be subject to review at the end of each fiscal year and may be revised for the next fiscal year.

Table 13.1-1: [AC/HP Tune-up] Default EER and HSPF per Size Category⁵³⁴

| Size Category (Btuh) | AC Only Default EER | Heat Pump Default EER | Default HSPF |
|-------------------------|------------------------|--------------------------|--------------|
| < 65,000 | 11.2 | 11.2 | 7.7 |
| ≥ 65,000 and < 135,000 | 10.1 | 9.9 | 10.9 |
| ≥ 135,000 and < 240,000 | 9.5 | 9.1 | 10.6 |
| ≥ 240,000 and < 760,000 | 9.3 | 8.8 | 10.6 |
| ≥ 760,000 | 9.0 | 8.8 | 10.6 |

13.1.1.3 High-Efficiency Condition

After the tune-up, the equipment must be clean with airflows and refrigerant charges adjusted as appropriate and set forth above, with the added specification that refrigerant charge adjustments must be within +/- 3 degrees of target sub-cooling for units with thermal expansion valves (TXV) and +/- 5 degrees of target super heat for units with fixed orifices or capillary tubes.

The efficiency standard, or efficiency after the tune-up, is deemed to be the manufacturer specified energy efficiency ratio (EER) of the existing central air conditioner or heat pump, which has been determined by using the following logic and standards. The useful life of an AC unit is 19 years. The useful life of a heat pump is 16 years. Therefore, it is conservatively thought that the majority of existing, functioning units were installed under the federal standard in place between January 23, 2006 and January 1, 2015 for units less than 65,000 Btuh, which set a baseline of 13 SEER and 7.7 HSPF,⁵³⁵ and prior to January 1, 2010 for units greater than 65,000 Btuh. A 13 SEER is equivalent to approximately 11.2 EER⁵³⁶ using the conversion developed by Lawrence Berkeley Lab and US DOE: $EER = -0.02 \times SEER^2 + 1.12 \times SEER$. A 3.2 and 3.1 COP is equivalent to approximately 10.9 and 10.6 HSPF respectively using the conversion of $HSPF = 3.412 \times COP$.

⁵³⁴ Code specified EER and HSPF value from ASHRAE 90.1-2010 (efficiency value effective January 23, 2006 for units < 65,000 Btu/hr and prior to January 1, 2010 for units ≥ 65,000 Btu/hr). $HSPF = COP \times 3.412$.

⁵³⁵ Code specified HSPF from federal standard effective January 23, 2006 through January 1, 2015.

⁵³⁶ Code specified 13 SEER from federal standard effective January 23, 2006 through January 1, 2015, converted to EER using $EER = -0.02 \times SEER^2 + 1.12 \times SEER$. National Renewable Energy Laboratory (NREL). "Building America House Simulation Protocols." U.S. Department of Energy. Revised October 2010. <http://www.nrel.gov/docs/fy11osti/49246.pdf>.

13.1.2 Energy and Demand Savings Methodology

13.1.2.1 Savings Algorithms and Input Variables

Savings are based on an assumed efficiency loss factor of 5% because of dirty coils, dirty filters, improper airflow, and/or incorrect refrigerant charge.⁵³⁷

Energy Savings

Heating energy savings are only applicable to heat pumps.

$$\text{Energy Savings } [\Delta kWh] = kWh_{\text{Savings,C}} + kWh_{\text{Savings,H}}$$

Equation 13.1-3

$$kWh_{\text{Savings,C}} = Cap_C \times \left(\frac{1}{EER_{\text{pre}}} - \frac{1}{EER_{\text{post}}} \right) \times \frac{EFLH_C}{1,000}$$

Equation 13.1-4

$$kWh_{\text{Savings,H}} = Cap_H \times \left(\frac{1}{HSPF_{\text{pre}}} - \frac{1}{HSPF_{\text{post}}} \right) \times \frac{EFLH_H}{1,000}$$

Equation 13.1-5

Where:

| | | |
|----------------------|---|---|
| Cap_C | = | Rated cooling capacity of the equipment based on model number [Btuh] (1 ton = 12,000 Btuh). |
| Cap_H | = | Rated heating capacity of the equipment based on model number [Btuh] (1 ton = 12,000 Btuh). |
| EER_{pre} | = | Cooling efficiency of the equipment pre-tune-up using Equation 13.1-1 [Btuh/W]. |
| EER_{post} | = | Cooling efficiency of the equipment after the tune-up [Btuh/W]. |
| $HSPF_{\text{pre}}$ | = | Heating efficiency of the equipment pre-tune-up using Equation 2 [Btuh/W]. |
| $HSPF_{\text{post}}$ | = | Heating efficiency of the equipment after the tune-up [Btuh/W]. |
| $EFLH_{C/H}$ | = | Cooling/heating equivalent full-load hours [hours]; see Table 13.2-9 in Section 13.1, Split System/Single Packaged Air Conditioners and Heat Pumps Measure. |
| 1,000 | = | Constant to convert from watts to kilowatts. |

⁵³⁷ Energy Center of Wisconsin, May 2008; "Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research."

Demand Savings Algorithms

Demand savings are determined by applying a demand factor.

$$\text{Demand Savings } [\Delta kW] = \text{Capacity} \times \left(\frac{1}{EER_{pre}} - \frac{1}{EER_{post}} \right) \times \frac{DF}{1,000}$$

Equation 13.1-6

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 13.2-10 through Table 13.2-12 in Section 13.2 Split and Packaged Air Conditioners and Heat Pumps.

13.1.2.2 Deemed Energy Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

13.1.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure. See engineering algorithms in the previous section for calculating energy and demand savings.

13.1.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 5 years for AC or HP tune-ups.⁵³⁸

13.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- The most recent tune-up service date or confirmation that system has not been serviced within the previous five years
- Equipment type (split AC, split HP, packaged AC, packaged HP, PTAC, PTHP)
- Manufacturer and model number
- Cooling capacity of the serviced HVAC unit (tons)

⁵³⁸ GDS Associates, Inc. (2007). Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures. Prepared for The New England State Program Working Group; Page 1-3, Table 1.

- Heating capacity of the serviced HVAC unit, if applicable (tons)
- Before and after tune-up pictures of components illustrating condition change due to cleanings (Note: pictures that include well-placed familiar objects like hand tools often provide a sense of scale and a reference for color shading comparisons. Pictures of equipment nameplates are useful).
- Recommended:
 - Serial number
 - Refrigerant type
 - Amount of refrigerant added or removed
 - Target superheat or subcooling
 - Post tune-up superheat or subcooling
 - Static pressures before and after tune-up
 - Return and supply dry bulb and wet bulb temperatures

Document Revision History

Table 13.1-2: [AC/HP Tune-Up] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Clarified eligibility criteria. |
| FY 2026 | Updated tune-up checklist to match ENERGY STAR HVAC Maintenance Checklist |

13.2 SPLIT AND PACKAGED AIR CONDITIONERS AND HEAT PUMPS

13.2.1 Measure Description

This section summarizes the deemed savings methodology for the installation of air-cooled split system and single packaged air conditioning (AC) and heat pump (HP) systems. This measure covers assumptions made for baseline equipment efficiencies for early retirement (ER) based on the age of the replaced equipment and for replace-on-burnout (ROB) and new construction (NC) situations based on efficiency standards. Savings calculations incorporate the use of both full-load and part-load efficiency values. For ER, the actual age of the baseline system should be determined from the equipment nameplate or other physical documentation whenever possible. Default values are provided for when the actual age of the unit is unknown.

Applicable efficient measure types include:

- Packaged and split direct expansion (DX) ACs
- Packaged and split DX HPs

13.2.1.1 Eligibility Criteria

For a measure to be eligible to use this deemed savings approach, the following conditions must be met:

- The existing and proposed cooling equipment are electric.
- The building falls into one of the categories listed in Table 13.2-7. Building type descriptions and examples are provided in Table 13.2-7.
- ER projects involve the replacement of a working system. The ER approach cannot be used for projects involving a renovation where a major structural change or internal space remodel has occurred. An ROB approach should be used for these scenarios.
- Manufacturer datasheets for installed equipment or documentation of AHRI or DOE CCMS certification must be provided.^{539,540}

13.2.1.2 Baseline Condition

The baseline conditions related to efficiency and system capacity for ER, ROB, and NC are as follows.

Early Retirement

ER systems involve the replacement of a working system, prior to natural burnout. The ER baseline cannot be used for projects involving a renovation where a major structural change or internal space

⁵³⁹ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

⁵⁴⁰ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

remodel has occurred.

Two baseline condition efficiency values are required for an ER scenario, one for the ER (RUL) period and one for the ROB (EUL-RUL) period. For the ROB period, the baseline efficiency is the same as for an ROB/NC scenario. For the ER period, the baseline efficiency should be estimated according to the capacity, system type, and age (based on year manufactured) of the replaced system.⁵⁴¹ When the system age can be determined (from a nameplate, building prints, equipment inventory list, etc.), use the baseline efficiency levels provided in Table 13.2-1 through Table 13.2-5. If individual system components were installed at different times, use the condenser age as a proxy for the entire system. When the system age is unknown, assume a default value equal to the EUL. This corresponds to an age of 15 years. A default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible.

ER baseline efficiency values represent the code-specified efficiency in effect at the time the system was installed. Prior to 2002, code-specified efficiencies from ASHRAE 90.1-1989 were in effect. Code-specified efficiencies increased in 2002, approximating the effective date of ASHRAE 90.1-1999, which went into effect on October 29, 2001. Code-specified efficiencies increased again in 2010, 2015, 2018, and 2023 coinciding with the IECC 2009, IECC 2015, IECC 2018, and IECC 2021 code updates. The baseline efficiency levels shown in Table 13.2-1 through Table 13.2-5 are based on assumptions of the predominant heating types expected in the state. For air conditioners, baseline cooling efficiencies are displayed for a natural gas furnace heating section type. For HPs, baseline cooling efficiencies are displayed for electric resistance supplemental heating section type.

For units < 65,000 btuh (approximately 5.42 tons), EER, SEER, and HSPF values are converted to EER2, SEER2, and HSPF2 for consistency with the current federal standard. Unspecified EER2 are calculated by multiplying average EER/EER2 ratios, referencing EER2 values specified in the current federal standard for 12.2 and 11.7 EER. Unspecified SEER2 values are calculated by multiplying average SEER/SEER2 ratios, referencing SEER2 values specified for 14, 14.5, 15, and 16 SEER. Unspecified HSPF2 values are calculated by multiplying average HSPF/HSPF2 ratios, referencing HSPF2 values specified for 8.0 and 8.8 HSPF.

For 65,000+ btuh units, baseline EER values shown from ASHRAE/IECC assume natural gas heating for the predominant heating section type expected for commercial facilities in Texas. For units installed from 2002 to present, 0.2 EER may be added for “Electric Resistance (or None)” heating types. For units installed before 2002 and 135,000+ btuh (approximately 11.3 tons), 0.2 EER may be added for no heating.

⁵⁴¹ The actual age should be determined from the nameplate, building prints, equipment inventory list, etc. and whenever possible the actual source used should be identified in the project documentation.

Table 13.2-1: [DX HVAC] ER Baseline Full-Load Efficiency for ACs

| Year Installed (Replaced System) | Split < 3.75 tons [EER2] | Split ≥ 3.75 and < 5.4 tons [EER2] | Packaged < 5.4 tons [EER2] | All 5.4 to < 11.3 tons [EER] | All 11.3 to < 20 tons [EER] | All 20 to < 63.3 tons [EER] | All ≥ 63.3 tons [EER] |
|-------------------------------------|--------------------------------|---|----------------------------------|------------------------------------|-----------------------------------|-----------------------------------|-----------------------------|
| ≤ 2009 | 10.1 | 10.1 | 10.1 | 10.1 | 9.5 | 9.3 | 9.0 |
| 2010 – 2017 | 10.1 | 10.1 | 10.1 | 11.0 | 10.8 | 9.8 | 9.5 |
| 2018 – 2022 | 10.1 | 10.1 | 10.9 | 11.0 | 10.8 | 9.8 | 9.5 |
| ≥ 2023 | 11.7 | 11.2 | 10.9 | 11.0 | 10.8 | 9.8 | 9.5 |

Table 13.2-2: [DX HVAC] ER Baseline Part-Load Efficiency for ACs

| Year Installed (Replaced System) | Split < 3.75 ton [SEER2] | Split < 5.4 tons [SEER2] | Packaged < 5.4 tons [SEER2] | All 5.4 to < 11.3 ton [IEER] | All 11.3 to < 20 tons [IEER] | All 20 to < 63.3 tons [IEER] | All ≥ 63.3 tons [IEER] |
|-------------------------------------|--------------------------------|--------------------------------|-----------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------|
| ≤ 2009 | 12.4 | 12.4 | 12.4 | 10.3 | 9.7 | 9.4 | 9.1 |
| 2010 – 2017 | 12.4 | 12.4 | 12.4 | 11.2 | 11.0 | 9.9 | 9.6 |
| 2018 – 2022 | 12.4 | 12.4 | 13.4 | 12.6 | 12.2 | 11.4 | 11.0 |
| ≥ 2023 | 14.3 | 13.8 | 13.4 | 14.6 | 14.0 | 13.0 | 12.3 |

Table 13.2-3: [DX HVAC] ER Baseline Full-Load Cooling Efficiency for HPs

| Year Installed (Replaced System) | Split < 5.4 tons [EER2] | Packaged < 5.4 tons [EER2] | All 5.4 to < 11.3 tons [EER] | All 11.3 to < 20 tons [EER] | All 20 to < 63.3 tons [EER] | All ≥ 63.3 tons [EER] |
|-------------------------------------|-------------------------------|----------------------------------|------------------------------------|-----------------------------------|-----------------------------------|-----------------------------|
| ≤ 2009 | 10.1 | 10.1 | 10.1 | 9.3 | 9.0 | 9.0 |
| 2010 – 2017 | 10.1 | 10.1 | 11.0 | 10.6 | 9.5 | 9.5 |
| 2018 – 2022 | 10.9 | 10.9 | 11.0 | 10.6 | 9.5 | 9.5 |
| ≥ 2023 | 11.7 | 10.9 | 11.0 | 10.6 | 9.5 | 9.5 |

Table 13.2-4: [DX HVAC] ER Baseline Part-Load Cooling Efficiency for HPs

| Year Installed (Replaced System) | Split < 5.4 tons [SEER2] | Packaged < 5.4 tons [SEER2] | All 5.4 to < 11.3 tons [IEER] | All 11.3 to < 20 tons [IEER] | All 20 to < 63.3 tons [IEER] | All ≥ 63.3 tons [IEER] |
|-------------------------------------|--------------------------------|-----------------------------------|-------------------------------------|------------------------------------|------------------------------------|------------------------------|
| ≤ 2009 | 12.4 | 12.4 | 10.3 | 9.5 | 9.1 | 9.1 |
| 2010 – 2017 | 12.4 | 12.4 | 11.2 | 10.7 | 9.6 | 9.6 |
| 2018 – 2022 | 13.4 | 13.4 | 12.0 | 11.6 | 10.6 | 10.6 |
| ≥ 2023 | 14.3 | 13.4 | 14.1 | 13.5 | 12.5 | 12.5 |

Table 13.2-5: [DX HVAC] ER Baseline Heating Efficiency for HPs

| Year Installed (Replaced System) | Split < 5.4 tons [HSPF2] | Packaged < 5.4 tons [HSPF2] | All 5.4 to < 11.3 tons [COP] | All ≥ 11.3 to < 20 tons [COP] | All ≥ 20 tons [COP] |
|-------------------------------------|--------------------------------|-----------------------------------|------------------------------------|-------------------------------------|---------------------------|
| ≤ 2009 | 6.5 | 6.5 | 3.2 | 3.1 | 3.1 |
| 2010 – 2017 | 6.5 | 6.5 | 3.3 | 3.2 | 3.2 |
| 2018 – 2022 | 6.9 | 6.7 | 3.3 | 3.2 | 3.2 |
| ≥ 2023 | 7.5 | 6.7 | 3.4 | 3.3 | 3.2 |

Replace-on-Burnout and New Construction

Baseline efficiency levels for package and split DX ACs and HPs are provided in Table 13.2-6. The baseline part-load efficiency levels reflect the latest minimum efficiency requirements from the current federal standard, effective January 1, 2023, for units with a rated cooling capacity of less than 65,000 Btu/hour

(Btuh) (5.42 tons) and for units rated between 65,000-759,999 Btuh. Full load efficiency levels are estimated for < 65,000 Btuh systems using a comparison of AHRI SEER2 and EER2 efficiency ratings. Part-load efficiency for 760,000+ Btuh systems and full-load efficiency for 65,000+ Btuh systems are specified in IECC 2015.⁵⁴⁴

An updated federal standard, effective September 17, 2024 with a manufacturing compliance date of January 1, 2029, will establish new integrated ventilation, economizing, and cooling (IVEC) and integrated ventilation and heating efficiency (IVHE) minimum efficiency requirements. After the compliance date, IVEC will replace IEER, and IVHE will replace COP.

For ACs, baseline cooling efficiencies are specified for a natural gas furnace heating section type. For HPs, baseline cooling efficiencies are specified for electric resistance supplemental heating section type. For all other heating section types, or for no heating section type, the baseline efficiencies may need to be adjusted as specified by the footnotes in the tables.

Table 13.2-6: [DX HVAC] Baseline Efficiencies for ROB and NC Air Conditioners and Heat Pump⁵⁴⁵

| System Type | Capacity [Tons] | Baseline Efficiencies |
|-----------------|---|--|
| Air Conditioner | Split < 3.75 | 11.7 EER2 14.3 SEER2 |
| | Split ≥ 3.75 to < 5.42 | 11.2 EER2 13.8 SEER2 |
| | Packaged < 5.42 tons | 10.9 EER2 ⁵⁴⁶ 13.4 SEER2 |
| | All < 5.42 tons rated at ≥15.2 SEER2 | 9.8 EER2 ⁵⁴⁷ |
| | 5.42 to < 11.3 | 11.0 EER 14.6 IEER |
| | 11.3 to < 20 | 10.8 EER 14.0 IEER |
| | 20 to < 63.3 | 9.8 EER 13.0 IEER |

⁵⁴² US Department of Energy (DOE) federal minimum efficiency standard for < 65,000 btuh systems, 10 CFR 430.32.

<https://www.ecfr.gov/current/title-10/chapter-II/subchapter-D/part-430/subpart-C/section-430.32>.

⁵⁴³ US Department of Energy (DOE) federal minimum efficiency standard for 65,000-759,999 btuh systems, 10 CFR 431.97.

<https://www.ecfr.gov/current/title-10/chapter-II/subchapter-D/part-431/subpart-F/subject-group-ECFR2640f6ad978e4e6/section-431.97>.

⁵⁴⁴ 2015 International Energy Conservation Code (IECC). <https://codes.iccsafe.org/content/IECC2015>.

⁵⁴⁵ International Energy Conservation Code 2021. Table C403.3.2(1) and C403.3.2(2).

⁵⁴⁶ Unspecified EER2 values are calculated by multiplying average EER/EER2 ratios, referencing EER2 values specified in the current federal standard for 12.2 and 11.7 EER.

⁵⁴⁷ When installing any system with a part-load efficiency rating of 15.2 SEER2 or higher, the reduced 9.8 EER2 full-load efficiency baseline should be applied in lieu of the applicable value presented earlier in the table except where the specified baseline EER2 value is lower than 9.8 EER2.

| System Type | Capacity [Tons] | Baseline Efficiencies |
|---------------------|---|--|
| | ≥ 63.3 | 9.5 EER 12.3 IEER |
| Heat Pump (cooling) | Split < 5.42 | 11.7 EER2 14.3 SEER2 |
| | Packaged < 5.42 | 10.9 EER2 ⁵⁴⁸ 13.4 SEER2 |
| | All < 5.42 tons rated at ≥15.2 SEER2 | 9.8 EER2 ⁵⁴⁹ |
| | 5.42 to < 11.3 | 11.0 EER 14.1 IEER |
| | 11.3 to < 20 | 10.6 EER 13.5 IEER |
| | ≥ 20 | 9.5 EER 12.5 IEER |
| Heat Pump (heating) | Split < 5.42 | 7.5 HSPF2 |
| | Packaged < 5.42 | 6.7 HSPF2 |
| | 5.42 to < 11.3 | 3.4 COP |
| | ≥ 11.3 to < 20 | 3.3 COP |
| | ≥ 20 | 3.2 COP |

13.2.1.3 High-Efficiency Condition

Split and packaged systems must exceed the minimum efficiencies specified in Table 13.2-6. Split system efficiencies are driven primarily by the efficiency of the condenser unit. If the paired outdoor and indoor units are not listed on the AHRI certification listing and only provide DOE CCMS testing results, then the capacity and efficiency of the high-efficiency condition shall not exceed the average of the AHRI certification listing pairing for the matching condenser. The DOE CCMS listing provides documentation of the results that are on the AHRI certification listing and can be downloaded and filtered based on listing using a similar condenser and various indoor units.

For reference, both ENERGY STAR⁵⁵⁰ and the Consortium for Energy Efficiency (CEE)⁵⁵¹ offer suggested

⁵⁴⁸ Unspecified EER2 values are calculated by multiplying average EER/EER2 ratios, referencing values specified in the current federal standard for 12.2 and 11.7 EER.

⁵⁴⁹ When installing any system with a part-load efficiency rating of 15.2 SEER2 or higher, the reduced 9.8 EER2 full-load efficiency baseline should be applied in lieu of the applicable value presented earlier in the table except where the specified baseline EER2 value is lower than 9.8 EER2.

⁵⁵⁰ ENERGY STAR Heating & Cooling, https://www.energystar.gov/products/heating_cooling.

⁵⁵¹ CEE Program Resources, <http://www.cee1.org/content/cee-program-resources>.

guidelines for high-efficiency equipment. Additional conditions for ER, ROB, and NC are as follows.

New Construction and Replace-on-Burnout

This scenario includes equipment used for NC and retrofit/replacements that do not satisfy the ER criteria, such as units that are replaced after natural failure.

Early Retirement

The high-efficiency retrofits must meet the following criteria:

- For ER projects only, when downsizing, the pre-installed cooling capacity is limited to a maximum of 120 percent off the new equipment's cooling capacity. There is no limit on upsizing because the savings are calculated using the lower pre-capacity.
- For scenarios involving the replacement of a combination of systems by an alternate combination of systems of varying capacities, ER savings can still be claimed if the overall pre and post capacities for the total combination of systems are compliant with the guidance in the previous bullet. In these cases, a custom calculation should be performed to establish the following weighted savings factors to be applied over the ER portion of the savings calculation: manufacturer year, EUL, RUL, full- and part-load baseline efficiency, EFLH, and demand factor. These factors should be weighted based on contribution to overall capacity.
- No additional measures may be installed that directly affect the operation of the cooling equipment (i.e., control sequences, cooling towers, and condensers).

13.2.2 Energy and Demand Savings Methodology

13.2.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{Savings,C} + kWh_{Savings,H}$$

Equation 13.2-1

$$kWh_{Savings,C} = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times \frac{EFLH_C}{1,000}$$

Equation 13.2-2

$$kWh_{Savings,H} = \left(\frac{Cap_{H,pre}}{\eta_{baseline,H}} - \frac{Cap_{H,post}}{\eta_{installed,H}} \right) \times \frac{EFLH_H}{3,412}$$

Equation 13.2-3

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \left(\frac{\text{Cap}_{C,pre}}{\eta_{baseline,C}} - \frac{\text{Cap}_{C,post}}{\eta_{installed,C}} \right) \times \frac{DF}{1,000}$$

Equation 13.2-4

Where:

$\text{Cap}_{C/H,pre}$ = For ER and ROB, rated equipment cooling/heating capacity of the existing equipment at AHRI standard conditions with a maximum of 20% larger than the post capacity; for NC, rated equipment cooling/heating capacity of the new equipment at AHRI conditions [Btuh];
1 ton = 12,000 Btuh.

$\text{Cap}_{C/H,post}$ = Rated equipment cooling/heating capacity of the newly installed equipment at AHRI standard conditions with a maximum equal to the baseline pre capacity [Btuh]; 1 ton = 12,000 Btuh.

Note: The capacity in the equations may not always match the capacity of the units.

$\eta_{baseline,C}$ = Cooling efficiency of existing equipment (ER) or standard equipment (ROB/NC) [Btuh/W].

$\eta_{installed,C}$ = Rated cooling efficiency of the newly installed equipment [Btuh/W]. Efficiency rating must exceed ROB/NC baseline efficiency standards in Table 13.2-6.

$\eta_{baseline,H}$ = Heating efficiency of existing equipment (ER) or standard equipment (ROB/NC) [COP].

$\eta_{installed,H}$ = Rated heating efficiency of the newly installed equipment (Must exceed baseline efficiency standards in Table 13.2-6) [COP].

Note: Use EER2/EER for kW savings calculations and SEER2/IEER and COP for kWh savings calculations. The COP expressed for units > 5.4 tons is a full-load COP. Heating efficiencies expressed as HSPF will be approximated as a seasonal COP and should be converted by using the following equation:

$$\text{COP} = \frac{\text{HSPF}}{3.412}$$

Equation 13.2-5

DF = Demand factor (NCP, CP, or 4CP) for appropriate building type and equipment type; see Table 13.2-10 through Table 13.2-12.

$EFLH_{C/H}$ = Cooling/heating equivalent full-load hours for appropriate building type and equipment type [hours]; see Table 13.2-9.

1,000 = Constant to convert from watts to kilowatts.

3,412 = Constant to convert from Btu to kWh.

Early Retirement

The first-year savings algorithms in the above equations are used for all HVAC projects, across NC, ROB, and ER projects. However, ER projects require weighted savings calculated over both the ER and ROB periods, accounting for both the EUL and RUL. The ER savings are applied over the remaining useful life (RUL) period, and the ROB savings are applied over the remaining period (EUL-RUL). The final reported savings for ER projects are not actually a “first-year” savings, but an “average annual savings over the lifetime (EUL) of the measure.” These savings calculations are explained in Section 22.1.

System Type Conversion

Chiller to AC: Conversions from chiller-based systems to a split/package AC system are covered under this measure. The reference tables in the HVAC Chillers measure for the savings.

AC to HP: Conversions from AC to HP are acceptable in commercial applications. Use CAP_H , $\eta_{baseline,H}$, DF_H , and $EFLH_H$ values for the new HP as a proxy for the baseline AC heating savings coefficients.

13.2.2.2 Deemed Energy Savings Tables

Table 13.2-9 contains the effective full load hours for commercial ACs and HPs for various building types in San Antonio. These building types are derived from the EIA CBECS study.⁵⁵²

Building Type Selection. In situations where multiple TRM building types seem plausible or a predominant TRM building type is unclear, the utilities have two choices:

- **Deemed approach.** The deemed approach is a simplified method where utilities should choose a TRM building type based on the “best fit” for the facility. This is determined by the largest interior area for the potential building types. Although, if that is not best fit, the utilities will use their best judgment to make this decision and provide sufficient, defensible documentation for their decision.

The following building type combinations are pre-authorized exceptions to this rule. For these combinations, individual fixtures can be reported as either specified building type based on location. All other interior space combinations should reference a single deemed building type unless authorized by the evaluator.

- Office (any size) – Warehouse
- Hospital – Outpatient healthcare

⁵⁵² (CBECS) implemented by the US Energy Information Administration includes a principal building activity categorization scheme that separates the commercial sector into 29 categories and 51 subcategories based on principal building activity (PBA). For its purposes, the CBECS defines commercial buildings as those buildings greater than 1,000 square feet that devote more than half of their floorspace to activity that is neither residential, manufacturing, industrial, nor agricultural. The high-level building types adopted for the Guidebook are adapted from this CBECS categorization, with select building types added/removed. <https://www.eia.gov/consumption/commercial/>.

The “Other” building type can be used for business types that are not explicitly listed. The DF and EFLH values used for Other are the most conservative from the explicitly listed building types. When the Other building type is used, a description of the actual building type, the primary business activity, the business hours, and the HVAC schedule must be collected for the project site and stored in the utility tracking data system.

- For those combinations of technology, climate zone, and building type with no values, a project with that specific combination should use the “Other” building type.
- **Custom approach.** In more unique situations, utilities should consider projects “custom” where (1) the deemed building types in the TRM may not represent the project’s facility type, (2) the facility may represent multiple TRM building types without a clear predominant building type, or (3) the use of a predominant building type may be too conservative in the estimate of savings. The deemed methods only apply to specific scenarios and cannot be developed for all unique situations. Defensible documentation for HOU and CF assumptions should be provided.

Table 13.2-7: [DX HVAC] Commercial HVAC Building Type Descriptions and Examples

| Building Type | Principal Building Activity | Definition | Detailed Business Type Examples ⁵⁵³ |
|---------------|---------------------------------|---|--|
| Data Center | Data Center | Buildings used to house computer systems and associated components. | <ul style="list-style-type: none"> • Data Center |
| Education | College | Buildings used for academic or technical classroom instruction, such as elementary, middle, or high schools, and classroom buildings on college or university campuses. Buildings on education campuses for which the main use is not classroom are included in the category relating to their use. For example, administration buildings are part of “Office,” dormitories are “Lodging,” and libraries are “Public Assembly.” | <ul style="list-style-type: none"> • College or University • Career or Vocational Training • Adult Education • Elementary or Middle School (grade 8 or lower) • Preschool or Daycare • High School (grade 9 or greater) • Religious Education |
| | Primary School | | |
| | Secondary School ⁵⁵⁴ | | |
| Food Sales | Convenience | Buildings used for retail or wholesale of food. | <ul style="list-style-type: none"> • Gas Station with a Convenience Store • Convenience Store • Grocery Store or Food Market |
| | Supermarket | | |
| Food | Full-Service | Buildings used for preparation and sale | |

⁵⁵³ Principal Building Activities are based on sub-categories from CBECS questionnaire.

<https://www.eia.gov/consumption/commercial/building-type-definitions.php>

⁵⁵⁴ Individual middle and junior high schools may have a campus size and building activities that better align with secondary schools. The use of secondary school assumptions in lieu of primary school assumptions is subject to evaluator pre-approval. Otherwise, Education subcategory should be determined by lowest grade.

| Building Type | Principal Building Activity | Definition | Detailed Business Type Examples ⁵⁵³ |
|-------------------|-----------------------------|---|---|
| Service | Restaurant | of food and beverages for consumption. | <ul style="list-style-type: none"> • Restaurant or Cafeteria • Fast Food |
| | Quick-Service Restaurant | | |
| Healthcare | Hospital | Buildings used as diagnostic and treatment facilities for inpatient care. Buildings used as diagnostic and treatment facilities for outpatient care. Medical offices are included here if they use any type of diagnostic medical equipment (if they do not, they are categorized as an office building). | <ul style="list-style-type: none"> • Hospital • Inpatient Rehabilitation • Medical Office • Clinic or Outpatient Health Care • Veterinarian |
| | Outpatient Healthcare | | |
| Large Multifamily | Midrise Apartment | Buildings containing multifamily dwelling units, having multiple stories, and equipped with elevators. | No sub-categories collected. |
| Lodging | Large Hotel | Buildings used to offer multiple accommodations for short-term or long-term residents, including skilled nursing and other residential care buildings. | <ul style="list-style-type: none"> • Motel or Inn • Hotel • Dormitory, Fraternity, or Sorority • Retirement Home, Nursing Home, Assisted Living, or other Residential Care • Convent or Monastery |
| | Nursing Home | | |
| | Small Hotel/Motel | | |
| Mercantile | Stand-Alone Retail | Buildings used for the sale and display of goods other than food. Shopping malls comprised of multiple connected establishments. | <ul style="list-style-type: none"> • Retail Store • Beer, Wine, or Liquor Store • Rental Center • Dealership or Showroom for Vehicles or Boats • Studio or Gallery • Strip Shopping Center • Enclosed Malls |
| | Strip Mall | | |
| Office | Large Office | Buildings used for general office space, professional office, or administrative offices. Medical offices are included here if they do not use any type of diagnostic medical equipment (if they do, they are categorized as an outpatient health care building). | <ul style="list-style-type: none"> • Administrative or Professional Office • Government Office • Mixed-Use Office • Bank or Other Financial Institution • Medical Office • Sales Office • Contractor's Office (e.g., Construction, Plumbing, HVAC) |
| | Medium Office | | |

| Building Type | Principal Building Activity | Definition | Detailed Business Type Examples ⁵⁵³ |
|-------------------|-----------------------------|---|--|
| | Small Office | | <ul style="list-style-type: none"> • Non-Profit or Social Services • Research and Development • City Hall or City Center • Religious Office • Call Center |
| Public Assembly | Public Assembly | Buildings in which people gather for social or recreational activities, whether in private or non-private meeting halls. | <ul style="list-style-type: none"> • Social or Meeting (e.g., Community Center, Lodge, Meeting Hall, Convention Center, Senior Center) • Recreation (e.g., Gymnasium, Health Club, Bowling Alley, Ice Rink, Field House, Indoor Racquet Sports) • Entertainment or Culture (e.g., Museum, Theater, Cinema, Sports Arena, Casino, Night Club) • Library • Funeral Home • Student Activities Center • Armory • Exhibition Hall • Broadcasting Studio • Transportation Terminal |
| Religious Worship | Religious Worship | Buildings in which people gather for religious activities, (such as chapels, churches, mosques, synagogues, and temples). | No sub-categories collected. |
| Service | Service | Buildings in which some type of service is provided, other than food service or retail sales of goods. | <ul style="list-style-type: none"> • Vehicle Service or Vehicle Repair Shop • Vehicle Storage/Maintenance • Repair Shop • Dry Cleaner or Laundromat • Post Office or Postal Center • Car Wash • Gas Station with no Convenience Store • Photo Processing Shop • Beauty Parlor or Barber Shop • Tanning Salon • Copy Center or Printing Shop • Kennel |
| Warehouse | Warehouse | Buildings used to store goods, manufactured products, merchandise, raw materials, or personal belongings | <ul style="list-style-type: none"> • Refrigerated Warehouse • Non-refrigerated warehouse • Distribution or Shipping Center |

| Building Type | Principal Building Activity | Definition | Detailed Business Type Examples ⁵⁵³ |
|---------------|-----------------------------|-------------------------|--|
| | | (such as self-storage). | |
| Other | Other | Other | For building types not explicitly listed. |

Table 13.2-8: [DX HVAC] Floor Area and Floor Assumptions by Building Type

| Building Type | Principal Building Activity | Average Floor Area (ft ²) | Average # Floors |
|-------------------|-----------------------------|---------------------------------------|------------------|
| Data Center | Data Center | Not specified | Not specified |
| Education | College | Not specified | Not specified |
| | Primary School | 73,960 | 1 |
| | Secondary School | 210,887 | 2 |
| Food Sales | Convenience | Not specified | 1 |
| | Supermarket | 45,000 | 1 |
| Food Service | Full-Service Restaurant | 5,500 | 1 |
| | Quick-Service Restaurant | 2,500 | 1 |
| Healthcare | Hospital | 241,351 | 5 |
| | Outpatient Healthcare | 40,946 | 3 |
| Large Multifamily | Midrise Apartment | 33,740 | 4 |
| Lodging | Large Hotel | 122,120 | 6 |
| | Nursing Home | Not specified | Not specified |
| | Small Hotel/Motel | 43,200 | 4 |
| Mercantile | Stand-Alone Retail | 24,962 | 1 |
| | 24 Hr Stand-Alone Retail | 22,500 | 1 |
| | Strip Mall | 498,588 | 12 |
| Office | Large Office | 53,628 | 3 |
| | Medium Office | 5,500 | 1 |
| | Small Office | Not specified | Not specified |
| Public Assembly | Public Assembly | Not specified | Not specified |
| Religious Worship | Religious Worship | Not specified | Not specified |
| Service | Service | 52,045 | 1 |
| Warehouse | Warehouse | Not specified | Not specified |
| Other | Other | Not specified | Not specified |

Table 13.2-9: [DX HVAC] Equivalent Full-Load Hours

| Building Type | Principal Building Activity | Package and Split DX | | |
|-------------------|-----------------------------|----------------------|-------------------|-------------------|
| | | AC | Heat Pump | |
| | | EFLH _C | EFLH _C | EFLH _H |
| Data Centers | Data Centers | 4,022 | 4,022 | - |
| Education | College | 2,101 | 2,101 | - |
| | Primary School | 1,633 | 1,633 | 251 |
| | Secondary School | 1,429 | 1,429 | 281 |
| Food Sales | Convenience | 2,307 | 2,307 | - |
| | Supermarket | 829 | 829 | - |
| Food Service | Full-Service Restaurant | 2,249 | 2,249 | 542 |
| | 24 Hr Full-Service | 2,548 | 2,548 | 680 |
| | Quick-Service Restaurant | 1,996 | 1,996 | 405 |
| | 24 Hr Quick-Service | 2,311 | 2,311 | 599 |
| Healthcare | Hospital | 3,534 | 3,534 | - |
| | Outpatient Healthcare | 2,925 | 2,925 | 223 |
| Large Multifamily | Midrise Apartment | 2,429 | 2,429 | - |
| Lodging | Large Hotel | 2,600 | 2,600 | 307 |
| | Nursing Home | 2,467 | 2,467 | - |
| | Small Hotel/Motel | 2,421 | 2,421 | 147 |
| Mercantile | Stand-Alone Retail | 1,554 | 1,554 | 230 |
| | 24 Hr Stand-Alone Retail | 2,059 | 2,059 | 276 |
| | Strip Mall | 1,467 | 1,467 | 247 |
| Office | Large Office | 2,866 | 2,866 | 175 |
| | Medium Office | 1,523 | 1,523 | 107 |
| | Small Office | 1,598 | 1,598 | 147 |
| Public Assembly | Public Assembly | 2,196 | 2,196 | - |
| Religious Worship | Religious Worship | 602 | 602 | - |
| Service | Service | 1,742 | 1,742 | - |
| Warehouse | Warehouse | 718 | 718 | - |
| Other | Other | 602 | 602 | 107 |

13.2.2.3 Deemed Demand Savings Tables

Table 13.2-10 through Table 13.2-12 contain the NCP, CP, and 4CP demand factors.

Table 13.2-10: [DX HVAC] Non-Coincident Peak Demand Factors

| Building Type | Principal Building Activity | DF _{NCP} | |
|-------------------|-----------------------------|-------------------|-------|
| | | DX AC | DX HP |
| Data Centers | Data Centers | 1.07 | 1.07 |
| Education | College | 1.12 | 1.12 |
| | Primary School | 1.10 | 1.10 |
| | Secondary School | 1.12 | 1.12 |
| Food Sales | Convenience | 1.13 | 1.13 |
| | Supermarket | 0.65 | 0.65 |
| Food Service | Full-Service Restaurant | 1.13 | 1.13 |
| | 24 Hr Full-Service | 1.14 | 1.14 |
| | Quick-Service Restaurant | 1.13 | 1.13 |
| | 24 Hr Quick-Service | 1.13 | 1.13 |
| Healthcare | Hospital | 0.98 | 0.98 |
| | Outpatient Healthcare | 0.90 | 0.90 |
| Large Multifamily | Midrise Apartment | 1.09 | 1.09 |
| Lodging | Large Hotel | 0.76 | 0.76 |
| | Nursing Home | 1.09 | 1.09 |
| | Small Hotel/Motel | 0.71 | 0.71 |
| Mercantile | Stand-Alone Retail | 1.04 | 1.04 |
| | 24 Hr Stand-Alone Retail | 1.06 | 1.06 |
| | Strip Mall | 1.02 | 1.02 |
| Office | Large Office | 1.09 | 1.09 |
| | Medium Office | 0.90 | 0.90 |
| | Small Office | 1.05 | 1.05 |
| Public Assembly | Public Assembly | 1.10 | 1.10 |
| Religious Worship | Religious Worship | 0.71 | 0.71 |
| Service | Service | 1.13 | 1.13 |
| Warehouse | Warehouse | 1.05 | 1.05 |
| Other | Other | 0.65 | 0.65 |

Table 13.2-11: [DX HVAC] Coincident Peak Demand Factors

| Building Type | Principal Building Activity | Package and Split DX | |
|-------------------|-----------------------------|----------------------|------------------|
| | | AC | Heat Pump |
| | | DF _{CP} | DF _{CP} |
| Data Centers | Data Centers | 1.05 | 1.05 |
| Education | College | 1.08 | 1.08 |
| | Primary School | 1.06 | 1.06 |
| | Secondary School | 1.08 | 1.08 |
| Food Sales | Convenience | 1.03 | 1.03 |
| | Supermarket | 0.61 | 0.61 |
| Food Service | Full-Service Restaurant | 1.06 | 1.06 |
| | 24 Hr Full-Service | 1.07 | 1.07 |
| | Quick-Service Restaurant | 1.03 | 1.03 |
| | 24 Hr Quick-Service | 1.06 | 1.06 |
| Healthcare | Hospital | 0.94 | 0.94 |
| | Outpatient Healthcare | 0.86 | 0.86 |
| Large Multifamily | Midrise Apartment | 1.05 | 1.05 |
| Lodging | Large Hotel | 0.72 | 0.72 |
| | Nursing Home | 1.05 | 1.05 |
| | Small Hotel/Motel | 0.68 | 0.68 |
| Mercantile | Stand-Alone Retail | 1.00 | 1.00 |
| | 24 Hr Stand-Alone Retail | 1.03 | 1.03 |
| | Strip Mall | 0.97 | 0.97 |
| Office | Large Office | 1.07 | 1.07 |
| | Medium Office | 0.83 | 0.83 |
| | Small Office | 1.00 | 1.00 |
| Public Assembly | Public Assembly | 1.06 | 1.06 |
| Religious Worship | Religious Worship | 0.68 | 0.68 |
| Service | Service | 1.06 | 1.06 |
| Warehouse | Warehouse | 0.92 | 0.92 |
| Other | Other | 0.61 | 0.61 |

Table 13.2-12: [DX HVAC] 4CP Demand Factors

| Building Type | Principal Building Activity | Package and Split DX | |
|-------------------|-----------------------------|----------------------|-------------------|
| | | AC | Heat Pump |
| | | DF _{4CP} | DF _{4CP} |
| Data Centers | Data Centers | 0.89 | 0.89 |
| Education | College | 0.91 | - |
| | Primary School | 0.86 | 0.86 |
| | Secondary School | 0.91 | 0.91 |
| Food Sales | Convenience | 0.93 | 0.93 |
| | Supermarket | 0.83 | 0.83 |
| Food Service | Full-Service Restaurant | 0.94 | 0.94 |
| | 24 Hr Full-Service | 0.98 | 0.98 |
| | Quick-Service Restaurant | 0.93 | 0.93 |
| | 24 Hr Quick-Service | 0.97 | 0.97 |
| Healthcare | Hospital | 0.93 | 0.93 |
| | Outpatient Healthcare | 0.93 | 0.93 |
| Large Multifamily | Midrise Apartment | 0.91 | 0.91 |
| Lodging | Large Hotel | 0.89 | 0.89 |
| | Nursing Home | 0.91 | 0.91 |
| | Small Hotel/Motel | 0.87 | 0.87 |
| Mercantile | Stand-Alone Retail | 0.86 | 0.86 |
| | 24 Hr Stand-Alone Retail | 0.88 | 0.88 |
| | Strip Mall | 0.86 | 0.86 |
| Office | Large Office | 0.91 | 0.91 |
| | Medium Office | 0.84 | 0.84 |
| | Small Office | 0.89 | 0.89 |
| Public Assembly | Public Assembly | 0.86 | 0.86 |
| Religious Worship | Religious Worship | 0.87 | 0.87 |
| Service | Service | 0.94 | 0.94 |
| Warehouse | Warehouse | 0.71 | 0.71 |
| Other | Other | 0.71 | 0.71 |

13.2.2.4 Measure Life and Lifetime Savings

Estimated Useful Life (EUL)

The EUL is 15 years for split and packaged ACs and HPs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID HVAC-airAC and HVAC-airHP.⁵⁵⁵

Remaining Useful Life (RUL)

The RUL of replaced systems is provided according to system age in Table 13.2-13. If individual system components were installed at different times, use the condenser age as a proxy for the entire system. For ER units of unknown age, assume a default value equal to the EUL. This corresponds to a default RUL of 2.8 years. Default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible. Both the RUL and EUL are needed to estimate savings for ER projects for two distinct periods: The ER period (RUL) and the ROB period (EUL - RUL). The calculations for ER projects are extensive, and as such are provided in Section 22.1.

Table 13.2-13: [DX HVAC] Remaining Useful Life or Replaced Unit⁵⁵⁶

| Age in Years of Replaced System | Split and Packaged A/C and HP Systems [years] | Age in Years of Replaced System | Split and Packaged A/C and HP Systems [years] |
|---------------------------------|---|---------------------------------|---|
| 1 | 14.0 | 10 | 5.7 |
| 2 | 13.0 | 11 | 5.0 |
| 3 | 12.0 | 12 | 4.4 |
| 4 | 11.0 | 13 | 3.8 |
| 5 | 10.0 | 14 | 3.3 |
| 6 | 9.1 | 15 | 2.8 |
| 7 | 8.2 | 16 | 2.0 |
| 8 | 7.3 | 17 | 1.0 |
| 9 | 6.5 | 18 ⁵⁵⁷ | 0.0 |

⁵⁵⁵ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

⁵⁵⁶ Current NC baseline matches the baseline for existing systems manufactured in 2023. Existing systems manufactured after 1/1/2023 are not eligible to use the early retirement baseline.

⁵⁵⁷ RULs are capped at the 75th percentile of equipment age, 18 years, as determined based on DOE survival curves. Systems older than 18 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

13.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- For Other building types only: A description of the actual building type, the primary business activity, the business hours, and the HVAC schedule
- Baseline type: ER, ROB, NC, system type conversion
- Baseline equipment type
- Baseline unit quantity
- Baseline rated cooling and heating capacities
- For ER ONLY: baseline age and method of determination (e.g., nameplate, blueprints, customer reported, not available)
- For ER ONLY: photograph of retired unit nameplate demonstrating model number, serial number, and manufacturer if blueprints are not provided; if photograph of nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (alternate forms of documentation can be approved at the evaluator's discretion)
- AHRI/DOE CCMS certificates or reference number matching model number
 - For exempted HPs, < 5.4 tons referencing the previous federal standard, a copy of the AHRI certificate or manufacturer specification sheet with date corresponding to the time of application or purchase demonstrating that the unit does not have a SEER2 efficiency rating is required.
- New unit equipment type
- New unit quantity
- New unit manufacturer and model
- New unit rated cooling and heating capacities
- New unit cooling and heating efficiency ratings
- For retrofit only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging or installed unit(s); OR an evaluator pre-approved inspection approach

- For new construction only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging or installed unit(s); as-built design drawings; HVAC specifications package that provides detailed make and model information on installed unit(s); OR an evaluator pre-approved inspection approach

Document Revision History

Table 13.2-14: [DX HVAC] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Removed < 5.4 ton HP sell-through exception. Updated ER baselines for compliance with updated federal standard. Updated NC/ROB 5.4+ ton baselines to incorporate current federal standard. Clarified pre- and post-capacity limits. Aligned building type names across all commercial measures. Incremented RUL table for code compliance. |
| FY 2026 | Defined grade levels for primary and secondary schools, updated early retirement age eligibility and criteria related to downsizing, and noted new federal standard and compliance date. |

13.3 HVAC CHILLERS

13.3.1 Measure Description

This measure presents the deemed savings methodology for the installation of chillers, covering assumptions made for baseline equipment efficiencies for early retirement (ER) based on the age of the replaced equipment and replace-on-burnout (ROB) and new construction (NC) situations based on efficiency standards.

Savings calculations incorporate the use of both full-load and part-load efficiency values. For ER, the actual age of the baseline system should be determined from the equipment nameplate or other physical documentation, whenever possible. Default values are provided for when the actual age of the unit is unknown. Minimum efficiencies are defined in units of kW/ton, the ratio of input power in kW to the cooling capacity in tons, or EER, the ratio of cooling capacity in Btu/h to input power in Watts.

Two paths are currently available for chiller compliance through the IECC and ASHRAE rating standards. Path A requires higher efficiency ratings for full-load operation, with lower ratings for part-load efficiency, and is most applicable to units that are expected to operate at or near fullload conditions. Path B requires higher efficiency ratings for part-load operation, with lower ratings for full-load efficiency, and is most applicable to units that are expected to operate primarily at part-load conditions with variable frequency drives. Either Path can be used for compliance on any particular chiller, but the chiller must meet the minimum requirements for both full and part-load efficiency that are set forth in the following sections.

Applicable efficient measure types include:⁵⁵⁸

- Compressor types: centrifugal or positive-displacement (screw, scroll, or reciprocating)
- Condenser/heat rejection type: air-cooled or water-cooled system type conversions. Retrofits involving a change from a chiller-based system to a packaged/split system are also covered under this measure. If this type of retrofit is performed, reference the tables from the split/single packaged air conditioners and heat pumps measure.
- Chiller type conversions: from an air-cooled chiller system to a water-cooled chiller system is also addressed in this measure. An additional adjustment is made to the basic chiller savings to account for the auxiliary equipment associated with a water-cooled chiller.

⁵⁵⁸ Savings can also be claimed by a retrofit involving a change in equipment type (e.g., air-cooled packaged DX system to a water-cooled centrifugal chiller, or a split system air-cooled heat pump to an air-cooled non-centrifugal chiller). If this type of retrofit is performed, reference the tables from the relevant HVAC measure.

13.3.1.1 Eligibility Criteria

For a measure to be eligible for this deemed savings approach the following conditions must be met:

- The existing and proposed cooling equipment are electric.
- The building falls into one of the categories listed in Table 13.2-7. Building type descriptions and examples are provided in in Table 13.2-7.
- ER projects involve the replacement of a working system that is at least five years old and before natural burnout occurs. The ER approach cannot be used for projects involving a renovation where a major structural change or internal space remodel has occurred. An ROB approach should be used for these scenarios.
- For redundant chiller configurations, the installed chiller must not be exclusively sequenced as a standby chiller. As an example, for N+1 configurations where the redundant chiller is rotated, the deemed savings approach should only be used for N chillers, where N is the total number of chillers in the redundant chiller configuration minus one. Multiple chillers sequenced in a lead-lag or base-trim configuration are eligible to use the deemed savings.
- Manufacturer datasheets for installed equipment or documentation of AHRI or DOE CCMS certification must be provided.^{559,560}

13.3.1.2 Baseline Condition

Early Retirement

ER systems involve the replacement of a working system prior to natural burnout. The ER baseline cannot be used for projects involving a renovation where a major structural change or internal space remodel has occurred.

Two baseline condition efficiency values are required for an ER scenario, one for the ER (RUL) period and one for the ROB (EUL-RUL) period. For the ROB period, the baseline efficiency is the same as for an ROB/NC scenario. For the ER period, the baseline efficiency should be estimated according to the capacity, chiller type, and age (based on year manufactured) of the replaced system.⁵⁶¹ When the chiller age can be determined (from a nameplate, building prints, equipment inventory list, etc.), use the baseline efficiency levels provided in Table 13.3-1 through Table 13.3-11. When the system age is unknown, assume a default value equal to the EUL. This corresponds to 20 years for non-centrifugal chillers and 25 years for centrifugal chillers. A default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented

⁵⁵⁹ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

⁵⁶⁰ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

⁵⁶¹ The actual age should be determined from the nameplate, building prints, equipment inventory list, etc. and whenever possible the actual source used should be identified in the project documentation.

as having a nameplate that is illegible.

ER baseline efficiency values represent the code-specified efficiency in effect at the time the chiller was installed. Prior to 2002, code-specified efficiencies from ASHRAE 90.1-1989 were in effect. Code-specified efficiencies increased in 2002, approximating the effective date of ASHRAE 90.1-1999, which went into effect on October 29, 2001. Code-specified efficiencies increased again in 2010, coinciding with the state of Texas code increase to IECC 2009 (Path A). Code-specified efficiencies increased again in 2010, 2015, 2018, and 2023 coinciding with the IECC 2009, IECC 2015, IECC 2018, and IECC 2021 code updates.

Different code-specified efficiencies were in effect prior to 2010 (ASHRAE 90.1-2010). Those efficiencies were expressed as coefficients of performance (COP). Those COP values have been converted to EER (Energy Efficiency Ratio) and kW/ton in the tables below by using $EER = COP \times 3.412$ and $kW/ton = 3.516 \div COP$. Values in the “< 2001” and “2002-2009” rows of Table 13.3-1, Table 13.3-5, and Table 13.3-9 are converted COP values.

ER Baseline – All Air-Cooled Chillers

Table 13.3-1: [Chillers] ER Baseline Full-Load Efficiency of Path A Air-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [EER] | ≥ 150 tons [EER] |
|--|---------------------|---------------------|
| ≤ 2001 | 9.212 | 8.530 |
| 2002 - 2015 | 9.562 | 9.562 |
| ≥ 2016 | 10.100 | 10.100 |

Table 13.3-2: [Chillers] ER Baseline Full-Load Efficiency of Path B Air-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [EER] | ≥ 150 tons [EER] |
|--|---------------------|---------------------|
| ≤ 2001 | 9.212 | 8.530 |
| 2002 - 2015 | 9.562 | 9.562 |
| ≥ 2016 | 9.700 | 9.700 |

Table 13.3-3: [Chillers] ER Baseline Part-Load Efficiency of Path A Air-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [IPLV] | ≥ 150 tons [IPLV] |
|--|----------------------|----------------------|
| ≤ 2001 | 9.554 | 8.530 |
| 2002 - 2009 | 10.416 | 10.416 |

| Year Installed (Replaced System) | < 150 tons [IPLV] | ≥ 150 tons [IPLV] |
|--|----------------------|----------------------|
| 2010 - 2015 | 12.500 | 12.500 |
| ≥ 2016 | 13.700 | 14.000 |

Table 13.3-4: [Chillers] ER Baseline Part-Load Efficiency of Path B Air-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [IPLV] | ≥ 150 tons [IPLV] |
|--|----------------------|----------------------|
| ≤ 2001 | 9.554 | 8.530 |
| 2002 - 2009 | 10.416 | 10.416 |
| 2010 - 2015 | 12.500 | 12.500 |
| ≥ 2016 | 15.800 | 16.100 |

ER Baseline - Centrifugal Water-Cooled Chillers

Table 13.3-5: [Chillers] ER Baseline Full-Load Efficiency of Path A Centrifugal Water-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [kW/ton] | ≥ 150 to 300 tons [kW/ton] | ≥ 300 to 600 tons [kW/ton] | ≥ 600 tons [kW/ton] |
|--|------------------------|----------------------------------|----------------------------------|------------------------|
| ≤ 2001 | 0.925 | 0.837 | 0.748 | 0.748 |
| 2002 - 2009 | 0.703 | 0.634 | 0.576 | 0.576 |
| 2010 - 2015 | 0.634 | 0.634 | 0.576 | 0.570 |
| ≥ 2016 | 0.610 | 0.610 | 0.560 | 0.560 |

Table 13.3-6: [Chillers] ER Baseline Full-Load Efficiency of Path B Centrifugal Water-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [kW/ton] | ≥ 150 to 300 tons [kW/ton] | ≥ 300 to 600 tons [kW/ton] | ≥ 600 tons [kW/ton] |
|--|------------------------|----------------------------------|----------------------------------|------------------------|
| ≤ 2001 | 0.925 | 0.837 | 0.748 | 0.748 |
| 2002 - 2009 | 0.703 | 0.634 | 0.576 | 0.576 |
| 2010 - 2015 | 0.639 | 0.639 | 0.600 | 0.590 |
| ≥ 2016 | 0.695 | 0.635 | 0.595 | 0.585 |

Table 13.3-7: [Chillers] ER Baseline Part-Load Efficiency of Path A Centrifugal Water-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [IPLV] | ≥ 150 to 300 tons [IPLV] | ≥ 300 to 600 tons [IPLV] | ≥ 600 tons [IPLV] |
|--|----------------------|--------------------------------|--------------------------------|----------------------|
| ≤ 2001 | 0.902 | 0.781 | 0.733 | 0.733 |
| 2002 - 2009 | 0.670 | 0.596 | 0.549 | 0.549 |
| 2010 - 2015 | 0.596 | 0.596 | 0.549 | 0.539 |
| ≥ 2016 | 0.550 | 0.550 | 0.520 | 0.500 |

Table 13.3-8: [Chillers] ER Baseline Part-Load Efficiency of Path B Centrifugal Water-Cooled Chillers

| Year Installed (Replaced System) | < 150 tons [IPLV] | ≥ 150 to 300 tons [IPLV] | ≥ 300 to 600 tons [IPLV] | ≥ 600 tons [IPLV] |
|--|----------------------|--------------------------------|--------------------------------|----------------------|
| ≤ 2001 | 0.902 | 0.781 | 0.733 | 0.733 |
| 2002 - 2009 | 0.670 | 0.596 | 0.549 | 0.549 |
| 2010 - 2015 | 0.450 | 0.450 | 0.400 | 0.400 |
| ≥ 2016 | 0.440 | 0.400 | 0.390 | 0.380 |

ER Baseline - Positive-Displacement Water-Cooled Chillers

Table 13.3-9: [Chillers] ER Baseline Full-Load Efficiency of Path A Screw/Scroll/Recip. Water-Cooled Chillers

| Year Installed (Replaced System) | < 75 tons [kW/ton] | ≥75 to 150 tons [kW/ton] | ≥ 150 to 300 tons [kW/ton] | ≥ 300 to 600 tons [kW/ton] | ≥ 600 tons [kW/ton] |
|--|-----------------------|--------------------------------|----------------------------------|----------------------------------|---------------------------|
| ≤ 2001 | 0.925 | 0.925 | 0.837 | 0.748 | 0.748 |
| 2002 - 2009 | 0.790 | 0.790 | 0.718 | 0.639 | 0.639 |
| 2010 - 2015 | 0.780 | 0.775 | 0.680 | 0.620 | 0.620 |
| ≥ 2016 | 0.750 | 0.720 | 0.660 | 0.610 | 0.560 |

Table 13.3-10: [Chillers] ER Baseline Full-Load Efficiency of Path B Screw/Scroll/Recip. Water-Cooled Chillers

| Year Installed (Replaced System) | < 75 tons [kW/ton] | ≥75 to 150 tons [kW/ton] | ≥ 150 to 300 tons [kW/ton] | ≥ 300 to 600 tons [kW/ton] | ≥ 600 tons [kW/ton] |
|--|-----------------------|--------------------------------|----------------------------------|----------------------------------|---------------------------|
| ≤ 2001 | 0.925 | 0.925 | 0.837 | 0.748 | 0.748 |
| 2002 - 2009 | 0.790 | 0.790 | 0.718 | 0.639 | 0.639 |
| 2010 - 2015 | 0.800 | 0.790 | 0.718 | 0.639 | 0.639 |
| ≥ 2016 | 0.780 | 0.750 | 0.680 | 0.625 | 0.585 |

Table 13.3-11: [Chillers] ER Baseline Part-Load Efficiency of Path A Screw/Scroll/Recip. Water-Cooled Chillers

| Year Installed (Replaced System) | < 75 tons [IPLV] | ≥75 to 150 tons [IPLV] | ≥ 150 to 300 tons [IPLV] | ≥ 300 to 600 tons [IPLV] | ≥ 600 tons [IPLV] |
|--|---------------------|------------------------------|--------------------------------|--------------------------------|-------------------------|
| ≤ 2001 | 0.902 | 0.902 | 0.781 | 0.733 | 0.733 |
| 2002 - 2009 | 0.676 | 0.676 | 0.628 | 0.572 | 0.572 |
| 2010 - 2015 | 0.630 | 0.615 | 0.580 | 0.540 | 0.540 |
| ≥ 2016 | 0.600 | 0.560 | 0.540 | 0.520 | 0.500 |

Table 13.3-12: [Chillers] ER Baseline Part-Load Efficiency of Path B Screw/Scroll/Recip. Water-Cooled Chillers

| Year Installed (Replaced System) | < 75 tons [IPLV] | ≥75 to 150 tons [IPLV] | ≥ 150 to 300 tons [IPLV] | ≥ 300 to 600 tons [IPLV] | ≥ 600 tons [IPLV] |
|--|---------------------|------------------------------|--------------------------------|--------------------------------|-------------------------|
| ≤ 2001 | 0.902 | 0.902 | 0.781 | 0.733 | 0.733 |
| 2002 - 2009 | 0.676 | 0.676 | 0.628 | 0.572 | 0.572 |
| 2010 - 2015 | 0.600 | 0.586 | 0.540 | 0.490 | 0.490 |
| ≥ 2016 | 0.500 | 0.490 | 0.440 | 0.410 | 0.380 |

Replace-on-Burnout and New Construction

New baseline efficiency levels for chillers are provided in Table 13.3-13, which includes both full load and Integrated Part Load Value (IPLV) ratings. The IPLV rating accounts for chiller efficiency at part-load operation for a given duty cycle. These baseline efficiency levels reference standard IECC 2021. This standard contains two paths for compliance, Path A or Path B. Path A is intended for applications where significant operating time is expected at full-load conditions, while Path B is an alternative set of efficiency levels for chillers intended for applications where considerable time is spent at part-load operation (such as with a VSD chiller). Both paths are eligible to claim demand savings using the applicable full-load baseline efficiencies for the selected path in combination with the demand coefficients defined in this measure. Similarly, both paths are eligible to claim energy savings using the applicable part-load baseline efficiencies for the selected path in combination with the energy coefficients defined in this measure.

Table 13.3-13: [Chillers] Baseline Efficiencies for ROB and NC Air-Cooled and Water-Cooled Chillers⁵⁶²

| System Type | Equipment Type | Efficiency Type | Capacity [Tons] | Path A | | Path B | |
|----------------|-------------------|--------------------|--------------------|-----------|----------|-----------|----------|
| | | | | Full-Load | IPLV | Full-Load | IPLV |
| Air-Cooled | All | EER | < 150 | ≥ 10.100 | ≥ 13.700 | ≥ 9.700 | ≥ 15.800 |
| | | | ≥ 150 | ≥ 10.100 | ≥ 14.000 | ≥ 9.700 | ≥ 16.100 |

⁵⁶² International Energy Conservation Code 2021. Table C403.3.2(3).

| System Type | Equipment Type | Efficiency Type | Capacity [Tons] | Path A | | Path B | |
|--------------|--|-----------------|-----------------|-----------|---------|-----------|---------|
| | | | | Full-Load | IPLV | Full-Load | IPLV |
| Water-Cooled | Electric, Positive Displacement (Screw/Scroll/Reciprocating) | kW/ton | < 75 | ≤ 0.750 | ≤ 0.600 | ≤ 0.780 | ≤ 0.500 |
| | | | ≥ 75 and < 150 | ≤ 0.720 | ≤ 0.560 | ≤ 0.750 | ≤ 0.490 |
| | | | ≥ 150 and < 300 | ≤ 0.660 | ≤ 0.540 | ≤ 0.680 | ≤ 0.440 |
| | | | ≥ 300 and < 600 | ≤ 0.610 | ≤ 0.520 | ≤ 0.625 | ≤ 0.410 |
| | | | ≥ 600 | ≤ 0.560 | ≤ 0.500 | ≤ 0.585 | ≤ 0.380 |
| | Electric, Centrifugal | kW/ton | < 150 | ≤ 0.610 | ≤ 0.550 | ≤ 0.695 | ≤ 0.440 |
| | | | ≥ 150 and < 300 | ≤ 0.610 | ≤ 0.550 | ≤ 0.635 | ≤ 0.400 |
| | | | ≥ 300 and < 400 | ≤ 0.560 | ≤ 0.520 | ≤ 0.595 | ≤ 0.390 |
| | | | ≥ 400 | ≤ 0.560 | ≤ 0.500 | ≤ 0.585 | ≤ 0.380 |

13.3.1.3 High-Efficiency Condition

Chillers must exceed the minimum efficiencies specified in Table 13.3-13 for either Path A or Path B. For whichever path is used, the chiller must exceed the minimum baseline efficiency for both full-load and IPLV of that path to qualify. Additional conditions for ROB, ER, and NC are as follows:

New Construction and Replace-on-Burnout

This scenario includes chillers used for NC and retrofit/replacements that are not covered by ER, such as units that are replaced after natural failure.

Early Retirement

The high-efficiency retrofits must meet the following criteria:

- For ER projects only, when downsizing, the pre-installed cooling capacity is limited to a maximum of 120 percent of the new equipment's cooling capacity. There is no cap on upsizing because the savings are calculated using the lower pre-capacity.

For scenarios involving the replacement of a combination of systems by an alternate combination of systems of varying capacities, ER savings can still be claimed if the overall pre and post capacities for the total combination of systems are compliant with the guidance in the previous bullet. In these cases, a custom calculation should be performed to establish the following weighted savings factors to be applied over the ER portion of the savings calculation:

manufacturer year, EUL, RUL, path A/B full- and part-load baseline efficiency, EFLH, and demand factor. These factors should be weighted based on contribution to overall capacity.

- No additional measures are being installed that directly affect the operation of the cooling equipment (i.e., control sequences, cooling towers, and condensers).

13.3.2 Energy and Demand Savings Methodology

13.3.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = (Cap_{C,pre} \times \eta_{baseline} - Cap_{C,post} \times \eta_{installed}) \times EFLH_c$$

Equation 13.3-1

Demand Savings

$$\text{Demand Savings } [\Delta kW] = (Cap_{C,pre} \times \eta_{baseline} - Cap_{C,post} \times \eta_{installed}) \times DF$$

Equation 13.3-2

Where:

$Cap_{C,pre}$ = For ER and ROB, rated equipment cooling capacity of the existing equipment at AHRI standard conditions with a maximum of 20 percent larger than the post-capacity; for NC, rated equipment cooling capacity of the new equipment at AHRI standard conditions [Tons].

$Cap_{C,post}$ = Rated equipment cooling capacity of the newly installed equipment at AHRI standard conditions with a maximum equal to the baseline pre-capacity [Tons].

Note: The capacity in the equations may not always match the capacity of the units

$\eta_{baseline}$ = Efficiency of existing equipment (ER) or standard equipment (ROB/NC) [kW/Ton] Use Table 13.3-1 through Table 13.3-11 or Equation 13.3-3.

$\eta_{installed}$ = Rated efficiency of the newly installed equipment [kW/Ton] Rated efficiency must exceed efficiency standards, shown in Table 13.3-13.

$EFLH_c$ = Cooling equivalent full-load hours for appropriate building type, and equipment type [hours]; see Table 13.3-14.

DF = Demand factor (NCP, CP, 4CP) for appropriate building type and equipment type; see Table 13.3-15 through Table 13.3-17.

EER Efficiency Ratings – All Air-Cooled Chillers:

Use full-load efficiency [kW/ton] for kW savings calculations and part-load efficiency [IPLV] for kWh savings calculations. Table 13.3-1 through Table 13.3-11 provide efficiency ratings for baseline equipment where the efficiency ratings are given in terms of EER, kW/ton, or IPLV. In the cases where the full-load efficiency of the baseline or installed equipment is provided in terms of EER rather than kW/ton, a conversion to kW/ton needs to be performed using the following conversion:

$$\frac{kW}{Ton} = \frac{12}{EER}$$

Equation 13.3-3

Air-to Water-Cooled Replacement: Adjustments for Auxiliary Equipment:

The equipment efficiency for an air-cooled chiller includes condenser fans, but the equipment efficiency for a water-cooled chiller does not include the condenser water pump and cooling tower (auxiliary equipment). Therefore, when an air-cooled chiller is replaced with a water-cooled chiller, the savings must be reduced to account for the impact of the water-cooled system's additional equipment. This type of retrofit is only applicable for ER situations. The following equations are used:

$$kW_{adj} = (HP_{CW\ pump} + HP_{CT\ fan}) \times \frac{0.746}{0.86} \times 0.80$$

Equation 13.3-4

$$kWh_{adj} = kW \times 8,760$$

Equation 13.3-5

Where:

$HP_{CW\ pump}$ = Horsepower of the condenser water pump.

$HP_{CT\ fan}$ = Horsepower of the cooling tower fan.

0.746 = Conversion from hp to kW [kW/hp].

0.86 = Assumed equipment efficiency.

0.80 = Assumed load factor.

8,760 = Total hours per year.

The energy and demand of the condenser water pump and cooling tower fans are subtracted from the final savings, to reach the net savings.

$$kW_{savings,net} = kW_{Chiller} - kW_{adj}$$

Equation 13.3-6

$$kWh_{savings,net} = kWh_{chiller} - kWh_{adj}$$

Equation 13.3-7

Early Retirement

The first-year savings algorithms in the above equations are used for all HVAC projects, across NC, ROB, and ER projects. However, ER projects require weighted savings calculated over both the ER period and the ROB period, accounting for the EUL and the RUL. The final reported savings for ER projects are not actually a “first-year” savings, but an “average annual savings over the lifetime (EUL) of the measure.” These savings calculations are explained in Section 22.1. Table 13.3-14 through Table 13.3-17 present the demand and energy coefficients as well as the Part Load Factor. These HVAC coefficients vary by climate zone, building type, and equipment type.

13.3.2.2 Deemed Energy Savings Tables

Deemed equivalent full-load hour (EFLH) values are presented by building type and climate zone. A description of the building types that are used for HVAC systems is presented in Table 13.2-7. These building types are derived from the EIA CBECS study.⁵⁶³

These tables also include an “Other” building type, which can be used for business types that are not explicitly listed. The EFLH values used for Other are the most conservative values from the explicitly listed building types. When Other building type is used, a description of the actual building type, the primary business activity, the business operating hours, and the HVAC schedule must be collected.

Table 13.3-14: [Chillers] Equivalent Full-Load Hours

| Building Type | Principal Building Activity | EFLH | |
|-------------------|-----------------------------|------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Education | College | 2,173 | 3,894 |
| | Primary School | 915 | 1,716 |
| | Secondary School | 1,477 | 2,647 |
| Healthcare | Hospital | 3,115 | 4,015 |
| Large Multifamily | Midrise Apartment | 1,378 | 2,528 |
| Lodging | Large Hotel | 2,595 | 3,180 |
| | Nursing Home | 1,400 | 2,568 |

⁵⁶³ The Commercial Building Energy Consumption Survey (CBECS) implemented by the US Energy Information Administration includes a principal building activity categorization scheme that separates the Commercial sector into 29 categories and 51 subcategories based on principal building activity (PBA). For its purposes, the CBECS defines Commercial buildings as those buildings greater than 1,000 square feet that devote more than half of their floorspace to activity that is neither residential, manufacturing, industrial, nor agricultural. The high-level building types adopted for the TRM are adapted from this CBECS categorization, with some building types left out and one additional building type—Large Multifamily—included. <https://www.eia.gov/consumption/commercial/>.

| Building Type | Principal Building Activity | EFLH | |
|-------------------|-----------------------------|------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Mercantile | Stand-Alone Retail | 1,184 | 1,652 |
| | 24 Hr Retail | 1,642 | 2,488 |
| Office | Large Office | 2,009 | 2,401 |
| Public Assembly | Public Assembly | 1,231 | 2,307 |
| Religious Worship | Religious Worship | 713 | 994 |
| Other | Other | 713 | 994 |

13.3.2.3 Deemed Demand Savings Tables

Deemed peak coincidence factor (CF) values are presented by building type and climate zone.

These tables also include an “Other” building type, which can be used for business types that are not explicitly listed. The CF and EFLH values used for Other are the most conservative values from the explicitly listed building types. Alternately, with evaluator pre-approval, a deemed building type specified in Tables 13.3-15 thru 17 can be used in lieu of “Other” if it has a similar building type activity or operating schedule. For example, healthcare outpatient is not listed in the deemed tables, but the “office” building could be used if its typical operating schedule aligns closely with that of an office building. When the “Other” building type is used, or if a non-listed building type is mapped to another deemed option, a description of the actual building type, the primary business activity, the business operating hours, and the HVAC schedule must be collected.

Table 13.3-15: [Chillers] Non-Coincident Peak Demand Factors

| Building Type | Principal Building Activity | DF _{NCP} | |
|-------------------|-----------------------------|-------------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Education | College | 0.89 | 0.72 |
| | Primary School | 0.60 | 0.63 |
| | Secondary School | 0.89 | 0.72 |
| Healthcare | Hospital | 0.89 | 0.85 |
| Large Multifamily | Midrise Apartment | 0.66 | 0.69 |
| Lodging | Large Hotel | 0.98 | 1.00 |
| | Nursing Home | 0.66 | 0.69 |
| Mercantile | Stand-Alone Retail | 0.82 | 0.76 |
| | 24 Hr Retail | 0.86 | 0.79 |
| Office | Large Office | 1.06 | 0.73 |
| Public Assembly | Public Assembly | 0.60 | 0.63 |

| Building Type | Principal Building Activity | DF _{NCP} | |
|-------------------|-----------------------------|-------------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Religious Worship | Religious Worship | 0.82 | 0.76 |
| Other | Other | 0.60 | 0.63 |

Table 13.3-16: [Chillers] Coincident Peak Demand Factors

| Building Type | Principal Building Activity | DF _{CP} | |
|-------------------|-----------------------------|------------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Education | College | 0.84 | 0.52 |
| | Primary School | 0.55 | 0.58 |
| | Secondary School | 0.84 | 0.52 |
| Healthcare | Hospital | 0.85 | 0.73 |
| Large Multifamily | Midrise Apartment | 0.63 | 0.61 |
| Lodging | Large Hotel | 0.61 | 0.68 |
| | Nursing Home | 0.63 | 0.61 |
| Mercantile | Stand-Alone Retail | 0.77 | 0.68 |
| | 24 Hr Retail | 0.81 | 0.71 |
| Office | Large Office | 0.98 | 0.69 |
| Public Assembly | Public Assembly | 0.55 | 0.58 |
| Religious Worship | Religious Worship | 0.77 | 0.68 |
| Other | Other | 0.55 | 0.58 |

Table 13.3-17: [Chillers] 4CP Demand Factors

| Building Type | Principal Building Activity | DF _{4CP} | |
|-------------------|-----------------------------|-------------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Education | College | 0.70 | 0.61 |
| | Primary School | 0.45 | 0.59 |
| | Secondary School | 0.70 | 0.61 |
| Healthcare | Hospital | 0.78 | 0.77 |
| Large Multifamily | Midrise Apartment | 0.58 | 0.63 |
| Lodging | Large Hotel | 0.90 | 0.90 |
| | Nursing Home | 0.58 | 0.63 |
| Mercantile | Stand-Alone Retail | 0.66 | 0.68 |
| | 24 Hr Retail | 0.70 | 0.69 |

| Building Type | Principal Building Activity | DF _{4CP} | |
|-------------------|-----------------------------|-------------------|--------------|
| | | Air-Cooled | Water-Cooled |
| Office | Large Office | 0.84 | 0.70 |
| Public Assembly | Public Assembly | 0.45 | 0.59 |
| Religious Worship | Religious Worship | 0.66 | 0.68 |
| Other | Other | 0.45 | 0.59 |

13.3.2.4 Measure Life and Lifetime Savings

Estimated Useful Life (EUL)

The EUL of HVAC equipment is provided below:

- Screw / Scroll / Reciprocating Chillers – 20 years⁵⁶⁴
- Centrifugal Chillers – 25 years⁵⁶⁵

Remaining Useful Life (RUL)

The RUL of replaced systems is provided according to system age in Table 13.3-18. For ER units of unknown age, assume a default value equal to the EUL. This corresponds to a default RUL of 3.6 years for non-centrifugal chillers and 5.4 years for centrifugal chillers. Default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible. Both the RUL and EUL are needed to estimate savings for ER projects for two distinct periods: The ER period (RUL) and the ROB period (EUL - RUL). The calculations for ER projects are extensive, and as such are provided in Section 22.1.

Table 13.3-18: [Chillers] Remaining Useful Life or Replaced Unit⁵⁶⁶

| Age in Years of Replaced System | Non-Centrifugal Chilled Water Systems | Centrifugal Chilled Water Systems |
|---------------------------------|---------------------------------------|-----------------------------------|
| 1 | 18.7 | 23.9 |
| 2 | 17.7 | 22.9 |
| 3 | 16.7 | 21.9 |

⁵⁶⁴ DEER 2014 provides the value of 20 years for “High Efficiency Chillers.” DEER does not differentiate between centrifugal and non-centrifugal chillers.

⁵⁶⁵ Petition of AEP Texas Central Company, AEP Texas North Company, CenterPoint Energy Houston Electric, LLC, El Paso Electric Company, Entergy Texas Inc., Oncor Electric Delivery Company LLC, Sharyland Utilities, L.P., Southwestern Electric Power Company, Southwestern Public Service Company, And Texas-New Mexico Power Company To Revise Deemed Saving Values For Commercial HVAC And Solar Photovoltaic Measures, PUCT Docket No. 40885, Review of multiple studies looking at the lifetime of Centrifugal Chillers as detailed in petition workpapers.

⁵⁶⁶ Current NC baseline matches the baseline for existing systems manufactured in 2018. Existing systems manufactured after 1/1/2018 are not eligible to use the early retirement baseline. While IECC 2021 was adopted in 2023, efficiency requirements match. Values in gray are displayed for informational purposes only.

| Age in Years of Replaced System | Non-Centrifugal Chilled Water Systems | Centrifugal Chilled Water Systems |
|---------------------------------|---------------------------------------|-----------------------------------|
| 4 | 15.7 | 20.9 |
| 5 | 14.7 | 19.9 |
| 6 | 13.7 | 18.9 |
| 7 | 12.7 | 17.9 |
| 8 | 11.8 | 16.9 |
| 9 | 10.9 | 15.9 |
| 10 | 10.0 | 14.9 |
| 11 | 9.1 | 13.9 |
| 12 | 8.3 | 12.9 |
| 13 | 7.5 | 11.9 |
| 14 | 6.8 | 10.9 |
| 15 | 6.2 | 10.1 |
| 16 | 5.5 | 9.3 |
| 17 | 5.0 | 8.7 |
| 18 | 4.5 | 8.1 |
| 19 | 4.0 | 7.5 |
| 20 | 3.6 | 7.1 |
| 21 | 3.0 | 6.6 |
| 22 | 2.0 | 6.3 |
| 23 | 1.0 | 5.9 |
| 24 ⁵⁶⁷ | 0.0 | 5.6 |
| 25 | - | 5.4 |
| 26 | - | 5.0 |
| 27 | - | 4.0 |
| 28 | - | 3.0 |
| 29 | - | 2.0 |
| 30 | - | 1.0 |
| 31 ⁵⁶⁸ | - | 0.0 |

⁵⁶⁷ RULs are capped at the 75th percentile of non-centrifugal equipment age, 24 years, as determined based on DOE survival curves. Non-centrifugal systems older than 24 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

⁵⁶⁸ Ibid.

13.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- For “Other” or similar building type approximations: A description of the actual building type, the primary business activity, the business hours, and the HVAC schedule.
- Baseline type: ER, ROB, NC, system type conversion
- Baseline equipment type (compressor/condenser type)
- Baseline unit quantity
- Baseline rated cooling capacity
- For ER ONLY: baseline age of system and method of determination (e.g., nameplate, blueprints, customer reported, not available)
- For ER ONLY: photograph of retired unit nameplate demonstrating model number, serial number, and manufacturer if blueprints are not provided; if photograph of nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (alternate forms of documentation can be approved at the evaluator’s discretion)
- Manufacturer, model, and serial number of new unit
 - AHRI/DOE CCMS certificates or reference number matching model number
- New unit equipment type (compressor/condenser type)
- New unit path (Path A, Path B)
- Is the installed chiller a standby unit in a redundant chiller configuration? (Yes, No)
- New unit quantity
- New unit rated cooling capacity
- New unit cooling efficiency ratings
- For retrofit only: Proof of purchase: invoice showing model number; photos of the model number on product packaging or installed unit(s); OR an evaluator pre-approved inspection approach

- For new construction only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging or installed unit(s); as-built design drawings; HVAC specifications package that provides detailed make and model information on installed unit(s); OR an evaluator pre-approved inspection approach
- For chiller type conversion only: Condenser water pump HP and cooling tower fan HP

Document Revision History

Table 13.3-19: [Chillers] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Aligned building type names across all commercial measures. Incremented RUL table for code compliance. |
| FY 2026 | Updated early retirement age eligibility and criteria related to downsizing, and provided guidance for building types. |

13.4 PACKAGED TERMINAL AIR CONDITIONERS/ HEAT PUMPS, SINGLE PACKAGE VERTICAL AIR CONDITIONERS/HEAT PUMPS, AND ROOM AIR CONDITIONERS

13.4.1 Measure Description

This measure presents the deemed savings methodology for the installation of packaged terminal air conditioners (PTAC), packaged terminal heat pumps (PTHP), single package vertical air conditioners (SPVAC), single package vertical heat pumps (SPVHP), and room AC (RAC) systems. It covers assumptions made for baseline equipment efficiencies for early retirement (ER) of PTAC/PTHPs, replace-on-burnout (ROB), and new construction (NC) situations based current and previous on efficiency standards. For ER, the actual age of the baseline system should be determined from the equipment nameplate or other physical documentation whenever possible. Default values are provided for when the actual age of the unit is unknown.

Applicable efficient measure types include:

- Packaged Terminal Air Conditioners and Heat Pumps. Both Standard and Non-Standard size equipment types are covered. Standard Size refers to equipment with wall sleeve dimensions having an external wall opening greater than, or equal to 16 inches high or greater than, or equal to 42 inches wide and a cross sectional area greater than 670 in². Non-Standard Size refers to equipment with existing wall sleeve dimensions having an external wall opening of less than 16 inches high or less than 42 inches wide and a cross sectional area less than 670 in².
- Single Package Vertical Air Conditioners and Heat Pumps. All cooling capacities less than 240,000 Btu/hr are covered.
- Room Air Conditioners. Includes all equipment configurations covered by the federal appliance standards, including equipment with or without reverse cycle, louvered or non-louvered sides, casement-only, and casement-slide.

13.4.1.1 Eligibility Criteria

For a measure to be eligible for this deemed savings approach the following conditions will be met:

- The existing and proposed cooling equipment are electric.
- The PTAC, PTHP, or RAC must be the primary cooling source for the space.
- ER projects involve the replacement of a working system that is at least five years old and before natural burnout occurs. The ER approach cannot be used for projects involving a renovation where a major structural change or internal space remodel has occurred. An ROB approach should be used for these scenarios.

- Manufacturer datasheets for installed equipment or documentation of AHRI or DOE CCMS certification must be provided.^{569,570}

13.4.1.2 Baseline Condition

Early Retirement

ER scenarios involve the replacement of a working system prior to natural burnout. The ER baseline cannot be used for projects involving a renovation where a major structural change or internal space remodel has occurred. Two baseline condition efficiency values are required for an ER scenario, one for the ER (RUL) period and one for the ROB (EUL-RUL) period. For the ROB period, the baseline efficiency is the same as for an ROB/NC scenario. For the ER period, the baseline efficiency should be estimated according to the capacity, system type (PTAC or PTHP), and age (based on year manufactured) of the replaced system. When the system age can be determined (from a nameplate, building prints, equipment inventory list, etc.), the baseline efficiency levels provided in

Table 13.4-1, reflecting ASHRAE Standard 90.1-2001 through 90.1-2007, should be used. PTHPs replacing PTACs with built-in electric resistance heat should use a baseline heating efficiency of 1.0 COP.

When the system age is unknown, assume a default value equal to the EUL. This corresponds to an age of 15 years. A default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible.

Existing standard size PTAC systems manufactured as of January 1, 2017 and standard size PTHP systems manufactured as of October 8, 2012, are not eligible for early retirement. All non-standard size PTAC/PTHPs are not eligible for early retirement.

Table 13.4-1: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] ER Baseline Efficiency for Standard Size PTAC/PTHPs^{571,572}

| Equipment | Cooling Capacity [Btuh] | Baseline Cooling Efficiency [EER] | Baseline Heating Efficiency [COP] (No Built-in Resistance Heat) | Baseline Heating Efficiency [COP] (With Built-in Resistance Heat) |
|-----------|-------------------------|--|---|---|
| PTAC | <7,000 | 11.0 | - | 1.0 |
| | 7,000-15,000 | $12.5 - (0.213 \times \text{Cap} / 1,000)$ | | |
| | >15,000 | 9.3 | | |
| PTHP | <7,000 | 10.8 | 3.0 | - |

⁵⁶⁹ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

⁵⁷⁰ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

⁵⁷¹ ER only applies to standard size units because the minimum efficiency requirements for non-standard systems have never changed, making the ER baseline efficiency the same as for ROB.

⁵⁷² Cap refers to the rated cooling capacity in Btuh. If the capacity is less than 7,000 Btuh, use 7,000 Btuh in the calculation. If the capacity is greater than 15,000 Btuh, use 15,000 Btuh in the calculation.

| Equipment | Cooling Capacity [Btuh] | Baseline Cooling Efficiency [EER] | Baseline Heating Efficiency [COP] (No Built-in Resistance Heat) | Baseline Heating Efficiency [COP] (With Built-in Resistance Heat) |
|-----------|-------------------------|--|---|---|
| | 7,000-15,000 | $12.3 - (0.213 \times \text{Cap} / 1,000)$ | $3.2 - (0.026 \times \text{Cap} / 1,000)$ | |
| | >15,000 | 9.1 | 2.8 | |

Replace-on-Burnout and New Construction:

Table 13.4-2 provides federal minimum efficiency standards for PTAC/PTHP units reflected in 10 CFR 431. The effective date for standard size PTACs is January 1, 2017, and the effective date for standard size PTHPs is October 8, 2012. The effective date for all non-standard PTAC/PTHPs is October 7, 2010.

Table 13.4-2: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] NC/ROB Baseline Efficiency Levels^{573,574}

| Equipment | Category | Cooling Capacity [Btuh] | Minimum cooling efficiency (EER) | Minimum heating efficiency (COP) |
|-----------|-------------------|-------------------------|--|---|
| PTAC | Standard Size | <7,000 | 11.9 | — |
| | | 7,000-15,000 | $14.0 - (0.300 \times \text{Cap}/1,000)$ | — |
| | | >15,000 | 9.5 | — |
| | Non-Standard Size | <7,000 | 9.4 | — |
| | | 7,000-15,000 | $10.9 - (0.213 \times \text{Cap}/1,000)$ | — |
| | | >15,000 | 7.7 | — |
| PTHP | Standard Size | <7,000 | 11.9 | 3.3 |
| | | 7,000-15,000 | $14.0 - (0.300 \times \text{Cap}/1,000)$ | $3.7 - (0.052 \times \text{Cap}/1,000)$ |
| | | >15,000 | 9.5 | 2.9 |
| | Non-Standard Size | <7,000 | 9.3 | 2.7 |
| | | 7,000-15,000 | $10.8 - (0.213 \times \text{Cap}/1,000)$ | $2.9 - (0.026 \times \text{Cap}/1,000)$ |
| | | >15,000 | 7.6 | 2.5 |

⁵⁷³ IECC 2015 Table C403.2.3(3)

⁵⁷⁴ Cap refers to the rated cooling capacity in Btuh. If the capacity is less than 7,000 Btuh, use 7,000 Btuh in the calculation. If the capacity is greater than 15,000 Btuh, use 15,000 Btuh in the calculation.

Table 13.4-3 provides federal minimum efficiency standards for SPVAC/SPVHP units reflected in 10 CFR 431. The effective date for the Final Rule was November 23, 2015. Compliance with the standards for SPVAC/SPVHPs with cooling capacities less than 65,000 Btu/hr was September 23, 2019; compliance with the standard for SPVAC/SPVHPs with cooling capacities between 65,000 and 135,000 Btu/hr was October 9, 2015; and compliance with the standard for SPVAC/SPVHPs with cooling capacities between 135,000 and 240,000 Btu/hr was October 9, 2016.

Table 13.4-3: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] NC/ROB Baseline Efficiency Levels⁵⁷⁵

| Equipment type | Cooling capacity (Btuh) | Minimum cooling efficiency (EER) | Minimum heating efficiency (COP) |
|--|-------------------------|----------------------------------|----------------------------------|
| Single package vertical air conditioners | < 65,000 | 11.0 | - |
| | ≥ 65,000 and < 240,000 | 10.0 | - |
| Single package vertical air heat pumps | < 65,000 | 11.0 | 3.3 |
| | ≥ 65,000 and < 240,000 | 10.0 | 3.0 |

Table 13.4-4 reflects the standards for room air conditioners, specified in 10 CFR 430.32(b). A new federal standard went into effect on August 30, 2023. However, this standard does not require manufacturer compliance until May 26, 2026.⁵⁷⁶

Table 13.4-4: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] NC/ROB Baseline Efficiency Levels⁵⁷⁷

| Category | Cooling Capacity [Btuh] | Minimum Cooling Efficiency [CEER] |
|---|-------------------------|-----------------------------------|
| Without reverse cycle, with louvered sides | < 8,000 | 11.0 |
| | ≥ 8,000 and < 14,000 | 10.9 |
| | ≥ 14,000 and < 20,000 | 10.7 |
| | ≥ 20,000 and ≤ 25,000 | 9.4 |
| | > 25,000 | 9.0 |
| Without reverse cycle, without louvered sides | < 8,000 | 10.0 |
| | ≥ 8,000 and < 11,000 | 9.6 |

⁵⁷⁵ 10 CFR 431.97 Table 10.

⁵⁷⁶ Current DOE minimum efficiency standard for residential room air conditioners. <https://www.regulations.gov/document/EERE-2014-BT-STD-0059-0057>.

⁵⁷⁷ Direct final rule for new Room Air Conditioner Standards was published on April 21st, 2011 (76 FR 22454), effective August 19th, 2011, and are required starting June 1st, 2014. These are found in 10 CFR Part 430.

| Category | Cooling Capacity [Btuh] | Minimum Cooling Efficiency [CEER] |
|--|-------------------------|-----------------------------------|
| | ≥ 11,000 and < 14,000 | 9.5 |
| | ≥ 14,000 and < 20,000 | 9.3 |
| | ≥ 20,000 | 9.4 |
| With reverse cycle, with louvered sides | < 20,000 | 9.8 |
| | ≥ 20,000 | 9.3 |
| With reverse cycle, without louvered sides | < 14,000 | 9.3 |
| | ≥ 14,000 | 8.7 |
| Casement-only | All capacities | 9.5 |
| Casement-slider | All capacities | 10.4 |

13.4.1.3 High-Efficiency Condition

The high-efficiency retrofits must exceed the minimum federal standards found in Table 13.4-2: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] NC/ROB Baseline Efficiency Levels:

| Equipment | Category | Cooling Capacity [Btuh] | Minimum cooling efficiency (EER) | Minimum heating efficiency (COP) |
|-----------|-------------------|-------------------------|----------------------------------|----------------------------------|
| PTAC | Standard Size | <7,000 | 11.9 | — |
| | | 7,000-15,000 | 14.0 – (0.300 x Cap/1,000) | — |
| | | >15,000 | 9.5 | — |
| | Non-Standard Size | <7,000 | 9.4 | — |
| | | 7,000-15,000 | 10.9 – (0.213 x Cap/1,000) | — |
| | | >15,000 | 7.7 | — |
| PTHP | Standard Size | <7,000 | 11.9 | 3.3 |
| | | 7,000-15,000 | 14.0 – (0.300 x Cap/1,000) | 3.7 – (0.052 x Cap/1,000) |
| | | >15,000 | 9.5 | 2.9 |
| | Non-Standard Size | <7,000 | 9.3 | 2.7 |
| | | 7,000-15,000 | 10.8 – (0.213 x Cap/1,000) | 2.9 – (0.026 x Cap/1,000) |
| | | >15,000 | 7.6 | 2.5 |

through Table 13.4-4.

The high-efficiency retrofits must also meet the following criteria:

- For ER projects only, when downsizing, the pre-installed cooling capacity is limited to a maximum of 120 percent of the new equipment's cooling capacity. There is no cap on upsizing because the savings are calculated using the lower pre-capacity.
- For scenarios involving the replacement of a combination of systems by an alternate combination of systems of varying capacities, ER savings can still be claimed if the overall pre and post capacities for the total combination of systems are compliant with the guidance in the previous bullet. In these cases, a custom calculation should be performed to establish the following weighted savings factors to be applied over the ER portion of the savings calculation: manufacturer year, EUL, RUL, baseline efficiency, EFLH, and demand factor. These factors should be weighted based on contribution to overall capacity.
- Non-standard size PTAC/PTHPs cannot be used for NC.
- No additional measures are being installed that directly affect the operation of the cooling equipment (i.e., control sequences).

13.4.2 Energy and Demand Savings Methodology

13.4.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{Savings,C} + kWh_{Savings,H}$$

Equation 13.4-1

$$kWh_{Savings,C} = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times \frac{EFLH_C}{1,000}$$

Equation 13.4-2

$$kWh_{Savings,H} = \left(\frac{Cap_{H,pre}}{\eta_{baseline,H}} - \frac{Cap_{H,post}}{\eta_{installed,H}} \right) \times \frac{EFLH_H}{3,412}$$

Equation 13.4-3

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times \frac{DF}{1,000}$$

Equation 13.4-4

Where:

$Cap_{C/H,pre}$ = For ER and ROB, rated equipment cooling/heating capacity of the existing equipment at AHRI standard conditions with a maximum of 20 percent larger than the post-capacity; for NC, rated equipment cooling/heating capacity of the new equipment at AHRI standard conditions [Btuh]; 1 ton = 12,000 Btuh.

$Cap_{C/H,post}$ = Rated equipment cooling/heating capacity of the newly installed equipment at AHRI standard conditions with a maximum equal to the baseline pre-capacity [Btuh]; 1 ton = 12,000 Btuh.

Note: The capacity in the equations may not always match the capacity of the units

$\eta_{baseline,C}$ = Cooling efficiency of existing (ER) or standard (ROB/NC) equipment [EER, Btu/W-h]; see Table 13.4-1 through Table 13.4-4

$\eta_{baseline,H}$ = Heating efficiency of existing (ER) or standard (ROB/NC) equipment [COP]; see Table 13.4-1 and Table 13.4-3.

$\eta_{installed,C}$ = Rated cooling efficiency of the newly installed equipment [EER, Btu/W-h]. Rated cooling efficiency must exceed minimum federal standards found in Table 13.4-2: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] NC/ROB Baseline Efficiency Levels

| Equipment | Category | Cooling Capacity [Btuh] | Minimum cooling efficiency (EER) | Minimum heating efficiency (COP) |
|-----------|-------------------|-------------------------|----------------------------------|----------------------------------|
| PTAC | Standard Size | <7,000 | 11.9 | — |
| | | 7,000-15,000 | 14.0 – (0.300 x Cap/1,000) | — |
| | | >15,000 | 9.5 | — |
| | Non-Standard Size | <7,000 | 9.4 | — |
| | | 7,000-15,000 | 10.9 – (0.213 x Cap/1,000) | — |
| | | >15,000 | 7.7 | — |
| PTHP | Standard Size | <7,000 | 11.9 | 3.3 |
| | | 7,000-15,000 | 14.0 – (0.300 x Cap/1,000) | 3.7 – (0.052 x Cap/1,000) |
| | | >15,000 | 9.5 | 2.9 |
| | Non-Standard Size | <7,000 | 9.3 | 2.7 |
| | | 7,000-15,000 | 10.8 – (0.213 x Cap/1,000) | 2.9 – (0.026 x Cap/1,000) |
| | | >15,000 | 7.6 | 2.5 |

through Table 13.4-4.⁵⁷⁸

| | | |
|-----------------------------|---|---|
| $\eta_{\text{installed},H}$ | = | Rated heating efficiency of the newly installed equipment [COP]. Rated heating efficiency must exceed minimum federal standards found in Table 13.4-3. ⁵⁷⁹ |
| DF | = | Demand factor (NCP, CP, or 4CP) for appropriate building and equipment type; see Table 13.4-6 through Table 13.4-8. |
| $EFLH_{C/H}$ | = | Cooling/heating equivalent full-load hours for newly installed equipment based on appropriate building and equipment type [hours]. Table 13.4-5 contains the effective full load hours for commercial packaged terminal air conditioners, packaged terminal heat pumps, and room AC systems in San Antonio. |
| 1,000 | = | Constant to convert from watts to kilowatts. |
| 3,412 | = | Constant to convert from Btu to kWh. |

Early Retirement

The first-year savings algorithms in the above equations are used for all HVAC projects, across NC, ROB, and ER projects. However, ER projects require a weighted savings calculated over both the ER and ROB periods taking the EUL and RUL into account. The ER savings are applied over the remaining useful life (RUL) period, and the ROB savings are applied over the remaining period (EUL-RUL). The final reported savings for ER projects are not actually a “first-year” savings, but an “average annual savings over the lifetime (EUL) of the measure.” These savings calculations are explained in Section 22.1.

13.4.2.2 Deemed Energy Savings Tables

Table 13.4-5 presents the deemed equivalent full-load hour (EFLH) values for PTAC/PTHPs, SPVAC/SPVHPs, and RACs. These values are calculated by building type and equipment type. A description of the calculation method can also be found in Docket No. 40885, Attachment B.

These tables also include an “Other” building type, which can be used for business types that are not explicitly listed. The DF and EFLH values used for Other are the most conservative values from the explicitly listed building types. When the Other building type is used, a description of the actual building type, the primary business activity, the business hours, and the HVAC schedule must be collected. For those combinations of technology, climate zone, and building type where no values are present, a project with that specific combination should use the “Other” building type.

⁵⁷⁸ Rated efficiency is commonly reported at both 230V and 208V. Savings calculations should reference efficiency at 230V, as AHRI rating conditions specify that voltage.

⁵⁷⁹ Ibid.

Table 13.4-5: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] Equivalent Full-Load Hours

| Building Type | Principal Building Activity | PTAC | PTHP | |
|---------------|-----------------------------|-------------------|-------------------|-------------------|
| | | EFLH _c | EFLH _c | EFLH _H |
| Education | Primary School | 1,330 | 1,330 | 86 |
| | Secondary School | 1,163 | 1,163 | 96 |
| Food Sales | Convenience | 1,878 | 1,878 | 120 |
| Food Service | Full-Service Restaurant | 1,831 | 1,831 | 185 |
| | 24 Hr Full-Service | 2,075 | 2,075 | 232 |
| | Quick-Service Restaurant | 1,625 | 1,625 | 138 |
| | 24 Hr Quick Service | 1,882 | 1,882 | 205 |
| Lodging | Large Hotel | 2,117 | 2,117 | 105 |
| | Nursing Home | 2,009 | 2,009 | 33 |
| | Small Hotel | 1,971 | 1,971 | 50 |
| Mercantile | Strip Mall | 1,194 | 1,194 | 84 |
| Office | Small Office | 1,301 | 1,301 | 50 |
| Other | Other | 1,163 | 1,163 | 33 |

13.4.2.3 Deemed Demand Savings Tables

Table 13.4-6 through Table 13.4-8 contain the NCP, CP, and 4CP demand factors for commercial PTAC/PTHPs, SPVAC/SPVHPs, and RACs in San Antonio. and RACs. These values are calculated by building type and equipment type.

Table 13.4-6: [PTACs, PTHPs, SPVACs, SPVHPs, & Room ACs] Non-Coincident Peak Demand Factors

| Building Type | Principal Building Activity | PTAC | PTHP |
|---------------|-----------------------------|------|------|
| Education | Primary School | 0.88 | 0.88 |
| | Secondary School | 0.90 | 0.90 |
| Food Sales | Convenience | 0.90 | 0.90 |
| Food Service | Full-Service Restaurant | 0.90 | 0.90 |
| | 24 Hr Full-Service | 0.91 | 0.91 |
| | Quick-Service Restaurant | 0.90 | 0.90 |
| | 24 Hr Quick Service | 0.90 | 0.90 |
| Lodging | Large Hotel | 0.61 | 0.61 |
| | Nursing Home | 0.87 | 0.87 |
| | Small Hotel | 0.57 | 0.57 |

| Building Type | Principal Building Activity | PTAC | PTHP |
|---------------|-----------------------------|------|------|
| Mercantile | Strip Mall | 0.82 | 0.82 |
| Office | Small Office | 0.84 | 0.84 |
| Other | Other | 0.57 | 0.57 |

Table 13.4-7: [PTACs, PTHPs, SPVACs, SPVHPs, & RACs] Coincident Peak Demand Factors

| Building Type | Principal Building Activity | PTAC | PTHP |
|---------------|-----------------------------|------|------|
| Education | Primary School | 0.85 | 0.85 |
| | Secondary School | 0.86 | 0.86 |
| Food Sales | Convenience | 0.82 | 0.82 |
| Food Service | Full-Service Restaurant | 0.85 | 0.85 |
| | 24 Hr Full-Service | 0.86 | 0.86 |
| | Quick-Service Restaurant | 0.82 | 0.82 |
| | 24 Hr Quick Service | 0.85 | 0.85 |
| Lodging | Large Hotel | 0.58 | 0.58 |
| | Nursing Home | 0.84 | 0.84 |
| | Small Hotel | 0.54 | 0.54 |
| Mercantile | Strip Mall | 0.78 | 0.78 |
| Office | Small Office | 0.80 | 0.80 |
| Other | Other | 0.54 | 0.54 |

Table 13.4-8: [PTACs, PTHPs, SPVACs, SPVHPs, & RACs] 4CP Demand Factors

| Building Type | Principal Building Activity | PTAC | PTHP |
|---------------|-----------------------------|------|------|
| Education | Primary School | 0.69 | 0.69 |
| | Secondary School | 0.73 | 0.73 |
| Food Sales | Convenience | 0.74 | 0.74 |
| Food Service | Full-Service Restaurant | 0.75 | 0.75 |
| | 24 Hr Full-Service | 0.78 | 0.78 |
| | Quick-Service Restaurant | 0.74 | 0.74 |
| | 24 Hr Quick Service | 0.78 | 0.78 |
| Lodging | Large Hotel | 0.71 | 0.71 |
| | Nursing Home | 0.73 | 0.73 |
| | Small Hotel | 0.70 | 0.70 |
| Mercantile | Strip Mall | 0.69 | 0.69 |

| Building Type | Principal Building Activity | PTAC | PTHP |
|---------------|-----------------------------|------|------|
| Office | Small Office | 0.71 | 0.71 |
| Other | Other | 0.69 | 0.69 |

13.4.2.4 Measure Life and Lifetime Savings

Estimated Useful Life (EUL)

The EUL of PTAC/PTHP units is 15 years, as specified in DEER 2014.⁵⁸⁰

The EUL of SPVAC/SPVHP units is 15 years, as determined by the DOE in its September 2015 final rule.⁵⁸¹

The EUL of RAC units is 10 years based on current DOE Final Rule standards for room air conditioners. This value is consistent with the EUL reported in the Department of Energy Technical Support Document for Room Air conditioners.⁵⁸²

Remaining Useful Life (RUL) for PTAC/PTHP Systems

The RUL of ER replaced systems is provided according to system age in Table 13.4-9.

For ER units of unknown age, assume a default value equal to the EUL. This corresponds to a default RUL of 2.8 years. Default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible. Both the RUL and EUL are needed to estimate savings for ER projects for two distinct periods: the ER period (RUL) and the ROB period (EUL - RUL). The calculations for ER projects are extensive, and as such are provided in Section 22.1.

Table 13.4-9: [PTACs, PTHPs, SPVACs, SPVHPs, & RACs] Remaining Useful Life of Standard Size PTACs⁵⁸³

| Age of Replaced System (Years) | RUL (Years) | Year Installed (Replaced System) | Year Installed (Replaced System) |
|--------------------------------|-------------|----------------------------------|----------------------------------|
| 1 | 14.0 | 10 | 5.7 |
| 2 | 13.0 | 11 | 5.0 |
| 3 | 12.0 | 12 | 4.4 |
| 4 | 11.0 | 13 | 3.8 |
| 5 | 10.0 | 14 | 3.3 |

⁵⁸⁰ <http://www.deeresources.com/>

⁵⁸¹ Department of Energy, Energy Conservation Program: Energy Conservation Standards for Single Package Vertical Air Conditioners and Single Package Vertical Heat Pumps, 80 FR 57467 <https://www.federalregister.gov/documents/2015/09/23/2015-23029/energy-conservation-program-energy-conservation-standards-for-single-package-vertical-air>

⁵⁸² Technical Support Document: Room Air Conditioners, June 2020, p. ES-14. <https://www.regulations.gov/document/EERE-2014-BT-STD-0059-0013>.

⁵⁸³ Current federal standard effective date is 1/1/2017. Existing systems manufactured after this date are not eligible to use the ER baseline and should use the ROB baseline instead. Grayed out values are displayed for informational purposes only.

| Age of Replaced System (Years) | RUL (Years) | Year Installed (Replaced System) | Year Installed (Replaced System) |
|--------------------------------|-------------|----------------------------------|----------------------------------|
| 6 | 9.1 | 15 | 2.8 |
| 7 | 8.2 | 16 | 2.0 |
| 8 | 7.3 | 17 | 1.0 |
| 9 | 6.5 | 18 ⁵⁸⁴ | 0.0 |

Table 13.4-10: [PTACs, PTHPs, SPVACs, SPVHPs, & RACs] Remaining Useful Life of Standard Size PTHPs⁵⁸⁵

| Age of Replaced System (Years) | RUL (Years) | Year Installed (Replaced System) | Year Installed (Replaced System) |
|--------------------------------|-------------|----------------------------------|----------------------------------|
| 1 | 14.0 | 10 | 5.7 |
| 2 | 13.0 | 11 | 5.0 |
| 3 | 12.0 | 12 | 4.4 |
| 4 | 11.0 | 13 | 3.8 |
| 5 | 10.0 | 14 | 3.3 |
| 6 | 9.1 | 15 | 2.8 |
| 7 | 8.2 | 16 | 2.0 |
| 8 | 7.3 | 17 | 1.0 |
| 9 | 6.5 | 18 ⁵⁸⁶ | 0.0 |

13.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- For 'Other' building type ONLY: a description of the actual building type, the primary business activity, the business hours, and the HVAC schedule

⁵⁸⁴ RULs are capped at the 75th percentile of equipment age, 18 years, as determined based on DOE survival curves. Systems older than 18 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

⁵⁸⁵ Current federal standard effective date is 10/8/2012. Existing systems manufactured after this date are not eligible to use the ER baseline and should use the ROB baseline instead. Grayed out values are displayed for informational purposes only.

⁵⁸⁶ RULs are capped at the 75th percentile of equipment age, 18 years, as determined based on DOE survival curves. Systems older than 18 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

- Baseline type: ER, ROB, NC, system type conversion
- Baseline unit quantity
- Baseline equipment type
- Baseline rated cooling and heating capacities
- For ER ONLY: baseline Age and Method of Determination (e.g., nameplate, blueprints, customer reported, not available)
- For ER ONLY: photograph of retired unit nameplate demonstrating model number, serial number, and manufacturer if blueprints are not provided; if photograph of nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (alternate forms of documentation can be approved at the evaluator's discretion)
- Manufacturer, model, and serial number of new unit
 - AHRI/DOE CCMS certificates or reference number matching model number
- New unit equipment type (PTAC, PTHP, SPVAC, SPVHP, RAC)
- New unit equipment configuration category: standard/non-standard (PTAC/PTHP only)
- New unit quantity
- New unit rated cooling and heating capacities
- New unit cooling and heating efficiency ratings
- For retrofit only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging and installed unit(s); OR an evaluator pre-approved inspection approach
- For new construction only: Proof of purchase: invoice showing model number; a photo of the model number on product packaging and installed unit(s); as-built design drawings; HVAC specifications package that provides detailed make and model information on installed unit(s); OR an evaluator pre-approved inspection approach

Document Revision History

Table 13.4-11: [PTACs, PTHPs, SPVACs, SPVHPs, & RACs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Added SPVAC and SPVHP units to measure. Corrected current federal standard effective data. Added separate RUL table for PTHP. Aligned building type names across all commercial measures. Incremented RUL table for code compliance. |
| FY 2026 | Updated early retirement age eligibility and criteria related to downsizing. |

COMPUTER ROOM AIR CONDITIONERS

13.4.4 Measure Description

This section summarizes the deemed savings methodology for the installation of computer room air conditioning (CRAC) systems. A CRAC unit is a device that monitors and maintains the temperature, air distribution, and humidity in a network room or data center. This measure covers assumptions made for baseline equipment efficiencies for early retirement (ER) based on the age of the replaced equipment and replace-on-burnout (ROB) and new construction (NC) situations based on efficiency standards. Savings calculations incorporate the use of only part-load efficiency values, as these types of units are only rated in units of sensible coefficient of performance (SCOP) for units manufactured before May 28, 2024, and net sensible coefficient of performance (NSenCOP) for units manufactured as of May 28, 2024. For ER, the actual age of the baseline system should be determined from the equipment nameplate or other physical documentation whenever possible. If the actual age of the unit is unknown, default values are provided.

13.4.4.1 Eligibility Criteria

For a measure to be eligible for this deemed savings approach the following conditions will be met:

- The existing and proposed cooling equipment are electric.
- The building type is a network room or data center.
- ER projects involve the replacement of a working system. The ER approach cannot be used for projects involving a renovation where a major structural change or internal space remodel has occurred. An ROB approach should be used for these scenarios.
- If these conditions are not met, the deemed savings approach cannot be used, and the M&V Methodology described in the commercial custom measure must be used.
- Manufacturer datasheets for installed equipment or documentation of AHRI or DOE CCMS certification must be provided.^{587,588}

13.4.4.2 Baseline Condition

The baseline conditions related to efficiency and system capacity for ER and ROB/NC are described in the following sections.

Early Retirement

ER scenarios involve the replacement of a working system prior to natural burnout. The ER baseline cannot be used for projects involving a renovation where a major structural change or internal space remodel has

⁵⁸⁷ Air-Conditioning, Heating, and Refrigeration Institute (AHRI) Directory: <https://www.ahridirectory.org/>.

⁵⁸⁸ Department of Energy Compliance Certification Management System (DOE CCMS): <https://www.regulations.doe.gov/certification-data/>.

occurred.

Two baseline condition efficiency values are required for an ER scenario, one for the ER (RUL) period and one for the ROB (EUL-RUL) period. For the ROB period, the baseline efficiency is the same as for an ROB/NC scenario. For the ER period, the baseline efficiency should be estimated according to the capacity, system type, and age (based on year manufactured) of the replaced system. When the system age can be determined (from a nameplate, building prints, equipment inventory list, etc.), the baseline efficiency levels provided in Table 0-1.

When the system age is unknown, assume a default value equal to the EUL. This corresponds to an age of 15 years. A default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible. Existing systems manufactured as of January 1, 2023 are not eligible for early retirement.

Table 0-1: [CRACs] ER Baseline Efficiency Levels⁵⁸⁹

| System Type | Capacity [Btu/hr] | Baseline Efficiencies [SCOP] | |
|---|------------------------|------------------------------|--------------|
| | | Downflow Units | Upflow Units |
| Air conditioners, air cooled | < 65,000 | 2.20 | 2.09 |
| | ≥ 65,000 and < 240,000 | 2.10 | 1.99 |
| | ≥ 240,000 | 1.90 | 1.79 |
| Air conditioners, water cooled | < 65,000 | 2.60 | 2.49 |
| | ≥ 65,000 and < 240,000 | 2.50 | 2.39 |
| | ≥ 240,000 | 2.40 | 2.29 |
| Air conditioners, water cooled with fluid economizer | < 65,000 | 2.55 | 2.44 |
| | ≥ 65,000 and < 240,000 | 2.45 | 2.34 |
| | ≥ 240,000 | 2.35 | 2.24 |
| Air conditioners, glycol cooled (rated at 40% propylene glycol) | < 65,000 | 2.50 | 2.39 |
| | ≥ 65,000 and < 240,000 | 2.15 | 2.04 |
| | ≥ 240,000 | 2.10 | 1.99 |
| Air conditioners, glycol cooled (rated at 40% propylene glycol) with fluid economizer | < 65,000 | 2.45 | 2.34 |
| | ≥ 65,000 and < 240,000 | 2.10 | 1.99 |

⁵⁸⁹ IECC 2018 Table C403.3.2(9).

| System Type | Capacity [Btu/hr] | Baseline Efficiencies [SCOP] | |
|-------------|----------------------|------------------------------|--------------|
| | | Downflow Units | Upflow Units |
| | ≥ 240,000 | 2.05 | 1.94 |

Replace-on-Burnout (ROB) and New Construction (NC)

Baseline efficiency levels for CRACs are provided in Table 0-2. These baseline efficiency levels reflect the minimum efficiency requirements from Department of Energy (DOE) 10 CFR 431, referencing ASRAE 90.1-2019. This standard updates the standard efficiency metric from SCOP to NSenCOP. The current federal standard is effective May 28, 2024.

13.4.4.3 High-Efficiency Condition

CRAC units must exceed the minimum efficiencies specified in Table 0-2. These baseline efficiency levels reflect the minimum efficiency requirements from IECC 2021, which uses sensible coefficient of performance (SCOP) as the standard efficiency metric.

Table 0-2: [CRACs] NC/ROB Baseline Efficiency Levels⁵⁹⁰

| System Type | Duct Location | Capacity [Btu/hr] | Baseline Efficiencies for Downflow/Upflow Units [NSenCOP] |
|---------------|------------------|-------------------------|---|
| Floor Mounted | | | |
| Air cooled | Downflow | < 80,000 | 2.70 |
| | | ≥ 80,000 and < 295,000 | 2.58 |
| | | ≥ 295,000 and < 930,000 | 2.36 |
| | Upflow-ducted | < 80,000 | 2.67 |
| | | ≥ 80,000 and < 295,000 | 2.55 |
| | | ≥ 295,000 and < 930,000 | 2.33 |
| | Upflow-nonducted | < 65,000 | 2.16 |
| | | ≥ 65,000 and < 240,000 | 2.04 |
| | | ≥ 240,000 and < 760,000 | 1.89 |
| | Horizontal | < 65,000 | 2.65 |
| | | ≥ 65,000 and < 240,000 | 2.55 |
| | | ≥ 240,000 and < 760,000 | 2.47 |

⁵⁹⁰ DOE 10 CFR 431: Table I-1 & I-2IECC 2015 Table C403.2.3(9). <https://www.federalregister.gov/documents/2022/03/07/2022-04151/energy-conservation-program-energy-conservation-standards-for-computer-room-air-conditioners>.

| System Type | Duct Location | Capacity [Btu/hr] | Baseline Efficiencies for Downflow/Upflow Units [NSenCOP] |
|------------------------------------|------------------|-------------------------|---|
| Air cooled with fluid economizer | Downflow | < 80,000 | 2.70 |
| | | ≥ 80,000 and < 295,000 | 2.58 |
| | | ≥ 295,000 and < 930,000 | 2.36 |
| | Upflow-ducted | < 80,000 | 2.67 |
| | | ≥ 80,000 and < 295,000 | 2.55 |
| | | ≥ 295,000 and < 930,000 | 2.33 |
| | Upflow-nonducted | < 65,000 | 2.09 |
| | | ≥ 65,000 and < 240,000 | 1.99 |
| | | ≥ 240,000 and < 760,000 | 1.81 |
| | Horizontal | < 65,000 | 2.65 |
| | | ≥ 65,000 and < 240,000 | 2.55 |
| | | ≥ 240,000 and < 760,000 | 2.47 |
| Water cooled | Downflow | < 80,000 | 2.82 |
| | | ≥ 80,000 and < 295,000 | 2.73 |
| | | ≥ 295,000 and < 930,000 | 2.67 |
| | Upflow-ducted | < 80,000 | 2.79 |
| | | ≥ 80,000 and < 295,000 | 2.70 |
| | | ≥ 295,000 and < 930,000 | 2.64 |
| | Upflow-nonducted | < 65,000 | 2.43 |
| | | ≥ 65,000 and < 240,000 | 2.32 |
| | | ≥ 240,000 and < 760,000 | 2.20 |
| | Horizontal | < 65,000 | 2.79 |
| | | ≥ 65,000 and < 240,000 | 2.68 |
| | | ≥ 240,000 and < 760,000 | 2.60 |
| Water cooled with fluid economizer | Downflow | < 80,000 | 2.77 |
| | | ≥ 80,000 and < 295,000 | 2.68 |
| | | ≥ 295,000 | 2.61 |
| | Upflow-ducted | < 80,000 | 2.74 |
| | | ≥ 80,000 and < 295,000 | 2.65 |
| | | ≥ 295,000 and < 930,000 | 2.58 |

| System Type | Duct Location | Capacity [Btu/hr] | Baseline Efficiencies for Downflow/Upflow Units [NSenCOP] |
|-------------------------------------|------------------|-------------------------|---|
| | Upflow-nonducted | < 65,000 | 2.35 |
| | | ≥ 65,000 and < 240,000 | 2.24 |
| | | ≥ 240,000 and < 760,000 | 2.12 |
| | Horizontal | < 65,000 | 2.71 |
| | | ≥ 65,000 and < 240,000 | 2.60 |
| | | ≥ 240,000 and < 760,000 | 2.54 |
| Glycol cooled | Downflow | < 80,000 | 2.56 |
| | | ≥ 80,000 and < 295,000 | 2.24 |
| | | ≥ 295,000 and < 930,000 | 2.21 |
| | Upflow-ducted | < 80,000 | 2.53 |
| | | ≥ 80,000 and < 295,000 | 2.21 |
| | | ≥ 295,000 and < 930,000 | 2.18 |
| | Upflow-nonducted | < 65,000 | 2.08 |
| | | ≥ 65,000 and < 240,000 | 1.90 |
| | | ≥ 240,000 and < 760,000 | 1.81 |
| | Horizontal | < 65,000 | 2.48 |
| | | ≥ 65,000 and < 240,000 | 2.18 |
| | | ≥ 240,000 and < 760,000 | 2.18 |
| Glycol cooled with fluid economizer | Downflow | < 80,000 | 2.51 |
| | | ≥ 80,000 and < 295,000 | 2.19 |
| | | ≥ 295,000 and < 930,000 | 2.15 |
| | Upflow-ducted | < 80,000 | 2.48 |
| | | ≥ 80,000 and < 295,000 | 2.16 |
| | | ≥ 295,000 and < 930,000 | 2.12 |
| | Upflow-nonducted | < 65,000 | 2.00 |
| | | ≥ 65,000 and < 240,000 | 1.82 |
| | | ≥ 240,000 and < 760,000 | 1.73 |
| | Horizontal | < 65,000 | 2.44 |
| | | ≥ 65,000 and < 240,000 | 2.10 |
| | | ≥ 240,000 and < 760,000 | 2.10 |

| System Type | Duct Location | Capacity [Btu/hr] | Baseline Efficiencies for Downflow/Upflow Units [NSenCOP] |
|---|---------------|------------------------|---|
| Ceiling Mounted | | | |
| Air cooled with free air discharge condenser | Ducted | < 29,000 | 2.05 |
| | | ≥ 29,000 and < 65,000 | 2.02 |
| | | ≥ 65,000 and < 760,000 | 1.92 |
| | Nonducted | < 29,000 | 2.08 |
| | | ≥ 29,000 and < 65,000 | 2.05 |
| | | ≥ 65,000 and < 760,000 | 1.94 |
| Air cooled with free air discharge condenser and fluid economizer | Ducted | < 29,000 | 2.01 |
| | | ≥ 29,000 and < 65,000 | 1.97 |
| | | ≥ 65,000 and < 760,000 | 1.87 |
| | Nonducted | < 29,000 | 2.04 |
| | | ≥ 29,000 and < 65,000 | 2.00 |
| | | ≥ 65,000 and < 760,000 | 1.89 |
| Air cooled with ducted condenser | Ducted | < 29,000 | 1.86 |
| | | ≥ 29,000 and < 65,000 | 1.83 |
| | | ≥ 65,000 and < 760,000 | 1.73 |
| | Nonducted | < 29,000 | 1.89 |
| | | ≥ 29,000 and < 65,000 | 1.86 |
| | | ≥ 65,000 and < 760,000 | 1.75 |
| Air cooled with fluid economizer and ducted condenser | Ducted | < 29,000 | 1.82 |
| | | ≥ 29,000 and < 65,000 | 1.78 |
| | | ≥ 65,000 and < 760,000 | 1.68 |
| | Nonducted | < 29,000 | 1.85 |
| | | ≥ 29,000 and < 65,000 | 1.81 |
| | | ≥ 65,000 and < 760,000 | 1.70 |
| Water cooled | Ducted | < 29,000 | 2.38 |
| | | ≥ 29,000 and < 65,000 | 2.28 |
| | | ≥ 65,000 and < 760,000 | 2.18 |
| | Nonducted | < 29,000 | 2.41 |
| | | ≥ 29,000 and < 65,000 | 2.31 |

| System Type | Duct Location | Capacity [Btu/hr] | Baseline Efficiencies for Downflow/Upflow Units [NSenCOP] |
|-------------------------------------|---------------|------------------------|---|
| | | ≥ 65,000 and < 760,000 | 2.20 |
| Water cooled with fluid economizer | Ducted | < 29,000 | 2.33 |
| | | ≥ 29,000 and < 65,000 | 2.23 |
| | | ≥ 65,000 and < 760,000 | 2.13 |
| | Nonducted | < 29,000 | 2.36 |
| | | ≥ 29,000 and < 65,000 | 2.26 |
| | | ≥ 65,000 and < 760,000 | 2.16 |
| Glycol cooled | Ducted | < 29,000 | 1.97 |
| | | ≥ 29,000 and < 65,000 | 1.93 |
| | | ≥ 65,000 and < 760,000 | 1.78 |
| | Nonducted | < 29,000 | 2.00 |
| | | ≥ 29,000 and < 65,000 | 1.98 |
| | | ≥ 65,000 and < 760,000 | 1.81 |
| Glycol cooled with fluid economizer | Ducted | < 29,000 | 1.92 |
| | | ≥ 29,000 and < 65,000 | 1.88 |
| | | ≥ 65,000 and < 760,000 | 1.73 |
| | Nonducted | < 29,000 | 1.95 |
| | | ≥ 29,000 and < 65,000 | 1.93 |
| | | ≥ 65,000 and < 760,000 | 1.76 |

1.1.1 Energy and Demand Savings Methodology

13.4.4.4 Savings Algorithms and Input Variables

Energy Savings

$$Energy\ Savings\ [\Delta kWh] = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times EFLH_C \times \frac{1\ kWh}{3,412\ Btu}$$

Equation 0-1

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \left(\frac{Cap_{C,pre}}{\eta_{baseline,C}} - \frac{Cap_{C,post}}{\eta_{installed,C}} \right) \times DF \times \frac{1 \text{ kW}}{3,412 \text{ Btuh}}$$

Equation 0-2

Where:

$Cap_{C,pre}$ = For ER and ROB, rated equipment cooling capacity of the newly installed equipment at AHRI standard conditions with a maximum of 20 percent larger than the post-capacity; for NC, rated equipment cooling capacity of the new equipment at AHRI-standard conditions [Btuh]; 1 ton = 12,000 Btuh.

$Cap_{C,post}$ = Rated equipment cooling capacity of the newly installed equipment at AHRI standard conditions with a maximum equal to the baseline pre-capacity [Btuh]; 1 ton = 12,000 Btuh.

Note: The capacity in the equations may not always match the capacity of the units. AHRI may rate cooling capacity in kW. In these cases, convert from kW to btu/hr by multiplying kW by 3,412.

$\eta_{baseline,C}$ = Cooling efficiency of existing equipment (ER) or standard equipment (ROB/NC) [SCOP for ER, NSenCOP for ROB/NC] in Table 0-1 or Table 0-2.

$\eta_{installed,C}$ = Rated cooling efficiency of the newly installed equipment [NSenCOP]. Efficiency rating must exceed ROB/NC baseline efficiency standards in Table 0-2.

Note: Use SCOP/NSenCOP for both kW and kWh savings calculations.

$EFLH_C$ = Cooling equivalent full-load hours for appropriate equipment type [hours] in Table 0-4.

DF = Demand factor (NCP, CP, or 4CP) for appropriate equipment type in Table 0-5.

1,000 = Constant to convert from watts to kilowatts.

3,412 = Constant to convert from Btu to kWh.

Early Retirement Savings

The first-year savings algorithms in the above equations are used for all HVAC projects, across NC, ROB, and ER projects. However, ER projects require a weighted savings calculated over both the ER and ROB periods taking the EUL and RUL into account. The ER savings are applied over the remaining useful life (RUL) period, and the ROB savings are applied over the remaining period (EUL-RUL). The final reported savings for ER projects are not actually a “first-year” savings, but an “average annual savings over the lifetime (EUL) of the measure.” These savings calculations are explained in Section 22.1.

When downsizing, the pre-installed cooling capacity is limited to a maximum of 120 percent of the new equipment’s cooling capacity. There is no cap when upsizing because the savings are calculated using the lower pre-capacity. For scenarios involving the replacement of a combination of the systems by an alternate combination of systems of varying capacities, ER savings can still be claimed if the overall pre- and post-capacities for the total combination of the systems are compliant with the above guidance. In these cases, a custom calculation should be performed to establish the following weighted savings factors to be applied over the ER portion of the savings calculation: manufacturer year, EUL, RUL, baselines efficiency, demand factor, and EFLH. These factors should be weighted based on contribution to overall capacity

13.4.4.5 Deemed Energy Savings Tables

Table 0-4 contains the effective full load hours for CRACs for data centers in San Antonio. This measure is restricted to the data center building types, derived from the EIA CBECS study.⁵⁹¹

Table 0-3: [CRACs] Commercial HVAC Building Type Descriptions and Examples

| Building Type | Definition | Detailed Business Type Examples |
|---------------|---|---------------------------------|
| Data Center | Buildings used to house computer systems and associated components. | 1) Data Center |

Table 0-4: [CRACs] Equivalent Full-Load Hours

| Building Type | EFLH _C | EFLH _H |
|---------------|-------------------|-------------------|
| Data Center | 4,022 | - |

13.4.4.6 Deemed Demand Savings Tables

Table 0-5 contains the NCP, CP, and 4CP demand factors for CRACs for data centers in San Antonio.

Table 0-5: [CRACs] Demand Factors

| Peak Type | DF |
|-----------|------|
| NCP | 1.07 |
| CP | 1.05 |
| 4CP | 0.89 |

⁵⁹¹ The Commercial Building Energy Consumption Survey (CBECS) implemented by the US Energy Information Administration includes a principal building activity categorization scheme that separates the commercial sector into 29 categories and 51 subcategories based on principal building activity (PBA). For its purposes, the CBECS defines commercial buildings as those buildings greater than 1,000 square feet that devote more than half of their floor space to activity that is neither residential, manufacturing, industrial, nor agricultural. The high-level building types adopted for the TRM are adapted from this CBECS categorization, with some building types left out and one additional building type - Large Multifamily – included.

13.4.4.7 Measure Life and Lifetime Savings

The EUL and RULs for this HVAC equipment are provided below. The reader should refer to the definitions of effective useful life and remaining useful life in the glossary in Volume 1 of the Texas TRM for guidance on how to determine the decision type for system installations.

Estimated Useful Life (EUL)

The EUL is 15 years for split and packaged ACs and HPs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID HVAC-airAC and HVAC-airHP.⁵⁹² This EUL is also applicable for CRACs.

Remaining Useful Life (RUL)

The RUL of replaced systems is provided according to system age in Table 0-6. If individual system components were installed at different times, use the condenser age as a proxy for the entire system. For ER units of unknown age, assume a default value equal to the EUL. This corresponds to a default RUL of 2.8 years. Default RUL may be used exclusively if applied consistently for all projects. Otherwise, the default should only be used when a project is reported and documented as having a nameplate that is illegible. Both the RUL and EUL are needed to estimate savings for ER projects for two distinct periods: The ER period (RUL) and the ROB period (EUL - RUL). The calculations for ER projects are extensive, and as such are provided in Section 22.1.

Table 0-6: [CRACs] Remaining Useful Life or Replaced Unit^{593, 594}

| Age in Years of Replaced System | Split and Packaged A/C and HP Systems [years] | Age in Years of Replaced System | Split and Packaged A/C and HP Systems [years] |
|---------------------------------|---|---------------------------------|---|
| 1 | 14.0 | 10 | 5.7 |
| 2 | 13.0 | 11 | 5.0 |
| 3 | 12.0 | 12 | 4.4 |
| 4 | 11.0 | 13 | 3.8 |
| 5 | 10.0 | 14 | 3.3 |
| 6 | 9.1 | 15 | 2.8 |
| 7 | 8.2 | 16 | 2.0 |
| 8 | 7.3 | 17 | 1.0 |

⁵⁹² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

⁵⁹³ Current NC baseline matches the baseline for existing systems manufactured in 2023. Existing CRAC systems manufactured after 5/28/2024 are not eligible to use the early retirement baseline and should use the ROB baseline instead. Grayed out values are displayed for informational purposes only.

⁵⁹⁴ PUCT Docket No. 40083, Attachment A describes the process in which the RUL of replaced systems has been calculated.

| Age in Years of Replaced System | Split and Packaged A/C and HP Systems [years] | Age in Years of Replaced System | Split and Packaged A/C and HP Systems [years] |
|---------------------------------|---|---------------------------------|---|
| 9 | 6.5 | 18 ⁵⁹⁵ | 0.0 |

13.4.5 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline type: ER, ROB, NC, system type conversion
- Baseline equipment type
- Baseline unit quantity
- Baseline rated cooling and heating capacity
- For ER ONLY: baseline Age and Method of Determination (e.g., nameplate, blueprints, customer reported, not available)
- For ER ONLY: photograph of retired unit nameplate demonstrating model number, serial number, and manufacturer if blueprints are not provided; if photograph of nameplate is unavailable or not legible, provide a photo and/or description documenting the reason why the nameplate photo was unobtainable (alternate forms of documentation can be approved at the evaluator's discretion)
- Manufacturer, model, and serial number of new unit
 - AHRI/DOE CCMS certificates or reference number matching model number
- New unit equipment type
- New equipment flow type/duct location
- New unit quantity
- New unit rated cooling capacity
- New unit cooling efficiency rating
- Proof of purchase: invoice showing model number; photo(s) of the model number on product

⁵⁹⁵ RULs are capped at the 75th percentile of equipment age, 18 years, as determined based on DOE survival curves. Systems older than 18 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

packaging or installed unit(s); OR evaluator pre-approved approach

- For NC ONLY, as built design drawings or HVAC specifications package that provides detailed manufacturer and model number information on installed unit(s) may also be accepted as the proof of purchase

Document Revision History

Table 0-7: [CRACs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Added reference to new standard and plan to incorporate in PY2025. |
| FY 2026 | Added early retirement criteria related to downsizing, updated early retirement and new construction/ROB baseline efficiency levels. |

13.5 HVAC VARIABLE FREQUENCY DRIVES

13.5.1 Measure Description

This measure involves the installation of a variable frequency drive (VFD) in a commercial HVAC application. Eligible applications include:

- AHU supply fan on a split or packaged HVAC system. The fan is in a variable air volume (VAV) system with terminal VAV boxes or constant air volume (CAV) unit with no control device.
- Hot water distribution pumps.
- Chilled water distribution and condenser pumps.
- Cooling tower fans

This measure does not apply to controls installed on the HVAC compressor. This measure accounts for the interactive air-conditioning demand savings during the peak demand period. The savings are on a per-control basis and the lookup tables show the total savings for eligible scenarios.

13.5.1.1 Eligibility Criteria

Supply fans may not have variable pitch blades. Supply fan drives must be less than or equal to 100 horsepower (hp). New construction systems are ineligible. Equipment used for process loads are ineligible.

13.5.1.2 Baseline Condition

The AHU supply fan baseline is a centrifugal supply fan with a single-speed motor on a direct expansion (DX) VAV or CAV air-conditioning (AC) unit. The motor is a standard efficiency motor based on ASHRAE Standard 90.1-2013 standards, which are provided by horsepower. The AC unit has standard cooling efficiency based on IECC 2015. The part-load fan control is an outlet damper, inlet damper, inlet guide vane, or no control (constant volume systems).

The HVAC pump baseline is a constant speed pump with a standard-efficiency motor. This measure is applicable to both primary and secondary hot or chilled water pumping systems.

The cooling tower fan baseline control is either fan cycling or any fan design that enables two-speed operation.

13.5.1.3 High-Efficiency Condition

The high efficiency condition is installation of a VFD on an AHU supply fan, cooling tower fan, condenser water pump, hot water pump, or chilled water pump.

For AHU supply fans, when applicable, the existing damper or inlet guide vane will be removed or set completely open permanently after installation. The VFD will maintain a constant static pressure by adjusting fan speed and delivering the same amount of air as the baseline condition.

13.5.2 Energy and Demand Savings Methodology

13.5.2.1 Savings Algorithms and Input Variables

Demand savings are calculated for each hour over the course of the year:

Step 1 – Determine the percent flow rate for each hour of the year, i .

Flow Rate for AHUs:

$$\%CFM_i = m \times t_{db\ i} + b$$

Equation 13.5-1

Where:

$t_{db\ i}$ = Dry bulb air temperature (DBT) at i^{th} hour taken from TMY3 hourly weather data.⁵⁹⁶

m = The slope of the relationship between DBT and CFM; see Table 13.5-1.

b = the intercept of the relationship between DBT and CFM; see Table 13.5-1.

The minimum flow rate is set to 60%CFM based on common design practice.⁵⁹⁷ Determination of the minimum dry bulb temperature assumes that cooling will only operate above the cooling reference temperature of 65°F dry bulb. The maximum DBT is the ASHRAE dry bulb design temperature for San Antonio.⁵⁹⁸

Table 13.5-1: [HVAC VFDs] AHU VFD %CFM Inputs

| Condition | Min | Max | Slope (m) | Intercept (b) |
|------------------|-----|------|-----------|---------------|
| Flow Rate (%cfm) | 60 | 100 | 1.17 | -15.80 |
| Dry Bulb T (°F) | 65 | 99.3 | | |

⁵⁹⁶ National Renewable Energy Laboratory's (NREL) National Solar Radiation Data Base: 1991 - 2005 Update for Typical Meteorological Year 3 (TMY3). Available at <https://sam.nrel.gov/weather-data.html>.

⁵⁹⁷ For AHU, a 60% minimum setpoint strategy is assumed, so any results below 60% are set to 60%. Similarly, any results greater than 100% are set to 100%.

⁵⁹⁸ ASHRAE 2021 Fundamentals, Ch 14 Appendix: design conditions for selected locations, 0.4% Cooling DB.

Flow Rate for Cooling Towers:

$$\%CFM_i = m \times t_{wb\ i} + b$$

Equation 13.5-2

Where:

$t_{db\ i}$ = Wet bulb air temperature (WBT) at i^{th} hour taken from TMY3 hourly weather data.⁵⁹⁹

m = The slope of the relationship between WBT and CFM; see Table 13.5-2.

b = the intercept of the relationship between WBT and CFM; see Table 13.5-2.

Table 13.5-2: [HVAC VFDs] Cooling Tower VFD %CFM Inputs

| Condition | Min | Max | Slope (m) | Intercept (b) |
|------------------|-------|------|-----------|---------------|
| Flow Rate (%cfm) | 40 | 100 | 3.24 | -153.26 |
| Wet Bulb T (°F) | 56.60 | 78.1 | | |

The minimum flow rate is set to 40 percent cfm based on the ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual.⁶⁰⁰ Determination of the minimum WBT assumes that the cooling tower will only operate above the cooling reference temperature of 65°F dry bulb. The minimum WBT is calculated using TMY3 data as the average WBT when the DBT is between 64°F and 65°F dry bulb. The maximum WBT is the ASHRAE wet bulb design temperature.⁶⁰¹

Flow Rate for Chilled Water and Condenser Pumps:

$$\%GPM_i = m \times t_{db\ i} + b$$

Equation 13.5-3

Where:

$t_{db\ i}$ = the hourly dry bulb temperature (DBT) based on TMY3 data.⁶⁰²

m = the slope of the relationship between DBT and GPM; see Table 13.5-3.

b = the intercept of the relationship between DBT and GPM; see Table 13.5-3.

The minimum flow rate is set to 10%GPM based on the ANSI/ASHRAE/IES Standard 90.1-2016

⁵⁹⁹ TMY3 data does not include WBT. WBT was estimated from TMY3 data by subtracting the dewpoint depression divided by 3 from the dry bulb temperature. This method is known as the “1/3rd rule” and is a shorthand technique often used to obtain a satisfactory approximation of the actual wet bulb temperature.

<https://theweatherprediction.com/habyhints/170/#:~:text=The%20technique%20is%20to%20first,for%20the%20wet-bulb%20temperature.>

⁶⁰⁰ PNNL, ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual, page 3.240, cooling tower minimum speed default.

⁶⁰¹ ASHRAE 2021 Fundamentals, Ch 14 Appendix: design conditions for selected locations, 0.4% Evaporation WB

⁶⁰² National Renewable Energy Laboratory's (NREL) National Solar Radiation Data Base: 1991 - 2005 Update for Typical Meteorological Year 3 (TMY3). Available at <https://sam.nrel.gov/weather-data.html>.

Performance Rating Method Reference Manual.⁶⁰³ Determination of the minimum dry bulb temperature assumes that cooling will only operate above the cooling reference temperature of 65°F dry bulb. The maximum DBT is the ASHRAE dry bulb design temperature for San Antonio.⁶⁰⁴

Table 13.5-3: [HVAC VFDs] Chilled Water and Condenser Water Pump VFD %GPM Inputs

| Condition | Min | Max | Slope (m) | Intercept (b) |
|------------------|-----|------|-----------|---------------|
| Flow Rate (%gpm) | 10 | 100 | 2.62 | -160.55 |
| Dry Bulb T (°F) | 65 | 99.3 | | |

Flow Rate for Hot Water Pumps:

$$\%GPM_i = m \times t_{db_i} + b$$

Equation 13.5-4

Where:

t_{db_i} = the hourly dry bulb temperature (DBT) based on TMY3 data.

m = the slope of the relationship between DBT and GPM; see Table 13.5-4.

b = the intercept of the relationship between DBT and GPM; see Table 13.5-4.

The minimum flow rate is set to 10%GPM based on the ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual.⁶⁰⁵ Determination of the minimum dry bulb temperature assumes that heating will only operate below the reference temperature of 65°F dry bulb. The maximum DBT is the ASHRAE dry bulb design temperature for San Antonio.⁶⁰⁶

Table 13.5-4: [HVAC VFDs] Hot Water Pump VFD %GPM Inputs

| Condition | Min | Max | Slope (m) | Intercept (b) |
|------------------|-----|------|-----------|---------------|
| Flow Rate (%gpm) | 10 | 100 | -2.56 | 176.67 |
| Dry Bulb T (°F) | 65 | 30.0 | | |

Step 2 – Calculate the percentage of power (% power) for the applicable baseline and the new VFD technology:

⁶⁰³ PNNL, ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual, page 3.249, pump minimum speed default.

⁶⁰⁴ ASHRAE 2021 Fundamentals, Ch 14 Appendix: design conditions for selected locations, 0.4% Cooling DB.

⁶⁰⁵ PNNL, ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual, page 3.249, pump minimum speed default.

⁶⁰⁶ ASHRAE 2021 Fundamentals, Ch 14 Appendix: design conditions for selected locations, 99.6% Heating DB.

Baseline Technologies

For AHU Supply Fans:⁶⁰⁷

$$\%power_{i,OutletDamper} = 0.00745 \times \%CFM_i^2 + 0.10983 \times \%CFM_i + 20.41905$$

Equation 13.5-5

$$\%power_{i,InletDamper} = 0.00013 \times \%CFM_i^3 - 0.01452 \times \%CFM_i^2 + 0.71648 \times \%CFM_i + 50.25833$$

Equation 13.5-6

$$\%power_{i,InletGuideVane} = 0.00009 \times \%CFM_i^3 - 0.00128 \times \%CFM_i^2 + 0.06808 \times \%CFM_i + 20$$

Equation 13.5-7

Note: %power for baseline technologies with no fan control is set equal to 1 for each hour where %power is less than 1 for the other baseline control types. When %power exceeds 1 for the other baseline control types, %power for no fan control is set equal to the maximum value from the other baseline control types.

For Cooling Tower:

$$\%power_{i,fan\ cycling} = \text{if } t_{wb_i} > t_{wb_min}, \text{ then } 1, \text{ otherwise } 0$$

Equation 13.5-8

For Chilled, Hot, and Condenser Water Pumps⁶⁰⁸:

$$\%power_{base} = 2.5294 \times \%GPM_i^3 - 4.7443 \times \%GPM_i^2 + 3.2485 \times \%GPM_i + 0$$

Equation 13.5-9

VFD Technology

For AHU Supply Fans:

$$\%power_{i,VFD} = 0.00004 \times \%CFM_i^3 + 0.00766 \times \%CFM_i^2 - 0.19567 \times \%CFM_i + 5.9$$

Equation 13.5-10

For Cooling Tower:⁶⁰⁹

$$\begin{aligned} \text{if } t_{wb_i} > t_{wb_min}, \text{ then } \%power_{VFD} \\ = 0.9484823 \times \%CFM_i^3 + 0.60556507 \times \%CFM_i^2 - 0.88567609 \times \%CFM_i \\ + 0.33162901, \text{ otherwise } 0 \end{aligned}$$

Equation 13.5-11

⁶⁰⁷ https://focusonenergy.com/sites/default/files/Focus%20on%20Energy_TRM_January2015.pdf, page 225. Please note, the CFM² coefficients in Equation 36 and Equation 37 have the wrong sign in the reference document.

⁶⁰⁸ PNNL, ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual, Table 87 Default Part-Load CIRC-PUMP-FPLR Coefficients – Constant Speed, no VSD.

⁶⁰⁹ PNNL, ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual, Table 85 Default Efficiency TWR-FAN-PLR Coefficients – VSD on Cooling Tower Fan.

For Chilled, Hot, and Condenser Water Pumps⁶¹⁰:

$$\%power_{VFD} = 0.7347 \times \%GPM_i^3 - 0.301 \times \%GPM_i^2 + 0.5726 \times \%GPM_i + 0$$

Equation 13.5-12

Note: for all applications, baseline %power should use a minimum of zero.

Demand Savings

Demand Savings are calculated for each hour, *i*, over the course of the year:

Step 3 – Calculate kW_{full} by using the horsepower from the motor nameplate, load factor, and the applicable motor efficiency corresponding to the motor horsepower in use shown in Table 13.5-5. Use that result and the hourly %power results for both the baseline and VFD technology to determine power consumption at each hour.

$$kW_{full} = 0.746 \times HP \times \frac{LF}{\eta}$$

Equation 13.5-13

$$kW_i = kW_{full} \times \%power_i$$

Equation 13.5-14

Where:

| | | |
|-------------|---|---|
| $\%power_i$ | = | Percentage of full load power at the <i>i</i> th hour calculated by an equation based on the technology and control type (outlet damper, inlet box damper, inlet guide vane-IGV, or VFD). ⁶¹¹ |
| kW_{full} | = | motor power demand operating at the design 100% flow[kW]. |
| kW_i | = | real-time power at the <i>i</i> th hour of a year [kW]. |
| HP | = | Rated horsepower of the motor [hp]. |
| LF | = | Load factor – ratio of the operating load to the nameplate rating of the motor – assumed to be 75%. |
| η | = | [For Fans]: Motor efficiency of a standard efficiency Open Drip Proof (ODP) motor operating at 1800 RPM taken from ASHRAE Standard 90.1-2013, Reference Table 13.5-5. [For Pumps]: Assumed to be 0.9 for all motor sizes. |
| 0.746 | = | Constant to convert from horsepower to kilowatts. |

⁶¹⁰ PNNL, ANSI/ASHRAE/IES Standard 90.1-2016 Performance Rating Method Reference Manual, Table 87 Default Part-Load CIRC-PUMP-FPLR Coefficients – Default (VSD, No Reset).

⁶¹¹ Fan curves by control type are provided in the BPA ASD Calculator, <https://www.bpa.gov/EE/Sectors/Industrial/Documents/ASDCalculators.xls>.

Table 13.5-5: [HVAC VFDs] Motor Efficiencies for Open Drip Proof Motors at 1,800 RPM ^{612,613}

| Motor Size (hp) | Nominal Efficiency |
|-----------------|--------------------|
| 1 | 0.855 |
| 2 | 0.865 |
| 3 | 0.865 |
| 5 | 0.895 |
| 7.5 | 0.910 |
| 10 | 0.917 |
| 15 | 0.930 |
| 20 | 0.930 |
| 25 | 0.936 |
| 30 | 0.941 |
| 40 | 0.941 |
| 50 | 0.945 |
| 60 | 0.950 |
| 75 | 0.950 |
| 100 | 0.954 |

Step 4 – Calculate the kW savings for each hour across the year. The kW savings are equal to the hourly kW usage difference between the baseline and VFD, multiplied by the occupancy schedule for the specific hour of operation by using the following.

Hourly Savings Calculations

$$(kW_i)_{\text{Saved}} = [(kW_i)_{\text{Baseline}} - (kW_i)_{\text{VFD}}] \times \text{schedule}_i$$

Equation 13.5-15

Where:

schedule_i = Occupancy schedule. 1 when building is occupied, 0.2 when building is unoccupied; see Table 13.5-6.

⁶¹² Table 10.8 Minimum Nominal Efficiency for General Purpose Design A and Design B Motors in ASHRAE Standard 90.1-2004, Standard Efficiency Open Drip Proof Motors at 1800 RPM.

⁶¹³ For unlisted motor horsepower values, round down to the next lowest horsepower value.

Table 13.5-6: [HVAC VFDs] Yearly Motor Operation Hours by Building Type⁶¹⁴

| Building Type | Weekday Schedule | Weekend Schedule | Annual Motor Operation Hours |
|---|------------------|--|------------------------------|
| Assembly, Worship | 9am-11pm | 9am-11pm | 5,840 |
| Convenience Store, Service, Strip Mall | 9am-10pm | 9am-8pm (Saturday) 10am-7pm (Sunday) | 5,298 |
| Education | 8am-11pm | Closed | 4,884 |
| Hospitals, Healthcare, Nursing Home, Hotel (common areas), Large Multifamily (Common Areas) | 24 hr | 24 hr | 8,760 |
| Office—Large, Medium | 7am-11pm | 7am-7pm (Saturday) | 5,592 |
| Office—Small | 7am-8pm | Closed | 4,466 |
| Restaurants | 6am-2am | 6am-2am | 7,592 |
| Stand-alone Retail, Supermarket- | 8am-10pm | 8am-11pm (Saturday) 10am-7pm (Sunday) | 5,674 |
| Warehouse | 7am-7pm | Closed | 4,258 |
| Other ⁶¹⁵ | 7am-7pm | Closed | 4,258 |

From these hourly kW savings, the methodologies in Section 2.3 provide the kW demand savings for the non-coincident peak, coincident peak, and ERCOT 4CP. The total NCP, CP, or 4CP demand saved can be calculated by multiplying the kW saved by the peak demand interactive effects factor, as shown below.

Total Peak Demand Saved Calculation, including interactive effects, applies only to AHUs.

$$Demand\ Savings\ [\Delta kW] = kW_{Saved} \times \left(1 + \frac{3.412}{Cooling_{SEER}}\right)$$

Equation 13.5-16

⁶¹⁴ Hours for all building types except for Assembly come from the Department of Energy Commercial Building Prototype Models, Scorecards, HVAC Operation Schedule. Motor hours are set to equal 1 when the HVAC Operation Schedule is “on” and 0.2 when the HVAC Operation Schedule is “off.” https://www.energycodes.gov/development/commercial/prototype_models. Assembly occupied hours come from COMNET Appendix C—Schedules (Rev 3) <https://comnet.org/appendix-c-schedules> updated 07/25/2016.

⁶¹⁵ The “other” building type may be used when none of the listed building types apply. The values used for other are the most conservative of the listed building types.

Where:

$$Cooling_{SEER} = \text{Air conditioner cooling efficiency, assumed at 12.6, based on IECC 2015 minimum efficiency of a unitary AC system between 5 and 10 tons.}$$

Energy Savings

Step 1 – For both the baseline and new technology, calculate the sum of individual kWh consumption in each hour of the year:

$$Annual\ kWh_{baseline\ or\ VFD} = \sum_{i=1}^{8,760} (kW_i \times schedule_i)$$

Equation 13.5-17

Where:

$$8,760 = \text{Total hours per year.}$$

Step 2 – Subtract the Annual kWh_{VFD} from the Annual kWh_{baseline} to get the Annual Energy Savings.

$$Energy\ Savings\ [\Delta kWh] = kWh_{baseline} - kWh_{VFD}$$

Equation 13.5-18

13.5.2.2 Deemed Energy and Demand Savings Tables

The energy and demand savings tables listed are calculated based on San Antonio specific TMY3 weather data and are presented per motor hp.

Table 13.5-7: [HVAC VFDs] Deemed Savings for AHU Outlet Damper Part-Load Fan Control per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 655 | 0.143 | 0.083 | 0.092 |
| Convenience Store, Service, Strip Mall | 585 | | | |
| Education | 551 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 1,044 | | | |
| Large Multifamily | 1,044 | | | |
| Office—Large, Medium | 632 | | | |
| Office—Small | 499 | | | |
| Restaurants | 886 | | | |
| Stand-alone Retail, Supermarket | 633 | | | |
| Warehouse | 474 | | | |
| Other | 474 | | | |

Table 13.5-8: [HVAC VFDs] Deemed Savings for AHU Inlet Damper Part-Load Fan Control per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 947 | 0.235 | 0.097 | 0.110 |
| Convenience Store, Service, Strip Mall | 843 | | | |
| Education | 799 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 1,546 | | | |
| Large Multifamily | 1,546 | | | |
| Office—Large, Medium | 917 | | | |
| Office—Small | 722 | | | |
| Restaurants | 1,300 | | | |
| Stand-alone Retail, Supermarket | 914 | | | |
| Warehouse | 686 | | | |
| Other | 686 | | | |

Table 13.5-9: [HVAC VFDs] Deemed Savings for AHU Inlet Guide Vane Part-Load Fan Control per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 188 | 0.052 | 0.016 | 0.018 |
| Convenience Store, Service, Strip Mall | 167 | | | |
| Education | 159 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 312 | | | |
| Large Multifamily | 312 | | | |
| Office—Large, Medium | 182 | | | |
| Office—Small | 143 | | | |
| Restaurants | 261 | | | |
| Stand-alone Retail, Supermarket | 181 | | | |
| Warehouse | 136 | | | |
| Other | 136 | | | |

Table 13.5-10: [HVAC VFDs] Deemed Savings for AHU No Existing Fan Control per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 1,710 | 0.423 | 0.151 | 0.202 |
| Convenience Store, Service, Strip Mall | 1,519 | | | |
| Education | 1,443 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 2,803 | | | |
| Large Multifamily | 2,803 | | | |
| Office—Large, Medium | 1,657 | | | |
| Office—Small | 1,302 | | | |
| Restaurants | 2,356 | | | |
| Stand-alone Retail, Supermarket | 1,649 | | | |
| Warehouse | 1,237 | | | |
| Other | 1,237 | | | |

Table 13.5-11: [HVAC VFDs] Deemed Savings for Cooling Tower Fans per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 800 | 0.526 | - | 0.088 |
| Convenience Store, Service, Strip Mall | 718 | | | |
| Education | 660 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 1,279 | | | |
| Large Multifamily | 1,279 | | | |
| Office—Large, Medium | 768 | | | |
| Office—Small | 594 | | | |
| Restaurants | 1,074 | | | |
| Stand-alone Retail, Supermarket | 769 | | | |
| Warehouse | 563 | | | |
| Other | 563 | | | |

Table 13.5-12: [HVAC VFDs] Deemed Savings for Chilled Water Pumps per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 933 | 0.295 | 0.138 | 0.227 |
| Convenience Store, Service, Strip Mall | 847 | | | |
| Education | 777 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 1,360 | | | |
| Large Multifamily | 1,360 | | | |
| Office—Large, Medium | 894 | | | |
| Office—Small | 704 | | | |
| Restaurants | 1,195 | | | |
| Stand-alone Retail, Supermarket | 908 | | | |
| Warehouse | 668 | | | |
| Other | 668 | | | |

Table 13.5-13: [HVAC VFDs] Deemed Savings for Hot Water Pumps per Motor hp

| Building Type | Savings per Motor HP | | | |
|--|----------------------|--------|-------|--------|
| | kWh | NCP kW | CP kW | 4CP kW |
| Assembly, Worship | 346 | 0.295 | - | - |
| Convenience Store, Service, Strip Mall | 300 | | | |
| Education | 302 | | | |
| Hospitals, Healthcare, Nursing Home, Hotel | 623 | | | |
| Large Multifamily | 623 | | | |
| Office—Large, Medium | 341 | | | |
| Office—Small | 269 | | | |
| Restaurants | 510 | | | |
| Stand-alone Retail, Supermarket | 331 | | | |
| Warehouse | 255 | | | |
| Other | 255 | | | |

13.5.2.3

13.5.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years for HVAC VFDs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID HVAC-VSD-fan.⁶¹⁶

13.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- Application type (AHU fan, cooling tower, chilled water pump, hot water pump)
- Motor horsepower
- For AHU supply fans, baseline part-load control type (outlet damper, inlet damper, inlet guide vane, constant volume/no control)

⁶¹⁶ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 13.5-14: [HVAC VFDs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Added cooling tower fan and condenser water pump applications. Updated maximum temperatures for linear regression equations to correspond with ASHRAE design conditions. Aligned building type names across all commercial measures. |
| FY 2026 | Savings calculations moved to Excel. Reviewed hours of operation and using same fan and pump hours referenced in the existing measure. |

14. COMMERCIAL: BUILDING ENVELOPE

14.1 COOL ROOFS

14.1.1 Measure Description

Reflective roofing materials reduce the overall heat load on a building by reducing the total heat energy absorbed into the building system from incident solar radiation. This reduction in total load provides space cooling energy savings during the cooling season but reduces free heat during the heating season, so the measure saves energy in the summer but uses more energy in winter. Cool roofs are most beneficial in warmer climates and may not be recommended for buildings where the primary heat source is electric resistance. The measure is for retrofit of existing buildings.

14.1.1.1 Eligibility Criteria

Eligibility Criteria

The ENERGY STAR roofing products certification program was discontinued effective June 1, 2022.⁶¹⁷ Moving forward, installed roofing products will still be required to demonstrate compliance with the previous ENERGY STAR specification.⁶¹⁸ For nonresidential facilities, these criteria for a high-efficiency roof include:

- An existing roof undergoing retrofit conditions as further defined under high-efficiency condition below; a roof installed in a new construction application is not eligible for applying these methodologies.
- A roof with a low slope of 2:12 inches or less.⁶¹⁹
- An initial solar reflectance of greater than or equal to 65%.
- A 3-year solar reflectance of greater than or equal to 50%.
- 75 percent of the roof surface over conditioned space must be replaced.
- No significant obstruction of direct sunlight to roof.
- The facility must be conditioned with central cooling, heating, or both.
- In lieu of the former ENERGY STAR list of qualified products, roofing products must now have a

⁶¹⁷ ENERGY STAR® Roof Products Sunset Decision Memo.

<https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Roof%20Products%20Sunset%20Decision%20Memo.pdf>.

⁶¹⁸ ENERGY STAR® Program Requirements for Roof Products v2.1.

https://www.energystar.gov/ia/partners/product_specs/program_reqs/roofs_prog_req.pdf.

⁶¹⁹ As defined in proposed ASTM Standard E 1918-97.

performance rating that is validated by the Cool Roof Rating Council (CRRC) ^{620,621} and be listed on the CRRC Rated Roof Products Directory.⁶²² This is consistent with the former ENERGY STAR test criteria's allowance for products already participating in the CRRC Product Rating Program⁶²³ to submit solar reflectance and thermal emittance product information derived from CRRC certification.

If one of these conditions are not met, the deemed savings approach cannot be used, and the Simplified M&V Methodology or the Full M&V Methodology must be used.

14.1.1.2 Baseline Condition

The baseline is the thermal resistance (i.e., R-value) of the existing roof make-up, and the solar reflectance and emissivity of the surface layer. The R-value is estimated based on code envelope requirements applicable in the year of construction. Solar reflectance and emissivity of the surface layer are assumed to be 0.2 and 0.9 respectively, based on roof properties listed in the LBLN Roofing Materials Database.⁶²⁴

The cooling and heating efficiencies are assumed based on the space conditioning of the top floor of the building and are based on typical code requirements applicable in the year of construction.

Table 14.1-1: [Cool Roofs] Assumed Cooling and Heating Efficiencies

| Year of Construction; Applicable Code | RTU | PTHP Cooling | PTHP Heating | Air Cooled Chiller | Water Cooled Chiller |
|---|-----|--------------|--------------|--------------------|----------------------|
| Before 2011; 2000 IECC | 2.9 | 2.9 | 2.9 | 2.5 | 4.2 |
| Between 2011-2016; 2009 IECC | 3.8 | 3.1 | 2.9 | 2.8 | 5.5 |
| After 2016; 2015 & 2018 IECC ⁶²⁵ | 3.8 | 3.1 | 2.9 | 2.8 | 5.5 |

14.1.1.3 High-Efficiency Condition

The high-efficiency condition depends on the project scope. The project scope is defined as one of:

- Adding surface layer only
- Adding insulation and surface layer

⁶²⁰ CRRC guidance for roof rating alternative to discontinued ENERGY STAR® program. <https://coolroofs.org/documents/CRRC-ENERGY-STAR-Sunset-Info-Sheet-2022-03-07.pdf>.

⁶²¹ CRRC Roof Rating Program. <https://coolroofs.org/programs/roof-rating-program>.

⁶²² CRRC Rated Roof Products Directory. <https://coolroofs.org/directory/roof>.

⁶²³ CRRC Rated Products Directory: <https://coolroofs.org/directory>.

⁶²⁴ Lawrence Berkeley National Lab Cool Roofing Material Database. <https://heatisland.lbl.gov/resources/cool-roofing-materials-database>.

⁶²⁵ There were no changes in the associated commercial HVAC efficiency requirements between IECC 2015 and 2018.

- Rebuilding entire roof assembly

If the project scope is only to add a new CRRC-rated material as the new surface layer, then the R-value used for the baseline condition is used for the high-efficiency condition. If the project scope is to add insulation and a CRRC-rated material as the new surface layer, then the R-value of the additional insulation is added to the R-value used for the baseline condition. If the entire roof assembly is rebuilt, then the R-value for each layer of the new roof construction is summed to get a total new R-value.

The measure requires installation of roof products that have been rated by the CRRC and demonstrate compliance with the previous ENERGY STAR-certified roof product performance specifications for the relevant roof application. Initial and 3-year reflectance ratings must meet or exceed the minimum thresholds specified in Table 14.1-2.

Table 14.1-2: [Cool Roofs] ENERGY STAR Specification⁶²⁶

| Roof Slope | Characteristic | Performance Specification |
|---------------------|---------------------------|---------------------------|
| Low Slope ≤ 2/12 | Initial Solar Reflectance | ≥ 0.65 |
| | 3-Year Solar Reflectance | ≥ 0.50 |

14.1.2 Energy and Demand Savings Methodology

14.1.2.1 Savings Algorithms and Input Variables

Energy savings are estimated using EnergyPlus v8.3.0 whole-building simulation. The prototype building characteristics match those used for developing Commercial HVAC demand factors and EFLH. The savings represent the difference of the modeled energy use of the baseline condition and the high efficiency condition divided by square foot of roof area. The demand savings are calculated following the method described in section 2.3.

The deemed energy and demand savings factors are used in the following formulas to calculate savings:

$$\text{Energy Savings } [\Delta kWh] = RA \times ESF$$

Equation 14.1-1

$$\text{Demand Savings } [\Delta kW] = RA \times DF \times 10^{-5}$$

Equation 14.1-2

Where:

$$RA = \text{Total area of ENERGY STAR roof [sq. ft].}$$

⁶²⁶ ENERGY STAR Roof Products Specification. https://www.energystar.gov/products/building_products/roof_products/key_product_criteria.

ESF = Energy Savings Factor from Table 14.1-4 by building type, pre/post insulation levels, and heating/cooling system.

DF = Demand factor for NCP, CP, or 4CP peak demand from Table 14.1-4 by building type, pre/post insulation levels, and heating/cooling system.

If the insulation levels are unknown, use the mapping in Table 14.1-3 to estimate the R-value based on the year of construction.

Table 14.1-3: [Cool Roofs] Estimated R-value based on Year of Construction

| Year of Construction | Estimated R-value ⁶²⁷ |
|----------------------|----------------------------------|
| Before 2011 | $R \leq 13$ |
| Between 2011 - 2016 | $13 \leq R \leq 20$ |
| After 2016 | $20 < R$ |

Table 14.1-4: [Cool Roofs] Savings Factors

| Building Type | Pre R-Value | Post R-Value | ESF | PSDF |
|---------------------|---------------------|---------------------|------|-------|
| Retail | $R \leq 13$ | $R \leq 13$ | 0.67 | 23.07 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 1.08 | 39.91 |
| | $R \leq 13$ | $20 < R$ | 1.10 | 42.66 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.43 | 13.86 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.44 | 15.85 |
| | $20 < R$ | $20 < R$ | 0.15 | 6.11 |
| Education - Chiller | $R \leq 13$ | $R \leq 13$ | 0.66 | 14.25 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.93 | 23.79 |
| | $R \leq 13$ | $20 < R$ | 1.06 | 27.75 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.35 | 7.90 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.42 | 11.03 |
| | $20 < R$ | $20 < R$ | 0.28 | 6.64 |

⁶²⁷ Estimated R-values are based on applicable code requirements in the year of construction.

| Building Type | Pre R-Value | Post R-Value | ESF | PSDF |
|------------------|---------------------|---------------------|------|-------|
| Education - RTU | $R \leq 13$ | $R \leq 13$ | 0.32 | 11.93 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.46 | 21.96 |
| | $R \leq 13$ | $20 < R$ | 0.51 | 25.08 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.20 | 8.44 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.25 | 11.44 |
| | $20 < R$ | $20 < R$ | 0.16 | 6.38 |
| Office - Chiller | $R \leq 13$ | $R \leq 13$ | 0.26 | 11.27 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.33 | 22.19 |
| | $R \leq 13$ | $20 < R$ | 0.37 | 24.96 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.14 | 9.37 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.18 | 11.91 |
| | $20 < R$ | $20 < R$ | 0.16 | 4.97 |
| Office - RTU | $R \leq 13$ | $R \leq 13$ | 0.31 | 10.95 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.51 | 19.30 |
| | $R \leq 13$ | $20 < R$ | 0.60 | 22.92 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.20 | 6.68 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.28 | 9.39 |
| | $20 < R$ | $20 < R$ | 0.16 | 5.49 |
| Hotel | $R \leq 13$ | $R \leq 13$ | 0.08 | 1.90 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.08 | 2.51 |
| | $R \leq 13$ | $20 < R$ | 0.08 | 2.78 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.06 | 1.35 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.06 | 1.60 |
| | $20 < R$ | $20 < R$ | 0.05 | 1.16 |
| Warehouse | $R \leq 13$ | $R \leq 13$ | 0.06 | 4.15 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.11 | 7.15 |
| | $R \leq 13$ | $20 < R$ | 0.19 | 12.05 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.03 | 1.96 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.09 | 5.93 |
| | $20 < R$ | $20 < R$ | 0.01 | 1.34 |

| Building Type | Pre R-Value | Post R-Value | ESF | PSDF |
|---------------|---------------------|---------------------|------|------|
| Other | $R \leq 13$ | $R \leq 13$ | 0.06 | 1.90 |
| | $R \leq 13$ | $13 \leq R \leq 20$ | 0.08 | 2.51 |
| | $R \leq 13$ | $20 < R$ | 0.08 | 2.78 |
| | $13 \leq R \leq 20$ | $13 \leq R \leq 20$ | 0.03 | 1.35 |
| | $13 \leq R \leq 20$ | $20 < R$ | 0.06 | 1.60 |
| | $20 < R$ | $20 < R$ | 0.01 | 1.16 |

14.1.2.2 Deemed Energy and Demand Savings Tables

There are no deemed energy or demand savings tables for this measure. Please use algorithms and inputs as described above.

14.1.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years for cool roofs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID BldgEnv-CoolRoof.⁶²⁸

14.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- Total and treated roofing square footage (over conditioned space)
- Roof slope
- Existing roof insulation R-value, or year of building construction
- New roof insulation R-value, if adding insulation
- New roof initial and 3-year solar reflectance
- New roof rated life
- CRRC certificate or record matching roof product manufacturer, brand, and model
- Proof of purchase, including date of purchase, manufacturer, and model

⁶²⁸ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 14.1-5: [Cool Roofs] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision |

14.2 WINDOW TREATMENTS

14.2.1 Measure Description

This section presents the deemed savings methodology for the installation of window films and fixed solar screens. The installation of window treatments decreases the window-shading coefficient and reduces the solar heat transmitted to the building space. During months when perimeter cooling is required in the building, this measure decreases cooling energy use and peak demand.

14.2.1.1 Eligibility Criteria

This measure is applicable for treatment of single or double-paned clear glass windows without reflective or low-E coatings in south or west facing orientations (as specified in Table 14.2-1). The treatment can be a film applied to the window or a permanent, fixed interior or exterior solar screen. This methodology may be adapted for windows with existing shading devices on an individual project basis with prior evaluator approval of baseline solar heat gain coefficient (SHGC).

Existing windows must have no solar films/screens, interior shades, or exterior awnings or overhangs and must be installed in buildings that are mechanically cooled (DX or chilled water). While highly reflective louvered or Venetian blinds can help reduce solar heat gain, they must be completely lowered and closed to be as effective as permanent shading devices.⁶²⁹ The louvered or venetian blinds are not eligible for the measure, although windows with existing interior louvered or Venetian blinds are not excluded from using this measure.

14.2.1.2 Baseline Condition

The baseline condition is single- or double-pane clear glass, without existing window treatments. However, existing windows with interior louvered or Venetian blinds are an allowable baseline with reduced SHGC values from Table 14.2-2.

14.2.1.3 High-Efficiency Condition

The high-efficiency condition is an eligible window treatment applied to eligible windows.

⁶²⁹ "Energy Efficient Window Coverings," US Department of Energy. [https://www.energy.gov/energysaver/energy-efficient-window-coverings#:~:text=Window%20blinds%E2%80%94vertical%20\(Venetian%20blinds,while%20providing%20good%20daylight%20indoors.](https://www.energy.gov/energysaver/energy-efficient-window-coverings#:~:text=Window%20blinds%E2%80%94vertical%20(Venetian%20blinds,while%20providing%20good%20daylight%20indoors.)

14.2.2 Energy and Demand Savings Methodology

14.2.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

This savings methodology estimates reduction in solar heat gain/insolation attributable to a given window treatment using shading coefficients for the treated and untreated window and solar heat gain estimates by window orientation according to ASHRAE Fundamentals. The reduction in building energy use attributable to reduction in cooling system energy use is estimated based on the reduced heat removal requirement for a standard efficiency cooling system.

Energy and Demand Savings Algorithms

$$Energy\ Savings_o\ [\Delta kWh_o] = \frac{A_{film,o} \times SHG_o \times (SHGC_{pre,o} - SHGC_{post,o})}{3,412 \times COP}$$

Equation 14.2-1

$$Energy\ Savings\ [\Delta kWh] = \sum Energy\ Savings_o$$

Equation 14.2-2

$$Demand\ Savings_o\ [\Delta kW_o] = \frac{A_{film,o} \times SHGF_o \times (SHGC_{pre,o} - SHGC_{post,o})}{3,412 \times COP}$$

Equation 14.2-3

$$Demand\ Savings\ [\Delta kW] = Demand\ Savings_{o,max}$$

Equation 14.2-4

Where:

ΔkW_o = Peak demand savings per window orientation.

ΔkWh_o = Energy savings per window orientation.

$A_{film,o}$ = Area of window film/screens applied to orientation [ft²].

$SHGF_o$ = Peak solar heat gain factor for orientation of interest and peak type [Btu/hr-ft²-year]; see Table 14.2-1.

SHG_o = Solar heat gain for orientation of interest [Btu/ ft²-year]; see Table 14.2-1.

$SHGC_{pre}$ = Solar heat gain coefficient for existing glass with no interior-shading device; see Table 14.2-2.

$SHGC_{post}$ = Solar heat gain coefficient for new film/fixed-shading device, from manufacturer specifications.

Note: Shading coefficients (SC) have been retired, but if a product specification lists SC instead of SHGC, you can convert to SHGC by multiplying SC by 0.87.⁶³⁰

COP = Cooling equipment COP based on Table 14.2-3 or actual COP equipment, whichever is greater; if building construction year is unknown, assume IECC 2009 as applicable code.

3,412 = Constant to convert from Btu to kWh.

Table 14.2-1: [Window Treatments] Solar Heat Gain Factors⁶³¹

| Orientation | Solar Heat Gain {SHG} [Btu/ft ² -year] | Peak Hour Solar Heat Gain (SHGF) [Btu/hr-ft ² -year] | | |
|------------------|---|---|-----|-----|
| | | NCP | CP | 4CP |
| South-East | 158,844 | 36 | 29 | 24 |
| South-South-East | 134,794 | 38 | 30 | 24 |
| South | 120,839 | 57 | 34 | 37 |
| South-South-West | 134,794 | 127 | 76 | 94 |
| South-West | 158,844 | 181 | 139 | 162 |
| West-South-West | 169,696 | 210 | 181 | 204 |
| West | 163,006 | 219 | 195 | 216 |
| West-North-West | 139,615 | 208 | 181 | 195 |
| North-West | 107,161 | 176 | 140 | 145 |

Table 14.2-2: [Window Treatments] Recommended Clear Glass SHGC_{pre} by Window Type & Thickness⁶³²

| Window Type/Thickness | Louvered Blinds | SHGC |
|----------------------------------|-----------------|------|
| Single-pane 1/8-inch clear glass | No | 0.86 |
| Single-pane 1/4-inch clear glass | | 0.81 |
| Double-pane 1/8-inch clear glass | | 0.76 |
| Double-pane 1/4-inch clear glass | | 0.70 |

⁶³⁰ 2001 ASHRAE Handbook: Fundamentals, p. 30.39.

⁶³¹ Values are taken from the 1997 ASHRAE Fundamentals, Chapter 29 Table 17, based on the amount of solar radiation transmitted through single-pane clear glass for a cloudless day at 32°N Latitude for the 21st day of each month by hour of day and solar orientation. The SHG values listed above have been aggregated into daily totals for weekdays during the months of April through October.

⁶³² 2021 ASHRAE Handbook: Fundamentals, Chapter 15 Fenestration, Table 10 Solar Heat Gain Coefficient (SHGC).
<https://www.ashrae.org/technical-resources/ashrae-handbook/ashrae-handbook-online>.

| Window Type/Thickness | Louvered Blinds | SHGC |
|----------------------------------|--------------------|------|
| Single-pane 1/8-inch clear glass | Yes ⁶³³ | 0.64 |
| Single-pane 1/4-inch clear glass | | 0.60 |
| Double-pane 1/8-inch clear glass | | 0.61 |
| Double-pane 1/4-inch clear glass | | 0.57 |

Table 14.2-3: [Window Treatments] Recommended COP by HVAC System Type⁶³⁴

| Construction Year/ Applicable Code | AC/HP | PTAC/PTHP | Air Cooled Chiller | Water Cooled Chiller |
|---|-------|-----------|-----------------------|-------------------------|
| Before 2011; 2000 IECC | 2.9 | 2.9 | 2.5 | 4.2 |
| Between 2011-2016; 2009 IECC | 3.8 | 3.1 | 2.8 | 5.5 |
| After 2016; 2015 & 2018 IECC ⁶³⁵ | 3.8 | 3.1 | 2.8 | 5.5 |

14.2.2.2 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GlazDaylt-WinFilm.⁶³⁶

14.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Existing window type, thickness, and SHGC
- Description of existing window presence of exterior shading from other buildings or obstacles
- Window film or solar screen SHGC
- Eligible window treatment application area by orientation (e.g., S, SSW, SW...)
- Year of construction, if available
- Cooling equipment type

⁶³³ 2021 ASHRAE Handbook: Fundamentals, Chapter 15 Fenestration, Table 14A IAC Values for Louvered Shades: Uncoated Single Glazings, Table 14B IAC Values for Louvered Shades: Uncoated Double Glazings. <https://www.ashrae.org/technical-resources/ashrae-handbook/ashrae-handbook-online>.

⁶³⁴ Based on review of applicable codes, including IECC 2000, 2009, and 2015.

⁶³⁵ There were no changes in the associated commercial HVAC efficiency requirements between IECC 2015 and 2018.

⁶³⁶ DEER READI (Remote Ex-Ante Database Interface). <http://www.deerresources.com/index.php/readi>.

- Cooling equipment rated efficiency

Document Revision History

Table 14.2-4: [Window Treatments] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Extended eligibility to windows with existing louvered or Venetian blinds. Added reduced baseline SHGC values for windows with louvered blinds. |
| FY 2026 | Updated measure to indicate solar screen must be permanent, fixed and interior or exterior. |

14.3 ENTRANCE AND EXIT DOOR AIR INFILTRATION

14.3.1 Measure Description

This measure applies to the installation of weather stripping or door sweeps on entrance and exit doors for a contained, pressurized space. Entrance and exit doors often leave clearance gaps to allow for proper operation. The gaps around the doors allow for the infiltration of unconditioned air into the building, adding to the cooling and heating load of the HVAC system. Weather stripping and door sweeps are designed to be installed along the bottom and jambs of exterior doors to prevent air infiltration to conditioned space.

14.3.1.1 Eligibility Criteria

Weather stripping or doors sweeps must be installed on doors of a conditioned and/or heated space. Treated doors must have visible gaps of at least 1/8 – 3/4 inches along the outside edge of the door. Spaces with interior vestibule doors are not eligible.

14.3.1.2 Baseline Condition

The baseline standard for this measure is a commercial building with exterior doors that are not sealed from unconditioned space.

14.3.1.3 High-Efficiency Condition

The high-efficiency condition for this measure is a commercial building with exterior doors that have been sealed from unconditioned space using weather stripping and/or brush style door sweeps.

14.3.2 Energy and Demand Savings Methodology

14.3.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

This savings methodology was derived by analyzing TMY3 weather data for San Antonio.

Derivation of Pre-Retrofit Air Infiltration Rate

The pre-retrofit air infiltration rate for each crack width is calculated by applying the methodologies presented in Chapter 5 of the ASHRAE Cooling and Heating Load Calculation Manual (CHLCM).⁶³⁷ Building type characteristics for a typical commercial building were found in the DOE study PNNL-

⁶³⁷ ASHRAE Cooling and Heating Load Calculation Manual, p. 5.8. 1980. https://www.hud.gov/sites/documents/DOC_10603.PDF.

20026,⁶³⁸ and an average building height of 20 feet is assumed for the deemed savings approach.

Because air infiltration is a function of the differential pressure due to stack effect, wind speed, velocity head, and the design conditions of the building, TMY3 for San Antonio was applied to account for the varying weather conditions that are characteristic throughout an average year.

Figure 5.13 from the ASHRAE CHLCM provides the infiltration rate based on various crack width and the corresponding pressure difference across a door. Figures 5.1 and 5.2 (CHLCM) provide the differential pressure due to stack and wind pressure necessary to determine the total pressure difference across the door.

Applying a regression analysis to Figure 5.1 returns an equation which allows solving for the pressure difference due to stack effect, Δp_s . The aggregate curve fit for Figure 5.1 is shown below where x is based on the dry bulb temperature from the TMY3 data, and the design temperature is based on the appropriate seasonal condition.

$$\frac{\Delta p_s}{C_d} = 0.0000334003x - 0.00014468$$

Equation 14.3-1

Where C_d is an assumed constant, 0.63, and the neutral pressure distance is 10 feet.

From Figure 5.2, $\Delta p_w/C_p$ is determined by applying a polynomial regression, which returns an equation for solving for the pressure difference due to wind, Δp_w . The curve fit for Figure 5.2 is shown below where x is the wind velocity based on TMY3 data.

$$\Delta p_w/C_p = 0.00047749x^2 - 0.00013041x$$

Equation 14.3-2

Where C_p is an assumed constant, 0.13 (average wind pressure coefficient from Table 5.5 from CHLCM).

This yields the total pressure difference across the door, Δp_{Total} .

$$\Delta p_{Total} = \Delta p_s + \Delta p_w$$

Equation 14.3-3

Solving for Δp_{Total} allows for the air infiltration rate per linear foot to be determined in Figure 5.13 (CHLCM). Applying a power regression analysis for each crack width (described in inches) represented in Figure 5.13 returns the equations listed below. In these equations, Q is the infiltration rate in cubic feet per minute through cracks around the door and P is the perimeter of the door in feet.

⁶³⁸ Cho, H., K. Gowri, & B. Liu, "Energy Saving Impact of ASHRAE 90.1 Vestibule Requirements: Modeling of Air Infiltration through Door Openings." November 2010. https://www.pnnl.gov/main/publications/external/technical_reports/PNNL-20026.pdf.

$$Q/P_{1/8"} = 41.572x^{0.5120}$$

Equation 14.3-4

$$Q/P_{1/4"} = 81.913x^{0.5063}$$

Equation 14.3-5

$$Q/P_{1/2"} = 164.26x^{0.5086}$$

Equation 14.3-6

$$Q/P_{3/4"} = 246.58x^{0.5086}$$

Equation 14.3-7

These infiltration rates were further disaggregated based on TMY3 average monthly day and night conditions.

Derivation of Design and Average Outside Ambient Temperatures

Taking average daytime and nighttime outdoor temperature values, standard set points and setbacks for daytime and nighttime design cooling and heating will yield the temperature difference needed for the sensible heat equation:

$$\Delta T = T_{design} - T_{ambient,avg}$$

Equation 14.3-8

Where:

T_{design} = Daytime and nighttime design temperature [°F]; see Table 14.3-2.

$T_{ambient,avg}$ = Average outside ambient temperature, specified by month [°F]; see Table 14.3-1.

Table 14.3-1: [Door Infiltration] Average Monthly Ambient Temperatures (°F)⁶³⁹

| Month | Day ⁶⁴⁰ | Night ⁶⁴¹ |
|-------|--------------------|----------------------|
| Jan | 53.4 | 45.4 |
| Feb | 63.6 | 52.8 |
| Mar | 63.6 | 53.0 |
| April | 76.6 | 63.4 |
| May | 86.1 | 75.2 |
| June | 89.7 | 78.3 |

⁶³⁹ TMY3 climate data.

⁶⁴⁰ Day hours are defined as 7 AM-7PM.

⁶⁴¹ Night hours are defined as 8PM-6AM.

| Month | Day ⁶⁴⁰ | Night ⁶⁴¹ |
|-------|--------------------|----------------------|
| July | 87.5 | 77.7 |
| Aug | 88.1 | 77.2 |
| Sept | 86.3 | 74.0 |
| Oct | 76.0 | 63.9 |
| Nov | 72.5 | 60.0 |
| Dec | 61.8 | 50.1 |

Table 14.3-2: [Door Infiltration] Daytime and Nighttime Design Temperatures

| Temperature Description | T _{design} (°F) |
|---|--------------------------|
| Daytime Cooling Design Temperature | 74 |
| Daytime Heating Design Temperature | 72 |
| Nighttime Cooling Design Temperature ⁶⁴² | 78 |
| Nighttime Heating Design Temperature ⁶⁴³ | 68 |
| Daytime Cooling Design Temperature | 74 |

To calculate HVAC load associated with air infiltration, the following sensible heat equations are used:

$$Energy\ Savings\ [\Delta kWh] = kWh_{C,Day} + kWh_{C,Night} + kWh_{H,Day} + kWh_{H,Night}$$

Equation 14.3-9

$$kWh_{C,Day} = \frac{CFM_{pre,day} \times CFM_{reduction} \times 1.08 \times \Delta T \times 1.0 \frac{kW}{ton} \times Hours_{day}}{12,000}$$

Equation 14.3-10

$$kWh_{C,Night} = \frac{CFM_{pre,night} \times CFM_{reduction} \times 1.08 \times \Delta T \times 1.0 \frac{kW}{ton} \times Hours_{night}}{12,000}$$

Equation 14.3-11

$$kWh_{H,Day} = \frac{CFM_{pre,day} \times CFM_{reduction} \times 1.08 \times \Delta T \times 1.0 \frac{kW}{ton} \times Hours_{day}}{COP \times 3,412}$$

Equation 14.3-12

⁶⁴² Assuming 4-degree setback.

⁶⁴³ Ibid.

$$kWh_{H,Night} = \frac{CFM_{pre,night} \times CFM_{reduction} \times 1.08 \times \Delta T \times 1.0 \frac{kW}{ton} \times Hours_{night}}{COP \times 3,412}$$

Equation 14.3-13

Demand savings can be derived by using the following.⁶⁴⁴

$$Demand\ Savings\ [\Delta kW] = \frac{CFM_{pre,day} \times CFM_{reduction} \times 1.08 \times \Delta T \times 1.0 \frac{kW}{ton}}{12,000}$$

Equation 14.3-14

Where:

| | | |
|-------------------|---|---|
| CFM_{pre} | = | Calculated pre-retrofit air infiltration [cfm]. |
| $CFM_{reduction}$ | = | 59% ⁶⁴⁵ × TDF. |
| TDF | = | Technical degradation factor = 85%. ⁶⁴⁶ |
| 1.08 | = | Sensible heat equation conversion. ⁶⁴⁷ |
| ΔT | = | Change in temperature across gap barrier [°F]. |
| $Hours_{day}$ | = | 12-hour cycles per day, per month = 4,380 hours. |
| $Hours_{night}$ | = | 12-hour cycles per night, per month = 4,380 hours. |
| COP | = | Heating coefficient of performance; 1.0 for electric resistance and 3.3 for heat pumps. |
| 1.0 | = | Constant to convert from kW to tons. |
| 12,000 | = | Constant to convert from Btuh to tons. |
| 3,412 | = | Constant to convert from Btu to kWh. |

14.3.2.2 Deemed Energy and Demand Savings Tables

Deemed energy and demand savings per standard door⁶⁴⁸ are specified below based on existing door gap width (inches). The gap width shall be measured on each of the four edges of the door to the nearest ¼ inch. The reported gap width for the door should reflect the average of the four measurements. The average gap width should be rounded to the nearest deemed gap width in inches. Projects that

⁶⁴⁴ CP demand savings are calculated by weighting demand savings for the top 20 peak hours. 4CP demand savings are calculated by averaging the demand savings calculated for the 4CP months. NCP demand savings are calculated by taking the maximum CP value from the top 20 hours.

⁶⁴⁵ CLEARresult, "Commercial Door Air Infiltration Memo." March 18, 2015. Average reduction in Arkansas based on test results from the CLEARresult Brush Weather Stripping Testing Method & Results (59% infiltration reduction).

⁶⁴⁶ This factor is applied to account for the difference between the laboratory test from the "Commercial Door Air Infiltration Memo" and the real-world ability to seal the openings around a door. In the absence of research regarding the actual difference, this factor was set to 0.85.

⁶⁴⁷ 2013 ASHRAE Handbook of Fundamentals; Equation 33, p. 16.11.

⁶⁴⁸ Standard door circumference calculated as (36" width + 80" height) ÷ 12 in/ft × 2 = 19.3 linear ft.

have more than 10 doors at the same project site, can provide a sample of measurements of 20 percent of the claimed doors and apply the average to all door in the project. Heating savings are specified for both electric resistance (ER) and heat pump (HP) heating. Cooling savings are available for buildings with electric cooling and gas heat, but no heating savings should be claimed for buildings with gas heat.

Table 14.3-3: [Door Infiltration] Deemed Energy Savings per Door of Weather Stripping/Door Sweep

| Savings Type | Gap Width (inches) | | | |
|--------------|--------------------|----------|----------|----------|
| | 1/8 | 1/4 | 1/2 | 3/4 |
| Cooling | 79.46 | 160.66 | 318.81 | 478.50 |
| ER Heating | 525.29 | 1,062.37 | 2,107.91 | 3,164.48 |
| HP Heating | 159.11 | 321.90 | 638.77 | 958.93 |

Table 14.3-4: [Door Infiltration] Deemed Demand Savings per Door of Weather Stripping/Door Sweep

| Peak Type | Gap Width (inches) | | | |
|-----------|--------------------|-------|-------|-------|
| | 1/8 | 1/4 | 1/2 | 3/4 |
| NCP | 0.143 | 0.288 | 0.574 | 0.860 |
| CP | 0.099 | 0.199 | 0.394 | 0.592 |
| 4CP | 0.064 | 0.130 | 0.257 | 0.387 |

14.3.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 11 years, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID BS-Wthr.⁶⁴⁹ This measure life is consistent with residential air infiltration measure in the Guidebook.

⁶⁴⁹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

14.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Treated door quantity
- Existing gap width on each of edge of the door
- Reported average gap width (1/8", 1/4", 1/2", 3/4")
- Existing weatherization measure (full, partial, none)
- New weatherization measure (weather stripping or door sweep)
-
- Cooling type (central refrigerated cooling, room air conditioning, none)
- Heating type (central gas, portable gas, central electric resistance, portable electric resistance, heat pump, none)
 - Additional documentation is required to validate electric resistance heat (e.g., nameplate photo, utility inspection, or other evaluator-approved approach);

Document Revision History

Table 14.3-5: [Door Infiltration] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | No revision. |
| FY 2026 | Adjusted savings normalization from per linear foot to per standard door. Updated documentation requirements. |

15. COMMERCIAL: FOOD SERVICE EQUIPMENT

15.1 ENERGY STAR® COMBINATION OVENS

15.1.1 Measure Description

This section covers the deemed savings methodology for the installation of ENERGY STAR combination ovens. Combination ovens are convection ovens that include the added capability to inject steam into the oven cavity and typically offers at least three distinct cooking modes; combination mode to roast or bake with moist heat, convection mode to operate purely as a convection oven providing dry heat, or a straight pressure-less steamer mode. The energy and demand savings are determined on a per-oven basis.

15.1.1.1 Eligibility Criteria

Eligible units must be compliant with the current ENERGY STAR qualifications, with half-size and full-size ovens as defined below and a pan capacity ≥ 3 and ≤ 40 .^{650,651}

- Full-Size Combination Oven: A combination oven capable of accommodating two 12.7 x 20.8 x 2.5-inch steam table pans per rack position, loaded from front-to-back or lengthwise.
- Half-Size Combination Oven: A combination oven capable of accommodating a single 12.7 x 20.8 x 2.5-inch steam table pan per rack position, loaded from front-to-back or lengthwise.
- Two-thirds-size combination ovens were added to the current ENERGY STAR specification but are excluded from this measure until the ENERGY STAR food service calculator is updated to include category-specific input assumptions.

Eligible building types include any non-residential application.

The following products are excluded from the ENERGY STAR eligibility criteria:

- Dual-fuel heat source combination ovens
- Hybrid ovens not defined as eligible above (e.g., those incorporating microwave settings)
- Conventional or standard ovens, conveyor, slow cook-and-hold, desk, hearth, microwave, range, rapid cook, reel-type, and rotisserie
- Full- and half-size gas combination ovens with a pan capacity of < 5 or > 40
- Full- and half-size electric combination ovens with a pan capacity of < 3 or > 40

⁶⁵⁰ ENERGY STAR Program Requirements for Commercial Ovens. Eligibility Criteria Version 3.0.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.0%20Commercial%20Ovens%20Final%20Specification_0.pdf

⁶⁵¹ ENERGY STAR Qualified Product Listing: <https://www.energystar.gov/productfinder/product/certified-commercial-ovens/results>.

- Two-thirds-size combination ovens with a pan capacity of > 5
- Mini and quadruple gas rack ovens
- Electric rack ovens

15.1.1.2 Baseline Condition

The baseline condition for retrofit situations is a half-size or full-size combination oven with a pan capacity ≥ 5 and ≤ 20 that does not meet ENERGY STAR key product criteria.

15.1.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v3.0 specification, effective January 12, 2023. Qualified products must meet the minimum energy efficiency and idle energy rate requirements from Table 15.1-1. Furthermore, Pan Capacity⁶⁵² must be ≥ 5 and ≤ 20 for both half and full-size combination ovens.

Table 15.1-1: [Combination Ovens] ENERGY STAR Specification⁶⁵³

| Operation | Idle Rate (kW) ⁶⁵⁴ | Cooking Energy Efficiency (%) |
|---|-------------------------------|-------------------------------|
| Full-size and half-size ovens with 5-40 pan capacity | | |
| Steam mode | $\leq 0.133P + 0.64$ | ≥ 55 |
| Convection mode | $\leq 0.083P + 0.35$ | ≥ 78 |
| Full-size and half-size ovens with 3-4 pan capacity | | |
| Steam mode | $\leq 0.60P$ | ≥ 51 |
| Convection mode | $\leq 0.05P + 0.55$ | ≥ 70 |

Furthermore, pan capacity⁶⁵⁵ must be ≥ 3 and ≤ 40 (for both half- and full-size combination ovens). Pan capacity must be ≥ 3 and ≤ 5 for two-thirds-size combination ovens.

⁶⁵² Pan Capacity is defined as the number of steam table pans the combination oven is designed to accommodate as per the ASTM F-1495-05 standard specification.

⁶⁵³ ENERGY STAR Commercial Ovens Key Product Criteria.

https://www.energystar.gov/products/commercial_food_service_equipment/commercial_ovens/key_product_criteria.

⁶⁵⁴ P = Pan Capacity.

⁶⁵⁵ Pan capacity is defined as the number of steam table pans the combination oven can accommodate as per the ASTM F-1495-05 standard specification.

15.1.2 Energy and Demand Savings Methodology

15.1.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

Deemed savings are calculated using the following algorithms:

$$\text{Energy Savings } [\Delta kWh] = kWh_{base} - kWh_{ES}$$

Equation 15.1-1

$$kWh_{base} = kWh_{ph,base} + kWh_{conv,base} + kWh_{st,base}$$

Equation 15.1-2

$$kWh_{ES} = kWh_{ph,ES} + kWh_{conv,ES} + kWh_{st,ES}$$

Equation 15.1-3

kWh_{ph} , kWh_{conv} and kWh_{st} are each calculated the same for both the baseline and ENERGY STAR cases, as shown below, except they require their respective input assumptions relative to convection and steam modes as seen in Table 15.1-2.

$$kWh = \left(E_{ph} + \left(\frac{W_{food} \times DOH \times E_{food} \times 50\%}{\eta_{cook}} \right) + E_{idle} \times \left(\left(DOH - \frac{W_{food} \times DOH}{PC} \right) \times 50\% \right) \right) \times \frac{AOD}{1,000}$$

Equation 15.1-4

$$\text{Demand Savings } [\Delta kW] = \frac{\Delta kWh - \left(\frac{\Delta E_{ph} \times AOD}{1,000} \right)}{DOH \times AOD} \times DF$$

Equation 15.1-5

Where:

kWh_{base} = Baseline annual energy consumption [kWh].

kWh_{ES} = ENERGY STAR annual energy consumption [kWh].

E_{ph} = Preheat energy [Wh].

ΔE_{ph} = Difference in baseline and ENERGY STAR preheat energy [Wh/BTU].

E_{food} = ASTM energy to food of energy absorbed by food product during cooking [Wh/lb].

E_{idle} = Idle energy rate [W].

W_{food} = Pounds of food cooked per hour [lb/hr].

η_{cook} = Cooking energy efficiency [%].

| | | |
|--------------|---|--|
| <i>PC</i> | = | <i>Production capacity per pan [lb/hr].</i> |
| <i>DOH</i> | = | <i>Equipment daily operating hours [hr/day].</i> |
| <i>AOD</i> | = | <i>Facility annual operating days [days/year].</i> |
| <i>1,000</i> | = | <i>Constant to convert from watts to kilowatts.</i> |
| <i>DF</i> | = | <i>Demand Factor for NCP, CP, or 4CP peak demand; see Table 15.1-3: Combination Ovens-Operating Schedule Assumptions</i> |

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and University | 10 | 260 |
| All other | 12 | 365 |

Table 15.1-.

Table 15.1-2: [Combination Ovens] ENERGY STAR Commercial Food Service Calculator Inputs⁶⁵⁶

| Variable | | Convection-Mode | | Steam-Mode | |
|---------------|-----------------|-----------------|--------------------------------|------------|----------------------------------|
| | | Baseline | ENERGY STAR | Baseline | ENERGY STAR |
| E_{ph} | $P < 5$ | 410 | | 600 | |
| | $5 \geq P < 15$ | 3,000 | 1,500 | 3,000 | 1,500 |
| | $P \geq 15$ | 3,750 | 2,000 | 3,750 | 2,000 |
| W_{food} | $P < 5$ | 10.4 | | | |
| | $5 \geq P < 15$ | 16.7 | | | |
| | $P \geq 15$ | 20.8 | | | |
| E_{food} | | 73.2 | | 30.8 | |
| η_{cook} | $3 \geq P < 5$ | 65% | 70% | 47% | 51% |
| | $P \geq 5$ | 72% | 78% | 52% | 55% |
| E_{idle} | $3 \geq P < 5$ | 680 | $(0.05P + 0.55) \times 1,000$ | 2,090 | $0.60P \times 1,000$ |
| | $5 \geq P < 15$ | 1,320 | $(0.083P + 0.35) \times 1,000$ | 5,260 | $(0.133P + 0.6400) \times 1,000$ |
| | $P \geq 15$ | 2,280 | | 8,710 | |
| PC | $P < 5$ | 29 | 37 | 45 | 59 |

⁶⁵⁶ ENERGY STAR Commercial Food Service Equipment Calculator. 7/15/21 amendment to March 2021 update.
https://www.energystar.gov/products/commercial_food_service_equipment.

| Variable | | Convection-Mode | | Steam-Mode | |
|----------|------------|-----------------|-------------|------------|-------------|
| | | Baseline | ENERGY STAR | Baseline | ENERGY STAR |
| | $P \geq 5$ | 107 | 174 | 151 | 247 |

Table 15.1-3: Combination Ovens-Operating Schedule Assumptions⁶⁵⁷

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and University | 10 | 260 |
| All other | 12 | 365 |

Table 15.1-4: [Combination Ovens] Demand Factors⁶⁵⁸

| Peak Type | DF |
|-----------|-----|
| NCP | 1.0 |
| CP | 0.9 |
| 4CP | 0.9 |

15.1.2.2 Deemed Energy Savings Tables

Deemed energy and demand savings are based on the input assumptions from Table 15.1-2 and Table 15.1-3: Combination Ovens-Operating Schedule Assumptions

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and University | 10 | 260 |
| All other | 12 | 365 |

Table 15.1-.

⁶⁵⁷ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

⁶⁵⁸ Itron, Inc., "2004-2005 Database for Energy Efficiency Resources (DEER) Update Study: Final Report." Prepared for Southern California Edison. December 2005. Table 3-14, p. 3-17.

Table 15.1-5: [Combination Ovens] Deemed Energy Savings (Education: K-12)⁶⁵⁹

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|------------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 3 | 104 | 0.096 | 0.0863 | 0.0863 |
| 4 ⁶⁶⁰ | 104 | 0.096 | 0.0863 | 0.0863 |
| 5 | 2,740 | 2.037 | 1.833 | 1.833 |
| 6 | 2,632 | 1.937 | 1.743 | 1.743 |
| 7 | 2,524 | 1.837 | 1.654 | 1.654 |
| 8 | 2,417 | 1.738 | 1.5641 | 1.564 |
| 9 | 2,309 | 1.638 | 1.475 | 1.475 |
| 10 | 2,202 | 1.539 | 1.385 | 1.385 |
| 11 | 2,094 | 1.439 | 1.295 | 1.295 |
| 12 | 1,987 | 1.340 | 1.206 | 1.206 |
| 13 | 1,879 | 1.240 | 1.116 | 1.116 |
| 14 | 1,772 | 1.141 | 1.0273 | 1.0273 |
| 15 | 3,742 | 2.881 | 2.593 | 2.593 |
| 16 | 3,637 | 2.784 | 2.505 | 2.505 |
| 17 | 3,531 | 2.686 | 2.418 | 2.418 |
| 18 | 3,426 | 2.589 | 2.330 | 2.330 |
| 19 | 3,321 | 2.492 | 2.242 | 2.242 |
| 20 | 3,216 | 2.394 | 2.155 | 2.155 |
| 21 | 3,111 | 2.297 | 2.067 | 2.067 |
| 22 | 3,005 | 2.199 | 1.979 | 1.979 |
| 23 | 2,900 | 2.102 | 1.892 | 1.892 |
| 24 | 2,795 | 2.004 | 1.804 | 1.804 |
| 25 | 2,690 | 1.907 | 1.716 | 1.716 |
| 26 | 2,584 | 1.810 | 1.629 | 1.629 |
| 27 | 2,479 | 1.712 | 1.541 | 1.541 |
| 28 | 2,374 | 1.615 | 1.453 | 1.453 |
| 29 | 2,269 | 1.517 | 1.366 | 1.366 |
| 30 | 2,164 | 1.420 | 1.278 | 1.278 |

⁶⁶⁰ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|--------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 31 | 2,058 | 1.323 | 1.190 | 1.190 |
| 32 | 1,953 | 1.225 | 1.103 | 1.103 |
| 33 | 1,848 | 1.128 | 1.015 | 1.015 |
| 34 | 1,743 | 1.030 | 0.927 | 0.927 |
| 35 | 1,637 | 0.933 | 0.840 | 0.840 |
| 36 | 1,532 | 0.835 | 0.752 | 0.752 |
| 37 | 1,427 | 0.738 | 0.664 | 0.664 |
| 38 | 1,322 | 0.641 | 0.577 | 0.577 |
| 39 | 1,217 | 0.543 | 0.489 | 0.489 |
| 40 | 1,111 | 0.446 | 0.401 | 0.401 |

Table 15.1-6: [Combination Ovens] Deemed Energy Savings (Education: College and University)

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|------------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 3 | 249 | 0.096 | 0.086 | 0.086 |
| 4 ⁶⁶¹ | 249 | 0.096 | 0.086 | 0.086 |
| 5 | 6,075 | 2.037 | 1.833 | 1.833 |
| 6 | 5,816 | 1.937 | 1.743 | 1.743 |
| 7 | 5,557 | 1.837 | 1.654 | 1.654 |
| 8 | 5,299 | 1.738 | 1.564 | 1.564 |
| 9 | 5,040 | 1.638 | 1.475 | 1.475 |
| 10 | 4,781 | 1.539 | 1.385 | 1.385 |
| 11 | 4,522 | 1.439 | 1.295 | 1.295 |
| 12 | 4,264 | 1.340 | 1.206 | 1.206 |
| 13 | 4,005 | 1.240 | 1.116 | 1.116 |
| 14 | 3,746 | 1.141 | 1.027 | 1.027 |
| 15 | 8,401 | 2.881 | 2.593 | 2.593 |
| 16 | 8,148 | 2.784 | 2.505 | 2.505 |
| 17 | 7,895 | 2.686 | 2.418 | 2.418 |
| 18 | 7,641 | 2.589 | 2.330 | 2.330 |

⁶⁶¹ Four pan capacity savings are set as identical to three pan capacity savings, as ENERGY STAR calculator reports negative savings.

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|--------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 19 | 7,388 | 2.492 | 2.242 | 2.242 |
| 20 | 7,135 | 2.394 | 2.155 | 2.155 |
| 21 | 6,882 | 2.297 | 2.067 | 2.067 |
| 22 | 6,628 | 2.199 | 1.979 | 1.979 |
| 23 | 6,375 | 2.102 | 1.892 | 1.892 |
| 24 | 6,122 | 2.004 | 1.804 | 1.804 |
| 25 | 5,868 | 1.907 | 1.716 | 1.716 |
| 26 | 5,615 | 1.810 | 1.629 | 1.629 |
| 27 | 5,362 | 1.712 | 1.541 | 1.541 |
| 28 | 5,108 | 1.615 | 1.453 | 1.453 |
| 29 | 4,855 | 1.517 | 1.366 | 1.366 |
| 30 | 4,602 | 1.420 | 1.278 | 1.278 |
| 31 | 4,349 | 1.323 | 1.190 | 1.190 |
| 32 | 4,095 | 1.225 | 1.103 | 1.103 |
| 33 | 3,842 | 1.128 | 1.015 | 1.015 |
| 34 | 3,589 | 1.030 | 0.927 | 0.927 |
| 35 | 3,335 | 0.933 | 0.840 | 0.840 |
| 36 | 3,082 | 0.835 | 0.752 | 0.752 |
| 37 | 2,829 | 0.738 | 0.664 | 0.664 |
| 38 | 2,576 | 0.641 | 0.577 | 0.577 |
| 39 | 2,322 | 0.543 | 0.489 | 0.489 |
| 40 | 2,069 | 0.446 | 0.401 | 0.401 |

Table 15.1-7: [Combination Ovens] Deemed Energy Savings (All Other)

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|------------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 3 | 420 | 0.096 | 0.086 | 0.086 |
| 4 ⁶⁶² | 420 | 0.096 | 0.086 | 0.086 |
| 5 | 10,015 | 2.037 | 1.833 | 1.833 |
| 6 | 9,579 | 1.937 | 1.743 | 1.743 |

⁶⁶² Four pan capacity savings are set as identical to three pan capacity savings, as ENERGY STAR calculator reports negative savings.

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|--------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 7 | 9,143 | 1.837 | 1.654 | 1.654 |
| 8 | 8,707 | 1.738 | 1.564 | 1.564 |
| 9 | 8,271 | 1.638 | 1.475 | 1.475 |
| 10 | 7,835 | 1.539 | 1.385 | 1.385 |
| 11 | 7,399 | 1.439 | 1.295 | 1.295 |
| 12 | 6,963 | 1.340 | 1.206 | 1.206 |
| 13 | 6,527 | 1.240 | 1.116 | 1.116 |
| 14 | 6,091 | 1.141 | 1.027 | 1.027 |
| 15 | 13,898 | 2.881 | 2.593 | 2.593 |
| 16 | 13,471 | 2.784 | 2.505 | 2.505 |
| 17 | 13,044 | 2.686 | 2.418 | 2.418 |
| 18 | 12,617 | 2.589 | 2.330 | 2.330 |
| 19 | 12,191 | 2.492 | 2.242 | 2.242 |
| 20 | 11,764 | 2.394 | 2.155 | 2.155 |
| 21 | 11,337 | 2.297 | 2.067 | 2.067 |
| 22 | 10,911 | 2.199 | 1.979 | 1.979 |
| 23 | 10,484 | 2.102 | 1.892 | 1.892 |
| 24 | 10,057 | 2.004 | 1.804 | 1.804 |
| 25 | 9,630 | 1.907 | 1.716 | 1.716 |
| 26 | 9,204 | 1.810 | 1.629 | 1.629 |
| 27 | 8,777 | 1.712 | 1.541 | 1.541 |
| 28 | 8,350 | 1.615 | 1.453 | 1.453 |
| 29 | 7,924 | 1.517 | 1.366 | 1.366 |
| 30 | 7,497 | 1.420 | 1.278 | 1.278 |
| 31 | 7,070 | 1.323 | 1.190 | 1.190 |
| 32 | 6,644 | 1.225 | 1.103 | 1.103 |
| 33 | 6,217 | 1.128 | 1.015 | 1.015 |
| 34 | 5,790 | 1.030 | 0.927 | 0.927 |
| 35 | 5,363 | 0.933 | 0.840 | 0.840 |
| 36 | 4,937 | 0.835 | 0.752 | 0.752 |
| 37 | 4,510 | 0.738 | 0.664 | 0.664 |

| Pan Capacity | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|--------------|-----------------------------|-------------------------|------------------------|-------------------------|
| 38 | 4,083 | 0.641 | 0.577 | 0.577 |
| 39 | 3,657 | 0.543 | 0.489 | 0.489 |
| 40 | 3,230 | 0.446 | 0.401 | 0.401 |

15.1.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for combination ovens, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID Cook-ElecCombOven.⁶⁶³

15.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Pan capacity
- ENERGY STAR idle rate
- ENERGY STAR cooking efficiency
- ENERGY STAR certification or alternative
- Proof of purchase including date of purchase, manufacturer, and model number
- Facility type (Education: K-12, Education: College and university, All other)

Document Revision History

Table 15.1-3: [Combination Ovens] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Specified reduced operating schedule for education applications. Aligned deemed savings tables and calculations input assumptions to ENERGY STAR March 2024 update |

⁶⁶³ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

15.2 ENERGY STAR® ELECTRIC CONVECTION OVENS

15.2.1 Measure Description

This section covers the savings from retrofit or new installation of full-size or half-size ENERGY STAR electric convection ovens. Convection ovens cook food by forcing hot dry air over the surface of the food product. The rapidly moving hot air strips away the layer of cooler air next to the food and enables the food to absorb the heat energy. The energy and demand savings are deemed, and based on oven energy rates, cooking efficiencies, operating hours, production capacities and building type. The energy and demand savings are determined on a per-oven basis.

15.2.1.1 Eligibility Criteria

Eligible units must be compliant with the current ENERGY STAR specification, with half-size and full-size electric ovens as defined below.^{664,665}

- Full-Size Convection Oven: A combination oven capable of accommodating standard full-size sheet pans measuring 18 x 26 x 1-inch
- Half-Size Convection Oven: A convection oven capable of accommodating half-size sheet pans measuring 18 x 13 x 1-inch

Eligible building types include any non-residential application.⁶⁶⁶

Convection ovens eligible for rebate do not include ovens that can heat the cooking cavity with saturated or superheated steam. However, eligible convection ovens may have moisture injection capabilities (e.g., baking ovens and moisture-assist ovens). Ovens that include a “hold feature” are eligible under this specification if convection is the only method used to fully cook the food.

The following products are excluded from the ENERGY STAR eligibility criteria:

- Half-size gas convection ovens
- Hybrid ovens not defined as eligible above (e.g., those incorporating microwave settings)
- Conventional or standard ovens, conveyor, slow cook-and-hold, deck, hearth, microwave, range, rapid cook, reel-type, and rotisserie
- Mini and quadruple gas rack ovens
- Electric rack ovens

⁶⁶⁴ ENERGY STAR Program Requirements for Commercial Ovens. Eligibility Criteria Version 3.0.

https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.0%20Commercial%20Ovens%20Final%20Specification_0.pdf

⁶⁶⁵ ENERGY STAR Qualified Product Listing: <https://www.energystar.gov/productfinder/product/certified-commercial-ovens/results>.

⁶⁶⁶ CEE Commercial Kitchens Initiative’s overview of the Food Service Industry:

https://library.cee1.org/system/files/library/4203/CEE_CommKit_InitiativeDescription_Mar2021.pdf.

15.2.1.2 Baseline Condition

The baseline condition for retrofit situations is an electric convection oven that does not meet ENERGY STAR key product criteria.

15.2.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v3.0 specification, effective January 12, 2023. Qualified equipment must meet the minimum energy efficiency and idle energy rate requirements from Table 15.2-1:

Table 15.2-1: [Convection Ovens] ENERGY STAR Specification⁶⁶⁷

| Oven Size | Idle Rate (W) | Cooking Energy Efficiency (%) |
|--------------------|---------------|-------------------------------|
| Full-size ≥ 5 pans | ≤ 1,400 | ≥ 76 |
| Full-size < 5 pans | ≤ 1,000 | |
| Half-size | | ≥ 71 |

15.2.2 Energy and Demand Savings Methodology

15.2.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{base} - kWh_{ES}$$

Equation 15.2-1

$$kWh_{base} = kWh_{ph,base} + kWh_{conv,base} + kWh_{st,base}$$

Equation 15.2-2

$$kWh_{ES} = kWh_{ph,ES} + kWh_{conv,ES} + kWh_{st,ES}$$

Equation 15.2-3

kWh_{ph}, kWh_{conv} and kWh_{st} are each calculated the same for both the baseline and ENERGY STAR cases, as shown below, except they require their respective input assumptions relative to preheat, cooking, and idle operation as seen in Table 15.2-2.

⁶⁶⁷ ENERGY STAR Commercial Ovens Key Product Criteria.

https://www.energystar.gov/products/commercial_food_service_equipment/commercial_ovens/key_product_criteria.

$$kWh = \left(E_{ph} + \left(\frac{W_{food} \times DOH \times E_{food} \times 50\%}{\eta_{cook}} \right) + E_{idle} \times \left(\left(DOH - \frac{W_{food} \times DOH}{PC} \right) \times 50\% \right) \right) \times \frac{AOD}{1,000}$$

Equation 15.2-4

$$Demand Savings [\Delta kW] = \frac{\Delta kWh - \left(\frac{\Delta E_{ph} \times AOD}{1,000} \right)}{DOH \times AOD} \times DF$$

Equation 15.2-5

Where:

| | | |
|-----------------|---|--|
| kWh_{base} | = | Baseline annual energy consumption [kWh]. |
| kWh_{ES} | = | ENERGY STAR annual energy consumption [kWh]. |
| E_{ph} | = | Preheat energy [Wh/BTU]. |
| ΔE_{ph} | = | Difference in baseline and ENERGY STAR preheat energy [Wh]. |
| E_{food} | = | ASTM energy to food of energy absorbed by food product during cooking [Wh/lb]. |
| E_{idle} | = | Idle energy rate [W]. |
| W_{food} | = | Pounds of food cooked per hour [lb/hr]. |
| η_{cook} | = | Cooking energy efficiency [%]. |
| PC | = | Production capacity per pan [lb/hr]. |
| DOH | = | Equipment daily operating hours [hr/day]. |
| AOD | = | Facility annual operating days [days/year]. |
| 1,000 | = | Constant to convert from watts to kilowatts. |

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 15.2-3: [Convection Ovens] Operating Schedule Assumptions

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 10 | 260 |
| All other | 12 | 365 |

Table 15.2-.

Table 15.2-2: [Convection Ovens] ENERGY STAR Commercial Food Service Calculator Inputs⁶⁶⁸

| Variable | Full-size ≥ 5 pans | | Full-size < 5 pans | | Half-size | |
|---------------|--------------------|-------------|--------------------|-------------|-----------|-------------|
| | Baseline | ENERGY STAR | Baseline | ENERGY STAR | Baseline | ENERGY STAR |
| E_{ph} | 1,563 | 1,389 | 1,563 | 1,389 | 890 | 700 |
| W_{food} | | | | | | 8.33 |
| E_{food} | | | | | | 73.2 |
| η_{cook} | 65% | 76% | 65% | 76% | 68% | 70.67% |
| E_{idle} | 2,000 | 1,400 | 2,000 | 1,000 | 1,030 | 1,000 |
| PC | 90 | 90 | 90 | 90 | 45 | 50 |

Table 15.2-3: [Convection Ovens] Operating Schedule Assumptions⁶⁶⁹

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 10 | 260 |
| All other | 12 | 365 |

Table 15.2-4: [Convection Ovens] Demand Factors⁶⁷⁰

| Peak Type | DF |
|-----------|-----|
| NCP | 1.0 |
| CP | 0.9 |
| 4CP | 0.9 |

15.2.2.2 Deemed Energy and Demand Savings Tables

Deemed energy and demand savings are based on the input assumptions from Table 15.2-2 and Table 15.2-3: [Convection Ovens] Operating Schedule Assumptions

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 10 | 260 |

⁶⁶⁸ ENERGY STAR Commercial Food Service Equipment Calculator. 7/15/21 amendment to March 2021 update.
https://www.energystar.gov/products/commercial_food_service_equipment.

⁶⁶⁹ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

⁶⁷⁰ Itron, Inc., "2004-2005 Database for Energy Efficiency Resources (DEER) Update Study: Final Report." Prepared for Southern California Edison. December 2005. Table 3-14, p. 3-17.

| Building Type | DOH | AOD |
|---------------|-----|-----|
| All other | 12 | 365 |

Table 15.2-.

Table 15.2-5: [Convection Ovens] Deemed Energy and Demand Savings

| Building Type | Oven Size | Annual Energy Savings [kWh] | NCP Peak Demand Savings [kW] | CP Peak Demand Savings [kW] | 4CP Peak Demand Savings [kW] |
|-----------------------------------|--------------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
| Education: K-12 | Full-size ≥ 5 pans | 766 | 0.6801 | 0.612 | 0.612 |
| | Full-size < 5 pans | 1,158 | 1.043 | 0.939 | 0.939 |
| Education: K-12 | Half-Size | 77 | 0.040 | 0.036 | 0.036 |
| Education: College and university | Full-size ≥ 5 pans | 1,814 | 0.680 | 0.612 | 0.612 |
| | Full-size < 5 pans | 2,758 | 1.043 | 0.939 | 0.939 |
| | Half-Size | 153 | 0.040 | 0.036 | 0.036 |
| All Other | Full-size ≥ 5 pans | 3,043 | 0.680 | 0.612 | 0.612 |
| | Full-size < 5 pans | 4,633 | 1.043 | 0.939 | 0.939 |
| | Half-Size | 244 | 0.040 | 0.036 | 0.036 |

15.2.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for electric convection ovens, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID Cook-ElecConvOven.⁶⁷¹

15.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Pan capacity
- Oven size
- ENERGY STAR idle rate

⁶⁷¹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

- ENERGY STAR cooking efficiency
- ENERGY STAR certification or alternative
- Proof of purchase including date of purchase, manufacturer, and model number
- Facility type (Education: K-12, Education: College and university, All other)

Document Revision History

Table 15.2-3: [Convection Ovens] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | No revision. |
| FY 2026 | Specified reduced operating schedule for education applications and updated corresponding deemed savings tables |

15.3 ENERGY STAR® DISHWASHERS

15.3.1 Measure Description

This section covers the deemed savings methodology for the installation of ENERGY STAR commercial dishwashers. On average, commercial dishwashers that have earned ENERGY STAR certification are 25% more energy-efficient and 25% more water-efficient than standard models. The energy savings associated with ENERGY STAR commercial dishwashers are primarily due to reduced water use and reduced need to heat water. A commercial kitchen may have external booster water heaters or booster water heaters may be internal to specific equipment. Both primary and booster water heaters may be either gas or electric; therefore, dishwasher programs need to ensure the savings calculations used are appropriate for the water heating equipment installed at the participating customer's facility. The energy and demand savings are determined on a per-dishwasher basis.

15.3.1.1 Eligibility Criteria

Eligible units must be compliant with the current ENERGY STAR specification and fall under one of the following categories.^{672,673} These categories are described in Table 15.3-1:

- Under Counter Dishwasher
- Stationary Rack, Single Tank, Door Type Dishwasher
- Single Tank Conveyor Dishwasher
- Multiple Tank Conveyor Dishwasher
- Pot, Pan & Utensil

Eligible building types include any non-residential application.⁶⁷⁴

Dishwashers intended for use in residential or laboratory applications are not eligible for ENERGY STAR under this product specification. Residential equipment is eligible for installation in commercial applications. In this scenario, refer to the residential savings methodology. Steam, gas, and other non-electric models also do not qualify.

Additionally, though single and multiple tank flight type conveyor dishwashing machines (where the dishes are loaded directly on the conveyor rather than transported within a rack – also referred to as a rackless conveyor) are eligible per the ENERGY STAR version 2.0 specification, they are considered ineligible for this Guidebook measure, since default values are not available for flight type dishwashers

⁶⁷² ENERGY STAR Program Requirements Product Specifications for Commercial Dishwashers. Eligibility Criteria Version 3.0.

https://www.energystar.gov/sites/default/files/Commercial%20Dishwashers%20Final%20Version%203.0%20Specification_0.pdf.

⁶⁷³ ENERGY STAR Qualified Product Listing: <https://www.energystar.gov/productfinder/product/certified-commercial-dishwashers/results>.

⁶⁷⁴ CEE Commercial Kitchens Initiative's overview of the Food Service Industry:

https://library.cee1.org/system/files/library/4203/CEE_CommKit_InitiativeDescription_Mar2021.pdf.

in the ENERGY STAR Commercial Kitchen Equipment Calculator.

Table 15.3-1: [Dishwashers] ENERGY STAR Equipment Type Descriptions

| Equipment Type | Equipment Descriptions |
|--|---|
| Under Counter Dishwasher | A machine with overall height of 38" or less, in which a rack of dishes remains stationary within the machine while being subjected to sequential wash and rinse sprays and is designed to be installed under food preparation workspaces. Under counter dishwashers can be either chemical or hot water sanitizing, with an internal booster heater for the latter. For purposes of this specification, only those machines designed for wash cycles of 10 minutes or less can qualify for ENERGY STAR. |
| Stationary Rack, Single Tank, Door Type Dishwasher | A machine in which a rack of dishes remains stationary within the machine while subjected to sequential wash and rinse sprays. This definition also applies to machines in which the rack revolves on an axis during the wash and rinse cycles. Subcategories of stationary door type machines include single and multiple wash tank, double rack, pot, pan and utensil washers, chemical dump type and hooded wash compartment ("hood type"). Stationary rack, single tank, door type models are covered by this specification and can be either chemical or hot water sanitizing, with an internal or external booster heater for the latter. |
| Single Tank Conveyor Dishwasher | A washing machine that employs a conveyor or similar mechanism to carry dishes through a series of wash and rinse sprays within the machine. Specifically, a single tank conveyor machine has a tank for wash water followed by a final sanitizing rinse and does not have a pumped rinse tank. This type of machine may include a pre-washing section before the washing section. Single tank conveyor dishwashers can either be chemical or hot water sanitizing, with an internal or external booster heater for the latter. |
| Multiple Tank Conveyor Dishwasher | A conveyor type machine that has one or more tanks for wash water and one or more tanks for pumped rinse water, followed by a final sanitizing rinse. This type of machine may include one or more pre-washing sections before the washing section. Multiple tank conveyor dishwashers can be either chemical or hot water sanitizing, with an internal or external hot water booster heater for the latter. |
| Pot, Pan, and Utensil | A stationary rack, door type machine designed to clean and sanitize pots, pans, and kitchen utensils. |

15.3.1.2 Baseline Condition

Baseline equipment is either a low⁶⁷⁵ or high temperature⁶⁷⁶ machine as defined by Table 15.3-1, which is not used in a residential or laboratory setting. For low temperature units, the DHW is assumed to be electrically heated. For high temperature units, the DHW can either be heated by electric or natural gas methods. For units heated with natural gas, the unit shall have an attached electric booster heater.

⁶⁷⁵ Low temperature machines apply a chemical sanitizing solution to the surface of the dishes to achieve sanitation.

⁶⁷⁶ High temperature machines apply only hot water to the surface of the dishes to achieve sanitation.

15.3.1.3 High-Efficiency Condition

Qualifying equipment must be compliant with the current ENERGY STAR v3.0 specification, effective July 27, 2021. High temperature equipment sanitizes using hot water and requires a booster heater. Low temperature equipment uses chemical sanitization and does not require a booster heater. Qualified products must be less than or equal to the maximum idle energy rate and water consumption requirements from Table 15.3-2.

Table 15.3-2: [Dishwashers] ENERGY STAR Specification⁶⁷⁷

| Machine Type | Low Temperature Efficiency Requirements | | High Temperature Efficiency Requirements | |
|-----------------------------|---|------------------------------|--|------------------------------|
| | Idle Energy Rate [kW] | Water Consumption [gal/rack] | Idle Energy Rate [kW] | Water Consumption [gal/rack] |
| Under Counter | ≤ 0.25 | ≤ 1.19 | ≤ 0.30 | ≤ 0.86 |
| Stationary Single Tank Door | ≤ 0.30 | ≤ 1.18 | ≤ 0.55 | ≤ 0.89 |
| Single Tank Conveyor | ≤ 0.85 | ≤ 0.79 | ≤ 1.20 | ≤ 0.70 |
| Multiple Tank Conveyor | ≤ 1.00 | ≤ 0.54 | ≤ 1.85 | ≤ 0.54 |
| Pot, Pan and Utensil | - | - | ≤ 0.90 | ≤ 0.58 ⁶⁷⁸ |

15.3.2 Energy and Demand Savings Methodology

15.3.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

Deemed savings are calculated using the following algorithms:

$$\begin{aligned}
 \text{Energy Savings } [\Delta kWh] &= (V_{base} - V_{ES}) \times \left(\frac{\Delta T_{DHW} + \Delta T_{boost}}{\eta_{DHW}} \right) \times \rho_{water} \times C_p \times \frac{1}{3,412} + (E_{idle,base} \\
 &- E_{idle,ES}) \times \left(1 - n_{racks} \times \frac{t_{wash}}{60} \right) \times DOH \times AOD
 \end{aligned}$$

Equation 15.3-1

$$V_{base} = t_{days} \times n_{racks} \times V_{rack,base}$$

Equation 15.3-2

⁶⁷⁷ ENERGY STAR Commercial Dishwashers Key Product Criteria.

https://www.energystar.gov/products/commercial_food_service_equipment/commercial_dishwashers/key_product_criteria.

⁶⁷⁸ Water Consumption for pot, pan and utensil is specified in gallons per square foot rather than gallons per rack.

$$V_{ES} = t_{days} \times n_{racks} \times V_{rack,ES}$$

Equation 15.3-3

$$Demand\ Savings\ [\Delta kW] = \frac{\Delta kWh}{DOH \times AOD} \times DF$$

Equation 15.3-4

Where:

| | | |
|--------------------|---|---|
| ρ_{water} | = | Density of water [lbs/gallon]. |
| C_p | = | Specific heat of water [Btu/lb °F]. |
| ΔT_{DHW} | = | Inlet water temperature increase for building water heater [°F]. |
| ΔT_{boost} | = | Inlet water temperature for booster water heater [°F]. |
| η_{DHW} | = | Building electric water heater and booster heater efficiency [%]. |
| n_{racks} | = | Number of racks washed per hour. |
| V_{base} | = | Baseline annual volume of water consumption [gal/year]. |
| V_{ES} | = | ENERGY STAR annual volume of water consumption [gal/year]. |
| $V_{rack,base}$ | = | Baseline per rack volume of water consumption [gal/rack]. |
| $V_{rack,ES}$ | = | ENERGY STAR per rack volume of water consumption [gal/rack]. |
| $E_{idle,base}$ | = | Baseline idle energy rate [kW]. |
| $E_{idle,ES}$ | = | ENERGY STAR idle energy rate [kW]. |
| t_{wash} | = | Wash time per rack [min]. |
| DOH | = | Equipment daily operating hours [hr/day]. |
| AOD | = | Facility annual operating days [days/year]. |
| 3,412 | = | Constant to convert from Btu to kWh. |
| 60 | = | Constant to convert from minutes to hours. |

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 15.3-4:
[Dishwashers] Operating Schedule Assumptions

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 10 | 260 |
| All other | 18 | 365 |

Table 15.3-5.

Table 15.3-3: [Dishwashers] ENERGY STAR Commercial Food Service Calculator Inputs⁶⁷⁹

| Inputs | Under Counter | Single Door Type | Single Tank Conveyor | Multiple Tank Conveyor | Pot, Pan and Utensil |
|---------------------------|--|------------------|----------------------|------------------------|----------------------|
| ρ_{water} | 61.4 ÷ 7.48 = 8.2 | | | | |
| C_p | 1.0 | | | | |
| ΔT_{DHW} | Gas Hot Water Heaters: 0°F Electric Hot Water Heaters: 70°F | | | | |
| ΔT_{boost} | Gas Booster Heaters: 0°F Electric Booster Heaters: 40°F | | | | |
| η_{DHW} | 98% | | | | |
| | | | | | |
| | | | | | |
| Low Temperature Units | | | | | |
| n_{racks} per hr | 4.17 | 15.56 | 2.22 | 33.33 | - |
| $V_{\text{rack,base}}$ | 1.73 | 2.10 | 1.31 | 1.04 | - |
| $V_{\text{rack,ES}}$ | 1.19 | 1.18 | 0.79 | 0.54 | - |
| $E_{\text{idle,base}}$ | 0.50 | 0.60 | 1.60 | 2.00 | - |
| $E_{\text{idle,ES}}$ | 0.25 | 0.30 | 0.85 | 1.00 | - |
| t_{wash} | 2.0 | 1.5 | 0.3 | 0.3 | - |
| High Temperature Units | | | | | |
| n_{racks} per hr | 4.17 | 15.56 | 22.22 | 33.33 | 15.56 |
| $V_{\text{rack,base}}$ | 1.09 | 1.29 | 0.87 | 0.97 | 0.70 |
| $V_{\text{rack,ES}}$ | 0.86 | 0.89 | 0.70 | 0.54 | 0.58 |

⁶⁷⁹ ENERGY STAR Commercial Food Service Equipment Calculator. 7/15/21 amendment to March 2021 update.
https://www.energystar.gov/products/commercial_food_service_equipment.

| Inputs | Under Counter | Single Door Type | Single Tank Conveyor | Multiple Tank Conveyor | Pot, Pan and Utensil |
|------------------------|---------------|------------------|----------------------|------------------------|----------------------|
| E _{idle,base} | 0.76 | 0.87 | 1.93 | 2.59 | 1.20 |
| E _{idle,ES} | 0.30 | 0.55 | 1.20 | 1.85 | 0.90 |
| t _{wash} | 2.0 | 1.0 | 0.3 | 0.2 | 3.0 |

Table 15.3-4: [Dishwashers] Operating Schedule Assumptions⁶⁸⁰

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 10 | 260 |
| All other | 18 | 365 |

Table 15.3-5: [Dishwashers] Demand Factors⁶⁸¹

| Peak Type | DF |
|-----------|-----|
| NCP | 1.0 |
| CP | 0.9 |
| 4CP | 0.9 |

15.3.2.2 Deemed Energy Savings Tables

The following deemed energy savings are based on the input assumptions from Table 15.3-3. Dual sanitizing dishwashers, with options for high and low temperature sanitization, should select the high temperature savings category unless documentation is provided demonstrating the use of low temperature/chemical sanitization.

Table 15.3-6: [Dishwashers] Deemed Energy Savings (Education: K-12)

| Facility Description | Under Counter | Single Door Type | Single Tank Conveyor | Multiple Tank Conveyor | Pot, Pan and Utensil |
|---|---------------|------------------|----------------------|------------------------|----------------------|
| Low Temp. Electric DHW | 650 | 2,854 | 2,865 | 3,993 | - |
| High Temp. Electric DHW w/ Electric Booster | 707 | 2,071 | 1,803 | 4,891 | 616 |

⁶⁸⁰ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

⁶⁸¹ Itron, Inc., "2004-2005 Database for Energy Efficiency Resources (DEER) Update Study: Final Report." Prepared for Southern California Edison. December 2005. Table 3-14, p. 3-17.

| Facility Description | Under Counter | Single Door Type | Single Tank Conveyor | Multiple Tank Conveyor | Pot, Pan and Utensil |
|---|---------------|------------------|----------------------|------------------------|----------------------|
| High Temp. Gas DHW w/ Electric Booster | 529 | 916 | 1,101 | 2,230 | 270 |
| High Temp./ Electric DHW w/ Gas Booster | 606 | 1,411 | 1,402 | 3,371 | 418 |

Table 15.3-7: [Dishwashers] Deemed Energy Savings (Education: College/University)

| Facility Description | Under Counter | Single Door Type | Single Tank Conveyor | Multiple Tank Conveyor | Pot, Pan and Utensil |
|---|---------------|------------------|----------------------|------------------------|----------------------|
| Low Temp. Electric DHW | 1,565 | 6,871 | 6,896 | 9,613 | - |
| High Temp. Electric DHW w/ Electric Booster | 1,703 | 4,985 | 4,339 | 11,774 | 1,484 |
| High Temp. Gas DHW w/ Electric Booster | 1,275 | 2,205 | 2,652 | 5,370 | 650 |
| High Temp./ Electric DHW w/ Gas Booster | 1,458 | 3,396 | 3,375 | 8,114 | 1,007 |

Table 15.3-8: [Dishwashers] Deemed Energy Savings (All Other)

| Facility Description | Under Counter | Single Door Type | Single Tank Conveyor | Multiple Tank Conveyor | Pot, Pan and Utensil |
|---|---------------|------------------|----------------------|------------------------|----------------------|
| Low Temp. Electric DHW | 3,955 | 17,362 | 17,426 | 24,292 | - |
| High Temp. Electric DHW w/ Electric Booster | 4,303 | 12,596 | 10,966 | 29,751 | 3,750 |
| High Temp. Gas DHW w/ Electric Booster | 3,221 | 5,572 | 6,700 | 13,569 | 1,642 |
| High Temp./ Electric DHW w/ Gas Booster | 3,684 | 8,592 | 8,528 | 20,504 | 2,545 |

Deemed Demand Savings Tables

The following deemed demand savings are based on the input assumptions from Table 15.3-3 and Table 15.3-4:
[Dishwashers] Operating Schedule Assumptions

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 10 | 260 |
| All other | 18 | 365 |

Table 15.3-5.

Table 15.3-9: [Dishwashers] Deemed Demand Savings (Education: K-12)

| Dishwasher Type | Peak Type | Low Temp. Electric DHW | High Temp. Electric DHW w/ Electric Booster | High Temp. Gas DHW w/ Electric Booster | High Temp. Electric DHW w/ Gas Booster |
|------------------------|-----------|------------------------|---|--|--|
| Under Counter | NCP | 0.602 | 0.655 | 0.490 | 0.561 |
| | CP | 0.542 | 0.589 | 0.441 | 0.505 |
| | 4CP | 0.542 | 0.589 | 0.441 | 0.505 |
| Stationary Single Tank | NCP | 2.643 | 1.917 | 0.848 | 1.306 |
| | CP | 2.378 | 1.726 | 0.763 | 1.176 |
| | 4CP | 2.378 | 1.726 | 0.763 | 1.176 |
| Single Tank Conveyor | NCP | 2.652 | 1.669 | 1.020 | 1.298 |
| | CP | 2.387 | 1.502 | 0.918 | 1.168 |
| | 4CP | 2.387 | 1.502 | 0.918 | 1.168 |
| Multi Tank Conveyor | NCP | 3.697 | 4.528 | 2.065 | 3.121 |
| | CP | 3.328 | 4.075 | 1.859 | 2.809 |
| | 4CP | 3.328 | 4.075 | 1.859 | 2.809 |
| Pot, Pan, Utensil | NCP | - | 0.571 | 0.250 | 0.387 |
| | CP | - | 0.514 | 0.225 | 0.349 |
| | 4CP | - | 0.514 | 0.225 | 0.349 |

Table 15.3-10: [Dishwashers] Deemed Demand Savings (Education: College and University)

| Dishwasher Type | Peak Type | Low Temp. Electric DHW | High Temp. Electric DHW w/ Electric Booster | High Temp. Gas DHW w/ Electric Booster | High Temp. Electric DHW w/ Gas Booster |
|------------------------|-----------|------------------------|---|--|--|
| Under Counter | NCP | 0.602 | 0.655 | 0.490 | 0.561 |
| | CP | 0.542 | 0.589 | 0.441 | 0.505 |
| | 4CP | 0.542 | 0.589 | 0.441 | 0.505 |
| Stationary Single Tank | NCP | 2.643 | 1.917 | 0.848 | 1.306 |
| | CP | 2.378 | 1.726 | 0.763 | 1.176 |
| | 4CP | 2.378 | 1.726 | 0.763 | 1.176 |
| Single Tank Conveyor | NCP | 2.652 | 1.669 | 1.020 | 1.298 |
| | CP | 2.387 | 1.502 | 0.918 | 1.168 |
| | 4CP | 2.387 | 1.502 | 0.918 | 1.168 |
| Multi Tank Conveyor | NCP | 3.697 | 4.528 | 2.065 | 3.121 |
| | CP | 3.328 | 4.075 | 1.859 | 2.809 |
| | 4CP | 3.328 | 4.075 | 1.859 | 2.809 |
| Pot, Pan, Utensil | NCP | - | 0.571 | 0.250 | 0.387 |
| | CP | - | 0.514 | 0.225 | 0.349 |
| | 4CP | - | 0.514 | 0.225 | 0.349 |

Table 15.3-11: [Dishwashers] Deemed Demand Savings (All Other)

| Dishwasher Type | Peak Type | Low Temp. Electric DHW | High Temp. Electric DHW w/ Electric Booster | High Temp. Gas DHW w/ Electric Booster | High Temp. Electric DHW w/ Gas Booster |
|------------------------|-----------|------------------------|---|--|--|
| Under Counter | NCP | 0.602 | 0.655 | 0.490 | 0.561 |
| | CP | 0.542 | 0.589 | 0.441 | 0.505 |
| | 4CP | 0.542 | 0.589 | 0.441 | 0.505 |
| Stationary Single Tank | NCP | 2.643 | 1.917 | 0.848 | 1.306 |
| | CP | 2.378 | 1.726 | 0.763 | 1.176 |
| | 4CP | 2.378 | 1.726 | 0.763 | 1.176 |
| Single Tank Conveyor | NCP | 2.652 | 1.669 | 1.020 | 1.298 |
| | CP | 2.387 | 1.502 | 0.918 | 1.168 |
| | 4CP | 2.387 | 1.502 | 0.918 | 1.168 |
| Multi Tank Conveyor | NCP | 3.697 | 4.528 | 2.065 | 3.121 |
| | CP | 3.328 | 4.075 | 1.859 | 2.809 |
| | 4CP | 3.328 | 4.075 | 1.859 | 2.809 |
| Pot, Pan, Utensil | NCP | - | 0.571 | 0.250 | 0.387 |
| | CP | - | 0.514 | 0.225 | 0.349 |
| | 4CP | - | 0.514 | 0.225 | 0.349 |

15.3.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) varies per eligible dishwasher type, as stated in the ENERGY STAR v2.0 Commercial Kitchen Equipment Savings Calculator.⁶⁸²

Table 15.3-12: [Dishwashers] Equipment Lifetime by Machine Type

| Machine Type | EUL (years) |
|---------------|-------------|
| Under Counter | 10 |

⁶⁸² ENERGY STAR Savings Calculator for ENERGY STAR Qualified Commercial Kitchen Equipment.

| Machine Type | EUL (years) |
|-----------------------------|-------------|
| Stationary Single Tank Door | 15 |
| Single Tank Conveyor | 20 |
| Multiple Tank Conveyor | 20 |
| Pot, Pan, and Utensil | 10 |

15.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Machine type
- Sanitization method (high temperature, low temperature)
- Energy source for primary water heater (gas, electric)
- Energy source for booster water heater (gas, electric)
- ENERGY STAR idle rate
- ENERGY STAR water consumption
- Verification of ENERGY STAR certification or alternative
- Proof of purchase including date of purchase, manufacturer, and model number
- Facility type (Education: K-12, Education: College and university, All other)

Document Revision History

Table 15.3-13: [Dishwashers] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Clarified that residential dishwashing equipment can be installed in commercial applications following the methodology in Volume 2 of TRM. |
| FY 2026 | Specified reduced operating schedule for education applications and updated corresponding deemed savings tables. Added guidance for dual sanitizing dishwashers and updated documentation requirements. |

15.4 ENERGY STAR® ELECTRIC FRYERS

15.4.1 Measure Description

This section covers the deemed savings methodology for the installation of ENERGY STAR electric fryers. Fryers that have earned ENERGY STAR certification offer shorter cook times and higher production rates through advanced burner and heat exchanger designs. Fry pot insulation reduces standby losses resulting in a lower idle energy rate. The energy and demand savings are determined on a per-fryer basis.

15.4.1.1 Eligibility Criteria

Eligible units must be compliant with the current ENERGY STAR specification, either counter-top or floor type designs, with standard-size and large vat fryers as defined below.^{683,684}

- Standard-Size Electric Fryer: A fryer with a vat that measures ≥ 12 inches and < 18 inches wide, and a shortening capacity ≥ 25 pounds and ≤ 65 pounds
- Large Vat Electric Fryer: A fryer with a vat that measures ≥ 18 inches and ≤ 24 inches wide, and a shortening capacity > 50 pounds

⁶⁸³ ENERGY STAR Program Requirements Product Specifications for Commercial Fryers. Eligibility Criteria Version 3.0.
<https://www.energystar.gov/sites/default/files/Commercial%20Fryers%20Program%20Requirements.pdf>.

⁶⁸⁴ ENERGY STAR Qualified Product Listing: <https://www.energystar.gov/productfinder/product/certified-commercial-fryers/results>.

Eligible building types include any non-residential application.⁶⁸⁵

The following products are excluded from the ENERGY STAR eligibility criteria:

- Fryers with vats measuring < 12 inches wide, or > 24 inches wide

15.4.1.2 Baseline Condition

The baseline condition is an electric standard-size fryer or large vat fryer that do not meet ENERGY STAR key product criteria.

15.4.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v3.0 specification, effective October 1, 2016. New electric standard fryers and large vat fryers must meet or exceed the requirements listed in Table 15.4-1.

Table 15.4-1: [Fryers] ENERGY STAR Specification⁶⁸⁶

| Inputs | Standard | Large-Vat |
|---------------------------|----------|-----------|
| Cooking energy efficiency | ≥ 83% | ≥ 80% |
| Idle energy rate [W] | ≤ 800 | ≤ 1,100 |

15.4.2 Energy and Demand Savings Methodology

15.4.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

Deemed savings are calculated using the following algorithms:

$$\text{Energy Savings } [\Delta kWh] = kWh_{base} - kWh_{ES}$$

Equation 15.4-1

$$kWh_{base} = kWh_{ph,base} + kWh_{cook,base} + kWh_{idle,base}$$

Equation 15.4-2

$$kWh_{ES} = kWh_{ph,ES} + kWh_{cook,ES} + kWh_{idle,ES}$$

Equation 15.4-3

kWh_{ph} , kWh_{cook} , and kWh_{idle} are each calculated the same for both the baseline and ENERGY STAR cases,

⁶⁸⁵ CEE Commercial Kitchens Initiative's overview of the Food Service Industry:

https://library.cee1.org/sites/default/files/library/4203/CEE_CommKit_InitiativeDescription_January2015.pdf.

⁶⁸⁶ ENERGY STAR Commercial Fryers Key Product Criteria.

https://www.energystar.gov/products/commercial_food_service_equipment/commercial_fryers/key_product_criteria.

as shown below, except they require their respective input assumptions relative to preheat, cooking, and idle operation as seen in Table 15.4-2.

$$kWh = \left(E_{ph} + \left(\frac{W_{food} \times DOH \times E_{food}}{\eta_{cook}} \right) + E_{idle} \times \left(DOH - \frac{t_{ph}}{60} - \frac{W_{food} \times DOH}{PC} \right) \right) \times \frac{AOD}{1,000}$$

Equation 15.4-4

$$Demand\ Savings\ [\Delta kW] = \frac{\Delta kWh - \left(\frac{\Delta E_{ph} \times t_{days}}{1,000} \right)}{DOH \times AOD} \times DF$$

Equation 15.4-5

Where:

| | | |
|-----------------|---|--|
| kWh_{base} | = | Baseline annual energy consumption [kWh]. |
| kWh_{ES} | = | ENERGY STAR annual energy consumption [kWh]. |
| E_{ph} | = | Preheat energy [Wh/BTU]. |
| ΔE_{ph} | = | Difference in baseline and ENERGY STAR preheat energy [Wh/BTU]. |
| E_{food} | = | ASTM energy to food of energy absorbed by food product during cooking [Wh/lb]. |
| E_{idle} | = | Idle energy rate [W]. |
| W_{food} | = | Pounds of food cooked per hour [lb/hr]. |
| η_{cook} | = | Cooking energy efficiency [%]. |
| PC | = | Production capacity [lb/hr]. |
| DOH | = | Equipment daily operating hours [hr/day] |
| t_{ph} | = | Preheat time [min/day]. |
| AOD | = | Facility annual operating days [days/year]. |
| 60 | = | Constant to convert from minutes to hours. |
| 1,000 | = | Constant to convert from watts to kilowatts. |

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 15.4-3: [Fryers] Operating Schedule Assumptions

| Building Type | DOH, Standard | DOH, Large Vat | AOD |
|-----------------------------------|---------------|----------------|-----|
| Education: K-12 | 6 | 180 | 180 |
| Education: College and university | 10 | 260 | 260 |
| All other | 16 | 12 | 365 |

Table 15.4-4.

Table 15.4-2: [Fryers] ENERGY STAR Commercial Food Service Calculator Inputs⁶⁸⁷

| Parameter | Standard-Sized Vat | | Large-Vat | |
|-------------------|--------------------|-------------|-----------|-------------|
| | Baseline | ENERGY STAR | Baseline | ENERGY STAR |
| E _{ph} | 2,400 | 1,900 | 2,400 | 1,900 |
| W _{food} | 9.375 | | 12.5 | |
| E _{food} | 167 | | | |
| η _{cook} | 75% | 83% | 70% | 80% |
| E _{idle} | 1,200 | 800 | 1,350 | 1,100 |
| C _{Cap} | 65 | 70 | 100 | 110 |
| | | | | |
| t _{ph} | 15 | | | |
| | | | | |

Table 15.4-3: [Fryers] Operating Schedule Assumptions⁶⁸⁸

| Building Type | DOH, Standard | DOH, Large Vat | AOD |
|-----------------------------------|---------------|----------------|-----|
| Education: K-12 | 6 | 180 | 180 |
| Education: College and university | 10 | 260 | 260 |
| All other | 16 | 12 | 365 |

Table 15.4-4: [Fryers] Demand Factors⁶⁸⁹

| Peak Type | DF |
|-----------|-----|
| NCP | 1.0 |
| CP | 0.9 |
| 4CP | 0.9 |

15.4.2.2 Deemed Energy Savings Tables

The following deemed energy savings are based on the input assumptions specified above.

⁶⁸⁷ ENERGY STAR Commercial Food Service Equipment Calculator. 7/15/21 amendment to March 2021 update.

https://www.energystar.gov/products/commercial_food_service_equipment.

⁶⁸⁸ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

⁶⁸⁹ Itron, Inc., "2004-2005 Database for Energy Efficiency Resources (DEER) Update Study: Final Report." Prepared for Southern California Edison. December 2005. Table 3-14, p. 3-17.

Table 15.4-5: [Fryers] Deemed Energy Savings by Building Type

| Building Type | Fryer Type | Annual Energy Savings [kWh] |
|-----------------------------------|------------|-----------------------------|
| Education: K-12 | Standard | 650 |
| | Large Vat | 704 |
| Education: College and university | Standard | 1,496 |
| | Large Vat | 1,619 |
| All other | Standard | 3,272 |
| | Large Vat | 2,696 |

15.4.2.3 Deemed Demand Savings Tables

Deemed demand savings are based on the input assumptions from Table 15.4-2 and Table 15.4-3: [Fryers] Operating Schedule Assumptions

| Building Type | DOH, Standard | DOH, Large Vat | AOD |
|-----------------------------------|---------------|----------------|-----|
| Education: K-12 | 6 | 180 | 180 |
| Education: College and university | 10 | 260 | 260 |
| All other | 16 | 12 | 365 |

Table 15.4-4.

Table 15.4-6: [Fryers] Deemed Demand Savings by Building Type

| Building Type | Fryer Type | Demand Savings [kW] | | |
|-----------------------------------|------------|---------------------|-------|-------|
| | | NCP | CP | 4CP |
| Education: K-12 | Standard | 0.519 | 0.476 | 0.467 |
| | Large Vat | 0.569 | 0.512 | 0.512 |
| Education: College and university | Standard | 0.525 | 0.473 | 0.473 |
| | Large Vat | 0.573 | 0.515 | 0.515 |
| All other | Standard | 0.529 | 0.476 | 0.476 |
| | Large Vat | 0.574 | 0.387 | 0.516 |

15.4.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for electric fryers, as specified in the California Database of

15.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Fryer type (standard or large vat)
- ENERGY STAR idle rate
- ENERGY STAR cooking efficiency
- ENERGY STAR certification or alternative
- Proof of purchase including date of purchase, manufacturer, and model number
- Facility type (Education: K-12, Education: College and university, All other)

Document Revision History

Table 15.4-7: [Fryers] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated documentation requirements to collect fryer type rather than fryer width. |
| FY 2026 | Specified reduced operating schedule for education applications and updated corresponding deemed savings tables. |

⁶⁹⁰ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

15.5 ENERGY STAR® ELECTRIC STEAM COOKERS

15.5.1 Measure Description

This section covers the deemed savings methodology for the installation of ENERGY STAR electric steam cookers. Steam cookers are available in 3, 4, 5, or ≥ 6 pan capacities. Steam cookers that have earned ENERGY STAR certification are up to 50% more efficient than standard models. They have higher production rates and reduced heat loss due to better insulation and a more efficient steam delivery system. The energy and demand savings are determined on a per-cooker basis.

15.5.1.1 Eligibility Criteria

Eligible units must be compliant with the current ENERGY STAR specification.^{691,692} Eligible building types include any non-residential application.⁶⁹³

Baseline and post-retrofit ENERGY STAR electric steam cookers must have equivalent pan capacities.

15.5.1.2 Baseline Condition

The baseline condition for retrofit situations is an electric steam cooker that does not meet ENERGY STAR key product criteria.

15.5.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v1.2 specification, effective August 1, 2003. Qualified products must meet the requirements from Table 15.5-1.

Table 15.5-1: [Steam Cookers] ENERGY STAR Specification⁶⁹⁴

| Pan Capacity | Cooking Energy Efficiency [%] ⁶⁹⁵ | Idle Rate [W] |
|------------------|--|---------------|
| 3-Pan | 50% | 400 |
| 4-Pan | 50% | 530 |
| 5-Pan | 50% | 670 |
| 6-Pan and Larger | 50% | 800 |

⁶⁹¹ ENERGY STAR Program Requirements Product Specifications for Commercial Steam Cookers. Eligibility Criteria Version 1.2.

https://www.energystar.gov/sites/default/files/specs/private/Commercial_Steam_Cookers_Program_Requirements%20v1_2.pdf.

⁶⁹² ENERGY STAR Qualified Product Listing: <https://www.energystar.gov/productfinder/product/certified-commercial-steam-cookers/results>.

⁶⁹³ CEE Commercial Kitchens Initiative's overview of the Food Service Industry:

https://library.cee1.org/sites/default/files/library/4203/CEE_CommKit_InitiativeDescription_January2015.pdf.

⁶⁹⁴ ENERGY STAR. Commercial Steam Cookers Key Product Criteria.

https://www.energystar.gov/products/commercial_food_service_equipment/commercial_steam_cookers/key_product_criteria.

⁶⁹⁵ Cooking Energy Efficiency is based on "heavy load (potato) cooking capacity," i.e., 12 by 20 by 2½ inch (300 by 500 by 65 mm) perforated hotel pans each filled with 8.0 ± 0.2 lb (3.6 ± 0.1 kg) of fresh, whole, US No. 1, size B, red potatoes.

15.5.2 Energy and Demand Savings Methodology

15.5.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

$$\text{Energy Savings } [\Delta kWh] = kWh_{base} - kWh_{ES}$$

Equation 15.5-1

$$kWh_{base} = kWh_{ph,base} + kWh_{cook,base} + kWh_{idle,base}$$

Equation 15.5-2

$$kWh_{ES} = kWh_{ph,ES} + kWh_{cook,ES} + kWh_{idle,ES}$$

Equation 15.5-3

kWh_{ph} , kWh_{cook} , and kWh_{idle} are each calculated the same for both the baseline and ENERGY STAR cases, as shown below, except they require their respective input assumptions relative to preheat, cooking, and idle operation as seen in Table 15.5-2.

$$kWh = \left(E_{ph} + \left(\frac{W_{food} \times DOH \times E_{food}}{\eta_{cook}} \right) + \left[(1 - 40\%) \times E_{idle} + \frac{40\% \times PC \times P \times E_{food}}{\eta_{cook}} \right] \times \left(1 - \frac{W_{food}}{PC \times P} \right) \times DOH \right) \times \frac{AOD}{1,000}$$

Equation 15.5-4

$$\text{Demand Savings } [\Delta kW] = \frac{\Delta kWh - \left(\frac{\Delta E_{ph} \times AOD}{1,000} \right)}{DOH \times AOD} \times DF$$

Equation 15.5-5

Where:

| | | |
|-----------------|---|--|
| kWh_{base} | = | Baseline annual energy consumption [kWh]. |
| kWh_{ES} | = | ENERGY STAR annual energy consumption [kWh]. |
| E_{ph} | = | Preheat energy [Wh/day]. |
| ΔE_{ph} | = | Difference in baseline and ENERGY STAR preheat energy [Wh/BTU]. |
| E_{food} | = | ASTM energy to food of energy absorbed by food product during cooking [Wh/lb]. |
| E_{idle} | = | Idle energy rate [W] (Differs for boiler-based or steam-generator equipment). |
| W_{food} | = | Pounds of food cooked per hour [lb/hr]. |

| | | |
|---------------|---|--|
| η_{cook} | = | Cooking energy efficiency [%] (Differs for boiler-based or steam generator equipment). |
| 40% | = | Percent of time in constant steam mode [%]. |
| PC | = | Production capacity [lb/hr]. |
| P | = | Pan capacity. |
| DOH | = | Equipment daily operating hours [hr/day]. |
| AOD | = | Facility annual operating days[days/year]. |
| 1,000 | = | Constant to convert from watts to kilowatts. |

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 15.5-3: Steam Cookers – Operating Schedule Assumptions

| Building Type | DOH | AOD |
|-----------------------------------|------|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 9.25 | 260 |
| All other | 9.25 | 311 |

Table 15.5-4.

Table 15.5-2: [Steam Cookers] ENERGY STAR Commercial Food Service Calculator Inputs⁶⁹⁶

| Parameter | Baseline Value | Post-Retrofit Value |
|------------|---|--|
| E_{ph} | 1,776 | 1,671.7 |
| W_{food} | | 10.81 |
| E_{food} | | 30.8 |
| η | Boiler Based: 26% Steam Generator: 30% | 50% |
| E_{idle} | Boiler Based: 1,000 Steam Generator: 1,200 | 3-Pan: 400 4-Pan: 530 5-Pan: 670 6-Pan: 800 |
| PC | 23.3 | 16.7 |
| P | | 3, 4, 5, or 6 |
| t_{on} | | 9.25 |
| t_{days} | | 311 |

⁶⁹⁶ ENERGY STAR Commercial Food Service Equipment Calculator. 7/15/21 amendment to March 2021 update.
https://www.energystar.gov/products/commercial_food_service_equipment.

Table 15.5-3: Steam Cookers – Operating Schedule Assumptions⁶⁹⁷

| Building Type | DOH | AOD |
|-----------------------------------|------|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 9.25 | 260 |
| All other | 9.25 | 311 |

Table 15.5-4: [Steam Cookers] Demand Factors⁶⁹⁸

| Peak Type | DF |
|-----------|-----|
| NCP | 1.0 |
| CP | 0.9 |
| 4CP | 0.9 |

15.5.2.2 Deemed Energy Savings Tables

The following deemed energy savings are based on the input assumptions from Table 15.5-2.

Table 15.5-5: [Steam Cookers] Deemed Energy Savings (Education: K-12)

| Steam Cooker Type | P | Annual Energy Savings [kWh] |
|-------------------|------------------|-----------------------------|
| Boiler Based | 3-Pan | 3,006 |
| | 4-Pan | 3,694 |
| | 5-Pan | 4,367 |
| | 6-Pan and larger | 5,040 |
| Steam Generator | 3-Pan | 2,528 |
| | 4-Pan | 3,062 |
| | 5-Pan | 3,579 |
| | 6-Pan and larger | 4,095 |

Table 15.5-6: [Steam Cookers] Deemed Energy Savings (Education: College/University)

| Steam Cooker Type | P | Annual Energy Savings [kWh] |
|-------------------|-------|-----------------------------|
| Boiler Based | 3-Pan | 6,678 |
| | 4-Pan | 8,211 |

⁶⁹⁷ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

⁶⁹⁸ Itron, Inc., "2004-2005 Database for Energy Efficiency Resources (DEER) Update Study: Final Report." Prepared for Southern California Edison. December 2005. Table 3-14, p. 3-17.

| Steam Cooker Type | P | Annual Energy Savings [kWh] |
|-------------------|------------------|-----------------------------|
| | 5-Pan | 9,710 |
| | 6-Pan and larger | 11,210 |
| Steam Generator | 3-Pan | 5,614 |
| | 4-Pan | 6,804 |
| | 5-Pan | 7,955 |
| | 6-Pan and larger | 9,105 |

Table 15.5-7: [Steam Cookers] Deemed Energy Savings (All Other)

| Steam Cooker Type | P | Annual Energy Savings [kWh] |
|-------------------|------------------|-----------------------------|
| Boiler Based | 3-Pan | 7,988 |
| | 4-Pan | 9,822 |
| | 5-Pan | 11,614 |
| | 6-Pan and larger | 13,408 |
| Steam Generator | 3-Pan | 6,715 |
| | 4-Pan | 8,139 |
| | 5-Pan | 9,515 |
| | 6-Pan and larger | 10,891 |

Deemed Demand Savings Tables

Deemed demand savings in the following tables are based on the input assumptions specified above. The deemed demand savings below apply to all building types.

Table 15.5-8: [Steam Cookers] Deemed Demand Savings

| Steam Cooker Type | P | Demand Savings (kW) | | |
|-------------------|------------------|---------------------|-------|-------|
| | | NCP | CP | 4CP |
| Boiler Based | 3-Pan | 2.766 | 2.489 | 2.489 |
| | 4-Pan | 3.403 | 3.063 | 3.063 |
| | 5-Pan | 4.026 | 3.623 | 3.623 |
| | 6-Pan and larger | 4.650 | 4.185 | 4.185 |
| Steam Generator | 3-Pan | 2.323 | 2.091 | 2.091 |
| | 4-Pan | 2.818 | 2.536 | 2.536 |
| | 5-Pan | 3.296 | 2.967 | 2.967 |

| Steam Cooker Type | P | Demand Savings (kW) | | |
|-------------------|------------------|---------------------|-------|-------|
| | | NCP | CP | 4CP |
| | 6-Pan and larger | 3.775 | 3.397 | 3.397 |

Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for electric steam cookers, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID Cook-ElecStmCooker.⁶⁹⁹

15.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Steam cooker type (boiler-based or steam generator)
- Pan capacity (3, 4, 5, or 6+)
- ENERGY STAR idle rate
- ENERGY STAR cooking efficiency
- ENERGY STAR certification or alternative
- Proof of purchase including date of purchase, manufacturer, and model number
- Facility type (Education: K-12, Education: College and University, All other)

Document Revision History

Table 15.5-9: [Steam Cookers] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Specified reduced operating schedule for education applications and updated corresponding deemed savings tables. |

⁶⁹⁹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

15.6 ENERGY STAR® HOT FOOD HOLDING CABINETS

15.6.1 Measure Description

This section covers the deemed savings methodology for the installation of ENERGY STAR hot food holding cabinets (HFHCs). An HFHC is a heated, fully enclosed compartment with one or more solid or transparent doors designed to maintain the temperature of hot food that has been cooked using a separate appliance. HFHCs that have earned ENERGY STAR certification incorporate better insulation to reduce heat loss and may also offer additional energy saving devices such as magnetic door gaskets, auto-door closers, or Dutch doors. The insulation of the cabinet offers better temperature uniformity within the cabinet from top to bottom. The energy and demand savings are deemed and based on an interior volume range of the holding cabinets and the building type. An average wattage has been calculated for each volume range, half size, three quarter size, and full size. The energy and demand savings are determined on a per-cabinet basis.

15.6.1.1 Eligibility Criteria

HFHCs must be compliant with the current ENERGY STAR specification.^{700,701} Eligible building types include any non-residential application..⁷⁰²

The following products are excluded from the ENERGY STAR eligibility criteria:

- Dual function equipment (e.g., “cook-and-hold” and proofing units)
- Heater transparent merchandising cabinets
- Drawer warmers

15.6.1.2 Baseline Condition

The baseline condition is a half-size, three-quarter size, or full-size hot food holding cabinet that does not meet ENERGY STAR key product criteria.

15.6.1.3 High-Efficiency Condition

Eligible equipment must be compliant with the current ENERGY STAR v2.0 specification, effective October 1, 2011. Table 15.6-1 presents idle energy rate requirements based on cabinet interior volume.

⁷⁰⁰ ENERGY STAR Program Requirements Product Specifications for Commercial Hot Food Holding Cabinets. Eligibility Criteria Version 2.0. https://www.energystar.gov/sites/default/files/specs/private/Commercial_HFHC_Program_Requirements_2.0.pdf.

⁷⁰¹ ENERGY STAR Qualified Product Listing: <https://www.energystar.gov/productfinder/product/certified-commercial-hot-food-holding-cabinets/results>.

⁷⁰² CEE Commercial Kitchens Initiative’s overview of the Food Service Industry: https://library.cee1.org/sites/default/files/library/4203/CEE_CommKit_InitiativeDescription_January2015.pdf.

Table 15.6-1: [HFHCs] ENERGY STAR Specification^{703,704}

| Product Category | Product Interior Volume [ft ³] | Idle Energy Rate [W] |
|--------------------|--|----------------------|
| Half Size | 0 < V < 13 | ≤ 21.5 V |
| Three-Quarter Size | 13 ≤ V ≤ 28 | ≤ 2.0 V + 254.0 |
| Full Size | 28 ≤ V | ≤ 3.8 V + 203.5 |

15.6.2 Energy and Demand Savings Methodology

15.6.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

Deemed savings are calculated using the following algorithms:

$$\text{Energy Savings } [\Delta kWh] = \frac{(E_{Idle,base} - E_{Idle,ES})}{1,000} \times DOH \times AOD$$

Equation 15.6-1

$$\text{Demand Savings } [\Delta kW] = \frac{(E_{Idle,base} - E_{Idle,ES})}{1,000} \times DF$$

Equation 15.6-2

Where:

| | | |
|------------------------------|---|---|
| <i>V</i> | = | <i>Product Interior Volume [ft³].</i> |
| <i>E_{Idle,base}</i> | = | <i>Baseline idle energy rate [W]; see Table 15.6-2.</i> |
| <i>E_{Idle,ES}</i> | = | <i>ENERGY STAR idle energy rate [W]; see Table 15.6-2.</i> |
| <i>DOH</i> | = | <i>Equipment daily operating hours [hours/day].</i> |
| <i>AOD</i> | = | <i>Facility operating days [days/year].</i> |
| <i>1,000</i> | = | <i>Constant to convert from watts to kilowatts.</i> |
| <i>DF</i> | = | <i>Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.3-1.</i> |

⁷⁰³ ENERGY STAR Commercial Fryers Key Product Criteria.

https://www.energystar.gov/products/commercial_food_service_equipment/commercial_hot_food_holding_cabinets/key_product_criteria.

⁷⁰⁴ V = Interior Volume, which equals Interior Height x Interior Width x Interior Depth.

Table 15.6-2: [HFHCs] ENERGY STAR Commercial Food Service Calculator Inputs⁷⁰⁵

| Input Variable | Half-Size $0 < V < 13$ | 3/4-Size $13 \leq V < 28$ | Full-Size $28 \leq V$ |
|------------------------|---------------------------|------------------------------|--------------------------|
| V^{706} | 8 | 22 | 53 |
| $E_{\text{Idle,base}}$ | $30 \times V$ | | |
| $E_{\text{Idle,ES}}$ | $21.5 \times V$ | $2 \times V + 254$ | $3.8 \times V + 203.5$ |

Table 15.6-3: [HFHCs] Operating Schedule Assumptions⁷⁰⁷

| Building Type | DOH | AOD |
|-----------------------------------|-----|-----|
| Education: K-12 | 6 | 180 |
| Education: College and university | 9 | 260 |
| All other | 9 | 365 |

Table 15.6-4: [HFHCs] Demand Factors⁷⁰⁸

| Peak Type | DF |
|-----------|-----|
| NCP | 1.0 |
| CP | 0.9 |
| 4CP | 0.9 |

15.6.2.2 Deemed Energy and Demand Savings Tables

Deemed energy and demand savings are based on the input assumptions specified above..

⁷⁰⁵ ENERGY STAR Commercial Food Service Equipment Calculator. 7/15/21 amendment to March 2021 update.

https://www.energystar.gov/products/commercial_food_service_equipment.

⁷⁰⁶ Averages of product interior volume determined based on review of ENERGY STAR qualified product listing.

⁷⁰⁷ Fisher-Nickel, Inc., "Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report." Prepared for the California Energy Commission. October 2014. Appendix E.

⁷⁰⁸ Itron, Inc., "2004-2005 Database for Energy Efficiency Resources (DEER) Update Study: Final Report." Prepared for Southern California Edison. December 2005. Table 3-14, p. 3-17.

Table 15.6-5: [HFHCs] Deemed Energy and Demand Savings

| Building Type | Size | Annual Energy Savings [kWh] | NCP Demand Savings [kW] | CP Demand Savings [kW] | 4CP Demand Savings [kW] |
|-----------------------------------|------------------|-----------------------------|-------------------------|------------------------|-------------------------|
| Education: K-12 | $0 < V < 13$ | 73 | 0.068 | 0.061 | 0.061 |
| | $13 \leq V < 28$ | 391 | 0.362 | 0.326 | 0.326 |
| | $28 \leq V$ | 1,280 | 1.185 | 1.067 | 1.067 |
| Education: College and university | $0 < V < 13$ | 159 | 0.068 | 0.061 | 0.061 |
| | $13 \leq V < 28$ | 847 | 0.362 | 0.326 | 0.326 |
| | $28 \leq V$ | 2,773 | 1.185 | 1.067 | 1.067 |
| All other | $0 < V < 13$ | 223 | 0.068 | 0.061 | 0.061 |
| | $13 \leq V < 28$ | 1,189 | 0.362 | 0.326 | 0.326 |
| | $28 \leq V$ | 3,893 | 1.185 | 1.067 | 1.067 |

15.6.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for HFHCs, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID Cook-HoldCab.⁷⁰⁹

15.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Manufacturer and model number
- Interior cabinet volume
- ENERGY STAR idle rate
- ENERGY STAR certification or alternative
- Proof of purchase including date of purchase, manufacturer, and model number
- Facility type (Education: K-12, Education: College and university, All other)

⁷⁰⁹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 15.6-6: [HFHCs] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Specified reduced operating schedule for education applications and updated corresponding deemed savings tables. |

15.7 PRE-RINSE SPRAY VALVES

15.7.1 Measure Description

This measure is for the installation of pre-rinse sprayers to reduce hot water usage, which saves energy associated with heating the water. Water heating is assumed to be electric. The energy and demand savings are determined on a per-sprayer basis.

15.7.1.1 Eligibility Criteria

Units must be used for commercial food preparation only and have flow rates that are no greater than the baseline flow rates specified in Table 15.7-1 per product class ounce-force (ozf). These savings are applicable only to sites where water heating fuel type is electric.

15.7.1.2 Baseline Condition

Effective January 28, 2019, the reference baseline equipment is a pre-rinse spray valve (PRSV) with a flowrate that does not exceed the maximum flow rate per product class as specified in Table 15.7-1.

Table 15.7-1: [PRSVs] Flow Rate Limits⁷¹⁰

| Product Class (ozf) | Flow Rate (gpm) |
|---------------------|-----------------|
| ≤ 5 | 1.00 |
| > 5 and ≤ 8 | 1.20 |
| > 8 | 1.28 |

15.7.1.3 High-Efficiency Condition

Following the passing of the Energy Policy Act of 2005, the EPA announced on September 21st, 2005 that it would no longer pursue an ENERGY STAR specification for Pre-rinse Spray Valves.⁷¹¹ Rather than simply disallowing pre-rinse spray valves altogether, the savings resulting from this measure will be algorithm-based (as opposed to deemed using baseline and high-efficiency assumptions). If a standard flow rate for post-retrofit equipment can be identified, future updates will address the transformation of this measure from an algorithm-based approach to one which is deemed.

The eligible high-efficiency equipment is a pre-rinse spray valve that has a flow rate no greater than the maximum flow rate per product class as specified in Table 15.7-1. The sprayer should be capable of the same cleaning ability as the old sprayer.⁷¹²

⁷¹⁰ Federal standards, 10 CFR 431.266. https://www.ecfr.gov/cgi-bin/text-idx?SID=2ab37ee5fd56d810322f3adce2124c6&mc=true&node=sp10.3.431.o&rgn=div6#se10.3.431_1266.

⁷¹¹ "Summary of ENERGY STAR Specification Development Process and Rationale for PreRinse Spray Valves." March 2006. https://www.energystar.gov/ia/partners/prod_development/downloads/PRSV_Decision_Memo_Final.pdf?1e37-d3b8.

⁷¹² FEMP Performance Requirements for Federal Purchases of Pre-Rinse Spray Valves, Based on ASTM F2324-03: Standard Test Method for Pre-Rinse Spray Valves (FEMP).

15.7.2 Energy and Demand Savings Methodology

15.7.2.1 Savings Algorithms and Input Variables

Energy Savings

Deemed savings are calculated based on the following algorithms:

$$\text{Energy Savings } [\Delta kWh] = \frac{U \times (F_B - F_P) \times AOD \times (T_H - T_C) \times \rho \times C_P}{RE \times 3,412}$$

Equation 15.7-1

Where:

| | | |
|--------|---|---|
| U | = | Water usage duration [minutes per day per unit]; see Table 15.7-2. |
| F_B | = | Baseline sprayer flow rate [GPM]; see Table 15.7-2. |
| F_P | = | PRSV flow rate [GPM], use actual value. |
| AOD | = | Facility annual operating days [days/year]; see Table 15.7-2. |
| T_H | = | Average mixed hot water (after spray valve) temperature [°F], 120°F. ⁷¹³ |
| T_C | = | Average supply (cold) water temperature [°F], 75.9°F. ⁷¹⁴ |
| ρ | = | Water density [lbs/gal], 8.33 |
| C_P | = | Specific heat of water [Btu/lb°F], 1 |
| RE | = | Recovery efficiency of an electric water heater; 0.98. ⁷¹⁵ |
| 3,412 | = | Constant to convert from Btu to kWh. |

⁷¹³ "CEE Commercial Kitchens Initiative Program Guidance on Pre-Rinse Spray Valves," Consortium of Energy Efficiency (CEE). Page 3.
<https://library.cee1.org/system/files/library/4252/PRSV%20Program%20Guidance.pdf>.

⁷¹⁴ FEMP Performance Requirements for Federal Purchases of Pre-Rinse Spray Valves, Based on ASTM F2324-03: Standard Test Method for Pre-Rinse Spray Valves. Average water temperature calculated according to the method in the Burch and Christensen 2007 paper "Towards Development of an Algorithm for Mains Water Temperature" and using typical meteorological year (TMY) dataset for TMY3 from Kelly Air Force Base.

⁷¹⁵ Recovery efficiency of electric water heaters as listed on the AHRI Directory of Certified Product Performance.
<https://www.ahridirectory.org>.

Table 15.7-2: [PRSVs] Assumed Variables for Energy and Demand Savings Calculations

| Variable | Assumption |
|--------------------|---|
| U ⁷¹⁶ | Food service – Full-service restaurant: 105 min/day/unit Food service – Quick-service restaurant: 45 min/day/unit Education – K-12 school: 105 min/day/unit Education – College/university, cafeteria: 210 min/day/unit Office, cafeteria: 210 min/day/unit |
| AOD ⁷¹⁷ | Food service – Full-service restaurant: 360 Food service – Quick-service restaurant: 360 Education – K-12 ⁷¹⁸ : 180 Office, cafeteria: 360 Education ⁷¹⁹ : College and university: 260 |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{\text{Energy Savings } [kWh] \times DF}{100,000}$$

Equation 15.7-2

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 15.7-3.

100,000 = Conversion factor to allow for better readability of DF values.

Table 15.7-3: [PRSVs] Demand Factors⁷²⁰

| Building Type ⁷²¹ | NCP | CP | 4CP |
|---|--------|-------|-------|
| Food service – Full-service restaurant | 11.416 | 3.612 | 1.338 |
| Food service – Quick-service restaurant | 11.416 | 6.118 | 5.854 |
| Education – K-12 school | 11.416 | 2.321 | - |
| Education – College/university, cafeteria | 11.416 | 2.321 | - |
| Office, cafeteria | 11.416 | 3.612 | 1.338 |

⁷¹⁶ “CEE Commercial Kitchens Initiative Program Guidance on pre-rinse valves”, page 3. Midpoint of typical hours of operation in footnoted building types. <https://library.cee1.org/system/files/library/4252/PRSV%20Program%20Guidance.pdf>.

⁷¹⁷ For facilities that operate year-round: assume operating days of 360 days/year for dormitories with few occupants in the summer: 360 x (9/12) = 270 days.

⁷¹⁸ Fisher-Nickel, Inc., “Characterizing the Energy Efficiency Potential of Gas-Fired Commercial Food Service Equipment. Final Project Report.” Prepared for the California Energy Commission. October 2014. Appendix E.

⁷¹⁹ Ibid.

⁷²⁰ Peak load share factors are developed in accordance with the definitions provided in Section 2.3 of this document, using load profiles derived from the American Society of Heating Refrigeration and Air-Conditioning Engineers, Inc., ASHRAE Handbook 2019. HVAC Applications. Chapter 50 51 - Service Water Heating, Section 9 – Hot Water Load and Equipment Sizing, Figure 24 – Hourly Flow Profiles for Various Building Types. DF values are multiplied by 100,000 to allow for easier readability of the values.

⁷²¹ This building type should be used for casual dining, institutional, and dormitory.

15.7.2.2 Deemed Energy Savings Tables

There are no deemed savings tables for this measure.

15.7.2.3 Deemed Demand Savings Tables

There are no deemed savings tables for this measure.

15.7.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 5 years, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID Cook-LowPreRinse.⁷²²

15.7.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Spray force in ounce-force (ozf)
- Baseline equipment flowrate
- Retrofit equipment flowrate
- Building type

Document Revision History

Table 15.7-4: [PRSVs] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Adjusted mixed water hot temperature to match CEE guidance. Aligned building type names across all commercial measures. |
| FY 2026 | Specified reduced operating schedule for education applications. |

⁷²² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

16. COMMERCIAL: REFRIGERATION

16.1 DOOR HEATER CONTROLS

16.1.1 Measure Description

This measure involves the installation of Door Heater Controls for glass-door refrigerated cases with anti-sweat heaters (ASH).

16.1.1.1 Eligibility Criteria

The efficient equipment must be a standard-heat configuration door heater control utilized in an eligible commercial retail facility on glass-door refrigerated cases for the purpose of dynamically controlling humidity.

16.1.1.2 Baseline Condition

The baseline condition is a cooler or a freezer door heater that operates 8,760 hours per year without any controls.

16.1.1.3 High-Efficiency Condition

The high-efficiency condition is a cooler or a freezer door heater connected to a heater control system, which measures the ambient humidity and temperature of the store, calculates the dew point (DP) temperature, and uses pulse width modulation to control the anti-sweat door heater based on specific algorithms for freezer and cooler doors.

16.1.2 Energy and Demand Savings Methodology

A door heater controller senses dew point (DP) temperature in the store and modulates power supplied to the heaters accordingly. DP inside a building is primarily dependent on the moisture content of outdoor ambient air. The reduced door heating also results in a reduced cooling load in the cooler. The savings are on a per-horizontal-linear foot of display case basis.

16.1.2.1 Savings Algorithms and Input Variables

Energy Savings

The energy savings from the installation of anti-sweat heater controls result from the reduced time the heater runs (kWh_{ASH}) and the reduced load on the freezer or cooler refrigeration ($\text{kWh}_{\text{refrig}}$). These savings are calculated using the following procedures:

Indoor dew point (T_{d-in}) for every hour can be calculated from outdoor dew point (T_{d-out}) during that hour by using the following equation:

$$T_{d-in} = 0.005379 \times (T_{d-out})^2 + 0.171795 \times T_{d-out} + 19.87006$$

Equation 16.1-1⁷²³

The pre-retrofit baseline assumes door heaters operate 8,760 hours annually. In the post-retrofit case, the duty for each hourly reading is calculated by assuming a linear relationship between indoor DP and duty cycle for each hour. It is assumed that the door heaters will be all off (duty cycle of 0%) at 42.89°F DP and all on (duty cycle of 100%) at 52.87°F DP for a typical supermarket⁷²⁴. Between these values, the door heaters' hourly duty cycle changes proportionally with DP, as modeled in Equation 16.1-2. For each hour of the year, the percent of time the door heater is on can be determined from that hour's DP.

$$\text{Door Heater ON\%} = \frac{T_{d-in} - \text{All OFF setpt (42.89°F)}}{\text{All ON setpt (52.87°F)} - \text{All OFF setpt (42.89°F)}}$$

Equation 16.1-2

The controller only changes the run-time of the heaters, not the kW demand. Therefore, the instantaneous door heater power (kW_{ASH}), as a resistive load, remains constant per linear foot of door heater⁷²⁵, at:

Medium temperature:

$kW_{ASH} = 0.109$ per door or 0.0436 per horizontal linear foot of door.⁷²⁶

Low temperature:

$kW_{ASH} = 0.191$ per door or 0.0764 per horizontal linear foot of door.⁷²⁷

Door heater energy consumption for each hour of the year is a product of power and run-time:

$$kWh_{ASH-Hourly} = kW_{ASH} \times \text{Door Heater ON\%} \times 1 \text{ hour}$$

Equation 16.1-3

$$kWh_{ASH} = \sum kWh_{ASH-Hourly}$$

Equation 16.1-4

⁷²³ San Diego Gas & Electric, Work Paper WPSDGENRRN0009: Anti-Sweat Heat (ASH) Controls, "Energy Savings Estimation Methodologies". page 4, Figure 2. August 2012. <https://www.sdge.com/sites/default/files/WPSDGENRRN0009%2520Rev%25200%2520Anti-Sweat%2520Heat%2520%2528ASH%2529%2520Controls%25200.doc>.

⁷²⁴ Ibid, "Direct ASH Power", page 6.

42.89°F DP and 52.87°F DP correspond to relative humidities of 35% and 50% respectively for a 72°F indoor space. These relative humidities are common practice setpoints for a typical supermarket of this temperature.

⁷²⁵ Pennsylvania TRM, "3.5.6 Controls: Anti-Sweat Heater Controls". page 381, Table 3-101. June 2016.

<http://www.puc.pa.gov/pcdocs/1350348.docx>. Additional reference from Pennsylvania TRM: State of Wisconsin, Public Service Commission of Wisconsin, Focus on Energy Evaluation, Business Programs Deemed Savings Manual. Table 4-75., March 22, 2010. https://focusonenergy.com/sites/default/files/bpdeemedavingsmanuav10_evaluationreport.pdf.

⁷²⁶ Ibid.

⁷²⁷ Ibid.

Where:

$$kWh_{ASH-Hourly} = \text{Hourly energy consumption of door heater.}$$

To calculate energy savings from the reduced refrigeration load using average system efficiency and assuming 35% of the anti-sweat heat becomes a load on the refrigeration system,⁷²⁸ the cooling load contribution from door heaters for each hour of the year can be determined by:

$$Q_{ASH}(\text{ton} - \text{hrs}) = 0.35 \times kW_{ASH} \times \frac{3,412}{12,000} \times \text{Door Heater ON\%}$$

Equation 16.1-5

Where:

$$Q_{ASH} = \text{Hourly cooling load contribution by door heaters.}$$

$$kWh_{ASH-Hourly} = \text{Hourly energy consumption of door heater.}$$

$$0.35 = \text{Portion of anti-sweat heat that becomes cooling load.}$$

$$3,412 = \text{Constant to convert kWh to Btu.}$$

$$12,000 = \text{Constant to convert tons to Btu/hr.}$$

The compressor power requirements are based on calculated cooling load and energy-efficiency ratios obtained from manufacturers' data. The compressor analysis is limited to the additional cooling load imposed by the door heaters, not the total cooling load of the refrigeration system.

For medium temperature refrigerated cases, the saturated condensing temperature (SCT) is calculated as the design dry-bulb temperature plus 15 degrees. For low temperature refrigerated cases (freezers), the SCT is the design dry-bulb temperature plus 10 degrees. The EER for both medium- and low-temperature applications is a function of SCT and part load ratio (PLR) of the compressor. PLR is the ratio of total cooling load to compressor capacity and is assumed to be a constant of 1/1.15, or approximately 0.87.⁷²⁹

For medium temperature compressors, the following equation is used to determine EER_{MT} [Btu/hr/watts] for each hour of the year.

$$EER_{MT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.1-6⁷³⁰

⁷²⁸ A Study of Energy Efficient Solutions for Anti-Sweat Heaters. Southern California Edison RTTC. December 1999.

⁷²⁹ Work Paper PGEREF108: Anti-Sweat Heat (ASH) Controls. Pacific Gas & Electric Company. May 29, 2009. Assumes 15% oversizing.

⁷³⁰ San Diego Gas & Electric, Work Paper WPSDGENRRN0009: Anti-Sweat Heat (ASH) Controls, "Energy Savings Estimation Methodologies". page 4, Figure 2. August 2012. https://www.sdge.com/sites/default/files/WPSDGENRRN0009%2520Rev%25200%2520Anti-Sweat%2520Heat%2520%2528ASH%2529%2520Controls%2520_0.doc.

Where:

| | | |
|-----------------------|---|---|
| <i>a</i> | = | 3.75346018700468. |
| <i>b</i> | = | -0.049642253137389. |
| <i>c</i> | = | 29.4589834935596. |
| <i>d</i> | = | 0.000342066982768282. |
| <i>e</i> | = | -11.7705583766926. |
| <i>f</i> | = | -0.212941092717051. |
| <i>g</i> | = | -1.46606221890819 x 10 ⁻⁶ . |
| <i>h</i> | = | 6.80170133906075. |
| <i>i</i> | = | -0.020187240339536. |
| <i>j</i> | = | 0.000657941213335828. |
| <i>PLR</i> | = | 1/1.15 = 0.87. |
| <i>T_{DB}</i> | = | Summer design dry-bulb temperature for San Antonio. |
| <i>SCT</i> | = | <i>T_{DB}</i> + 15°F. |

For low temperature compressors, the following equation is used to determine the EER_{LT} [Btu/hr/watts]:

$$EER_{LT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.1-7³¹

Where:

| | | |
|----------|---|--|
| <i>a</i> | = | 9.86650982829017. |
| <i>b</i> | = | -0.230356886617629. |
| <i>c</i> | = | 22.905553824974. |
| <i>d</i> | = | 0.00218892905109218. |
| <i>e</i> | = | -2.48866737934442. |
| <i>f</i> | = | -0.248051519588758. |
| <i>g</i> | = | -7.57495453950879 x 10 ⁻⁶ . |
| <i>h</i> | = | 2.03606248623924. |

⁷³¹ Ibid.

$$\begin{aligned}
 i &= -0.0214774331896676. \\
 j &= 0.000938305518020252. \\
 PLR &= 1/1.15 = 0.87. \\
 T_{DB} &= \text{Summer design dry-bulb temperature for San Antonio.} \\
 SCT &= T_{DB} + 10^{\circ}F.
 \end{aligned}$$

The annual energy used by the compressor to remove heat imposed by the door heaters for each hour is determined by calculating the hourly energy used based on calculated cooling load and EER, Equation 16.1-8, then summing the hourly energy for the entire year, Equation 16.1-9.

$$kWh_{refrig-hourly} = Q_{ASH} \times \frac{12}{EER}$$

Equation 16.1-8

$$kWh_{refrig} = \sum kWh_{refrig-Hourly}$$

Equation 16.1-9

Total annual energy consumption (direct door heaters and indirect refrigeration) is the sum of both annual kWh consumption variables:

$$kWh_{total} = kWh_{refrig} + kWh_{ASH}$$

Equation 16.1-10

Total energy savings is the difference between the baseline and post-retrofit case:

$$Energy\ Savings\ [\Delta kWh] = kWh_{total-baseline} - kWh_{total-post}$$

Equation 16.1-11

Demand Savings

Peak demand savings are calculated as the probability-weighted average of the top-20 hours with the highest coincidence with system peak and the hourly calculated kWh_{total} for said twenty hours per climate zone.

16.1.2.2 Deemed Energy and Demand Savings Tables

The energy and demand savings of Anti-Sweat Door Heater Controls are deemed values based on San Antonio weather and refrigeration temperature. Table 16.1-1 provides these deemed values.

Table 16.1-1: [Door Heater Controls] Deemed Savings

| Case Type | Annual Energy Savings [kWh/ft] | NCP Peak Demand Savings [kW/ft] | CP Peak Demand Savings [kW/ft] | 4CP Peak Demand Savings [kW/ft] |
|-------------------------|--------------------------------|---------------------------------|--------------------------------|---------------------------------|
| Medium Temperature Case | 196 | 0.052 | 0.018 | 0.023 |
| Low Temperature Case | 351 | 0.096 | 0.034 | 0.042 |

16.1.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for door heater controls, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GrocDisp-ASH.⁷³²

16.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Refrigeration Temperature
- Linear Feet of Medium-Temperature Doors
- Linear Feet of Low-Temperature Doors

Document Revision History

Table 16.1-2: [Door Heater Controls] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

⁷³² DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

16.2 ECM EVAPORATOR FAN MOTORS

16.2.1 Measure Description

This measure presents the algorithm methodology for the replacement of existing evaporator fan motors with electronically commutated motors (ECMs) in cooler and freezer display cases. ECMs can provide up to 65 percent reduction in fan energy use with higher efficiencies, automatic variable-speed drive, lower motor operating temperatures, and less maintenance.

16.2.1.1 Eligibility Criteria

This measure is eligible to be installed in any commercial retail facility, such as convenience stores, supermarkets, hotels, restaurants, and schools.⁷³³

All ECMs must be suitable, size-for-size replacements of evaporator fan motors.

16.2.1.2 Baseline Condition

The baseline efficiency condition is an existing shaded pole (SP) or permanent split capacitor (PSC) evaporator fan motor in a refrigerated case.

16.2.1.3 High-Efficiency Condition

The high-efficiency condition is an electronically commutated motor that replaces an existing evaporator fan motor.

16.2.2 Energy and Demand Savings Methodology

16.2.2.1 Savings Algorithms and Input Variables

Energy Savings

The energy savings from the installation of ECMs result from increased efficiency of the fan, and reduced heat produced from the fan operation. The energy and demand savings are calculated using the following equations:

Cooler and Freezer:

$$\text{Energy Savings } [\Delta kWh] = N \times \Delta kWh_{\text{per unit}}$$

Equation 16.2-1

⁷³³ Refrigeration and freezers utilized in a school setting typically function year-round. This operating schedule prevents malfunctioning due to periods of prolonged disuse and allows child nutrition meal programs offered to students and the community to operate during school off-seasons. Schools are therefore an applicable building type for this measure, which uses annual operating hours derived from a full-year schedule.

$$\Delta kWh_{per\ unit} = \Delta kW_{peak\ per\ unit} \times hours \times (1 - \%OFF)$$

Equation 16.2-2

Where:

| | | |
|-------------------------------|---|--|
| N | = | Number of motors replaced. |
| $\Delta kWh_{per\ unit}$ | = | Energy savings attributable to increased efficiency of each evaporator fan. |
| $\Delta kW_{peak\ per\ unit}$ | = | Power demand reduction attributable to the increased efficiency of each evaporator fan. |
| $hours$ | = | Annual operating hours are assumed to be 8,760 for coolers and freezers. ^{734,735} |
| $\%OFF$ | = | The percentage of time that the evaporator fan motors are off. If the facility does not have evaporator fan controls $\%OFF = 0$, if the facility has evaporator fan controls $\%OFF = 46\%$. ⁷³⁶ |

Demand Savings

Peak demand savings are calculated by the following equation:

Cooler

$$Demand\ Savings\ [\Delta kW] = N \times \Delta kW_{per\ unit}$$

Equation 16.2-3

$$\Delta kW_{peak\ per\ unit} = \frac{W_{base} - W_{ee}}{1,000} \times LF \times DC_{EvapCool} \times \left(1 + \frac{1}{COP_{cooler}}\right) \times DF$$

Equation 16.2-4

Freezer

$$Demand\ Savings\ [\Delta kW] = N \times \Delta kW_{per\ unit}$$

Equation 16.2-5

$$\Delta kW_{peak\ per\ unit} = \frac{W_{base} - W_{ee}}{1,000} \times LF \times DC_{EvapFreeze} \times \left(1 + \frac{1}{COP_{freezer}}\right) \times DF$$

Equation 16.2-6

⁷³⁴ The December 2018 VT TRM Evaporator Fan Motors measure attributes reduced operating hours to freezers. This is expressed through a reduced duty cycle of approximately $8,567 \div 8,760 = 97.8\%$. <https://puc.vermont.gov/document/ev-technical-reference-manual>.

⁷³⁵ "Commercial Refrigeration Loadshape Project Final Report," The Cadmus Group. Northeast Energy Efficiency Partnerships (NEEP), Regional Evaluation, Measurement, and Verification Forum, Lexington, MA 2015. Page 67, Table 34.

⁷³⁶ The Massachusetts Technical Reference Manual, 2012 Program Year – Plan Version, "Refrigeration – Evaporator Fan Controls," October 2011. Page 216, footnote 414 cites the following as the source for this variable:

"The value is an estimate by National Resource Management (NRM) based on extensive analysis of hourly use data. These values are also supported by Select Energy (2004). Cooler Control Measure Impact Spreadsheet User's Manual. Prepared for NSTAR."

Where:

W_{base} = Input wattage of existing/baseline evaporator fan motor; see The compressor power requirements are based on calculated cooling load and energy efficiency ratios obtained from manufacturers' data, as described below.

For medium-temperature refrigerated cases, the saturated condensing temperature (SCTMCT) is calculated as the design dry-bulb temperature plus 15 degrees. For low-temperature refrigerated cases, the SCTLT is the design dry-bulb temperature plus 10 degrees. The EER for both medium- and low-temperature applications is a function of SCT and part load ratio (PLR) of the compressor. PLR is the ratio of total cooling load to compressor capacity and is assumed to be a constant of 1/1.15 or approximately 0.87.

For medium temperature compressor, the following equation is used to determine EERMT [Btu/hr/watts] for each hour of the year:

$$EER_{MT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.2-7

Where:

a = 3.75346018700468
 b = -0.049642253137389
 c = 29.4589834935596
 d = 0.000342066982768282
 e = -11.7705583766926
 f = -0.212941092717051
 g = -1.46606221890819 x 10⁻⁶
 h = 6.80170133906075
 i = -0.020187240339536
 j = 0.000657941213335828
 PLR = 1/1.15 = 0.87
 $SCTMT$ = $T_{db} + 15$
 T_{db} = Dry-bulb temperature

For low temperature compressors, the following equation is used to determine EERLT [Btu/hr/watts] for each hour of the year:

$$EER_{LT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.2-8

Where:

| | | |
|--------------|---|--------------------------------------|
| <i>a</i> | = | 9.86650982829017 |
| <i>b</i> | = | -0.230356886617629 |
| <i>c</i> | = | 22.905553824974 |
| <i>d</i> | = | 0.00218892905109218 |
| <i>e</i> | = | -2.48866737934442 |
| <i>f</i> | = | -0.248051519588758 |
| <i>g</i> | = | -7.57495453950879 x 10 ⁻⁶ |
| <i>h</i> | = | 2.03606248623924 |
| <i>i</i> | = | -0.0214774331896676 |
| <i>j</i> | = | 0.000938305518020252 |
| <i>SCTLT</i> | = | <i>Tdb</i> + 10 |

Table 16.2-1.

| | | |
|-----------------------|---|--|
| <i>W_{ee}</i> | = | Input wattage of new energy efficient evaporator fan motor; see The compressor power requirements are based on calculated cooling load and energy efficiency ratios obtained from manufacturers' data, as described below. |
|-----------------------|---|--|

For medium-temperature refrigerated cases, the saturated condensing temperature (SCTMCT) is calculated as the design dry-bulb temperature plus 15 degrees. For low-temperature refrigerated cases, the SCTLT is the design dry-bulb temperature plus 10 degrees. The EER for both medium- and low-temperature applications is a function of SCT and part load ratio (PLR) of the compressor. PLR is the ratio of total cooling load to compressor capacity and is assumed to be a constant of 1/1.15 or approximately 0.87.

For medium temperature compressor, the following equation is used to determine EERMT [Btu/hr/watts] for each hour of the year:

$$EER_{MT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.2-7

Where:

| | | |
|--------------|---|--------------------------------------|
| <i>a</i> | = | 3.75346018700468 |
| <i>b</i> | = | -0.049642253137389 |
| <i>c</i> | = | 29.4589834935596 |
| <i>d</i> | = | 0.000342066982768282 |
| <i>e</i> | = | -11.7705583766926 |
| <i>f</i> | = | -0.212941092717051 |
| <i>g</i> | = | -1.46606221890819 x 10 ⁻⁶ |
| <i>h</i> | = | 6.80170133906075 |
| <i>i</i> | = | -0.020187240339536 |
| <i>j</i> | = | 0.000657941213335828 |
| <i>PLR</i> | = | 1/1.15 = 0.87 |
| <i>SCTMT</i> | = | <i>Tdb</i> + 15 |
| <i>Tdb</i> | = | Dry-bulb temperature |

For low temperature compressors, the following equation is used to determine EERLT [Btu/hr/watts] for each hour of the year:

$$EER_{LT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.2-8

Where:

| | | |
|----------|---|--------------------------------------|
| <i>a</i> | = | 9.86650982829017 |
| <i>b</i> | = | -0.230356886617629 |
| <i>c</i> | = | 22.905553824974 |
| <i>d</i> | = | 0.00218892905109218 |
| <i>e</i> | = | -2.48866737934442 |
| <i>f</i> | = | -0.248051519588758 |
| <i>g</i> | = | -7.57495453950879 x 10 ⁻⁶ |
| <i>h</i> | = | 2.03606248623924 |
| <i>i</i> | = | -0.0214774331896676 |

$$j = 0.000938305518020252$$

$$SCTLT = Tdb + 10$$

Table 16.2-1.

$$LF = \text{Load factor of evaporator fan motor, } 0.9.^{737}$$

$$DC_{EvapCool} = \text{Duty cycle of evaporator fan motor for cooler, } 100\%.^{738}$$

$$DC_{EvapFreeze} = \text{Duty cycle of evaporator fan motor for freezer, } 97.8\%.^{739,740}$$

$$COP_{cooler} = \text{Coefficient of performance of compressor in the cooler, } 12/EERMT; \text{ see Table 16.2-2.}$$

$$COP_{freezer} = \text{Coefficient of performance of compressor in the freezer, } 12/EERLT; \text{ see Table 16.2-2.}$$

$$DF = \text{Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.2-3.}$$

The compressor power requirements are based on calculated cooling load and energy efficiency ratios obtained from manufacturers' data, as described below.

For medium-temperature refrigerated cases, the saturated condensing temperature (SCT_{MCT}) is calculated as the design dry-bulb temperature plus 15 degrees. For low-temperature refrigerated cases, the SCT_{LT} is the design dry-bulb temperature plus 10 degrees. The EER for both medium- and low-temperature applications is a function of SCT and part load ratio (PLR) of the compressor. PLR is the ratio of total cooling load to compressor capacity and is assumed to be a constant of 1/1.15 or approximately 0.87.⁷⁴¹

For medium temperature compressor, the following equation is used to determine EER_{MT} [Btu/hr/watts] for each hour of the year:

$$EER_{MT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.2-7

Where:

$$a = 3.75346018700468$$

⁷³⁷ The Pennsylvania TRM, June 2016, cites the following as the source for determining the load factor of the evaporator fan motor: "ActOnEnergy; Business Program-Program Year 2, June 2009 through May 2010. Technical Reference Manual, No. 2009-01." Published 12/15/2009.

Pennsylvania TRM, "3.5.2 High-Efficiency Fan Motors for Reach-In Refrigerated Cases." page 365, Table 3-89. June 2016.

<http://www.puc.pa.gov/pcdocs/1350348.docx>.

⁷³⁸ "Efficiency Maine, Commercial/Industrial and Multifamily Technical Reference Manual 2020.1," July 1, 2019, p.83, footnote 401.

⁷³⁹ The December 2018 VT TRM Evaporator Fan Motors measure attributes reduced operating hours to freezers. This is expressed through a reduced duty cycle of approximately $8,567 \div 8,760 = 97.8\%$. <https://puc.vermont.gov/document/ev-technical-reference-manual>.

⁷⁴⁰ "Commercial Refrigeration Loadshape Project Final Report," The Cadmus Group. Northeast Energy Efficiency Partnerships (NEEP), Regional Evaluation, Measurement, and Verification Forum, Lexington, MA 2015. Page 67, Table 34.

⁷⁴¹ Work Paper PGEREF108: Anti-Sweat Heat (ASH) Controls. Pacific Gas and Electric Company. May 29,2009. Assumes 15 percent oversizing.

| | | |
|-------------------------|---|-------------------------------------|
| <i>b</i> | = | -0.049642253137389 |
| <i>c</i> | = | 29.4589834935596 |
| <i>d</i> | = | 0.000342066982768282 |
| <i>e</i> | = | -11.7705583766926 |
| <i>f</i> | = | -0.212941092717051 |
| <i>g</i> | = | -1.46606221890819 x 10 ⁶ |
| <i>h</i> | = | 6.80170133906075 |
| <i>I</i> | = | -0.020187240339536 |
| <i>j</i> | = | 0.000657941213335828 |
| <i>PLR</i> | = | 1/1.15 = 0.87 |
| <i>SCT_{MT}</i> | = | <i>T_{db}</i> + 15 |
| <i>T_{db}</i> | = | Dry-bulb temperature |

For low temperature compressors, the following equation is used to determine EER_{LT} [Btu/hr/watts] for each hour of the year:

$$EER_{LT} = a + (b \times SCT) + (c \times PLR) + (d \times SCT^2) + (e \times PLR^2) + (f \times SCT \times PLR) + (g \times SCT^3) + (h \times PLR^3) + (i \times SCT \times PLR^2) + (j \times SCT^2 \times PLR)$$

Equation 16.2-8

Where:

| | | |
|----------|---|-------------------------------------|
| <i>a</i> | = | 9.86650982829017 |
| <i>b</i> | = | -0.230356886617629 |
| <i>c</i> | = | 22.905553824974 |
| <i>d</i> | = | 0.00218892905109218 |
| <i>e</i> | = | -2.48866737934442 |
| <i>f</i> | = | -0.248051519588758 |
| <i>g</i> | = | -7.57495453950879 x 10 ⁶ |
| <i>h</i> | = | 2.03606248623924 |
| <i>i</i> | = | -0.0214774331896676 |
| <i>j</i> | = | 0.000938305518020252 |

$$SCT_{LT} = T_{db} + 10$$

Table 16.2-1: [ECM Motors] Motor Sizes, Efficiencies, and Input Watts^{742,743}

| Nominal Motor Size | Motor Output (W) | SP Eff | SP Input (W) | PSC Eff | PSC Input (W) | ECM Eff. | ECM Input (W) |
|--------------------|------------------|--------|--------------|---------|---------------|----------|---------------|
| (1-14W) | 9 | 30% | 30 | 60% | 15 | 70% | 13 |
| 1/40 HP (16-23W) | 19.5 | 30% | 65 | 60% | 33 | 70% | 28 |
| 1/20 HP (37W) | 37 | 30% | 123 | 60% | 62 | 70% | 53 |
| 1/15 HP (49W) | 49.0 | 30% | 163 | 60% | 82 | 70% | 70 |
| 1/4 HP | 186.5 | 30% | 622 | 60% | 311 | 70% | 266 |
| 1/3 HP | 248.7 | 30% | 829 | 60% | 415 | 70% | 355 |

Table 16.2-2: Compressor COP by Refrigeration Type

| Summer Design Dry Bulb Temperature | EER _{MT} ⁷⁴⁴ | EER _{LT} ⁷⁴⁵ | COP _{Cooler} | COP _{Freezer} |
|------------------------------------|----------------------------------|----------------------------------|-----------------------|------------------------|
| 100.4 | 6.00 | 4.63 | 2.00 | 2.59 |

Table 16.2-3: [ECM Motors] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.981 |
| 4CP | 0.974 |

⁷⁴² The first four rows are from the Pennsylvania TRM and the last two rows are estimated using logarithmic linear regression of smaller motor efficiencies.

⁷⁴³ Motor efficiencies: “Energy Savings Potential and Opportunities for High-Efficiency Electric Motors in Residential and Commercial Equipment.” Department of Energy. December 2013. Motor efficiencies for the baseline motors are from Table 2.1, which provides peak efficiency ranges for a variety of motors. ECM motor efficiencies are from discussion in section 2.4.3.

<https://www.energy.gov/sites/prod/files/2014/02/f8/Motor%20Energy%20Savings%20Potential%20Report%202013-12-4.pdf>.

⁷⁴⁴ See Door Heater Controls measure.

⁷⁴⁵ Ibid.

16.2.2.2 Deemed Energy and Demand Savings Tables

The energy and demand savings of ECMs are calculated using a deemed algorithm, based on dry bulb temperature, refrigeration temperature, and whether the motors have controls, and are therefore not associated with deemed energy nor demand tables. Evaporator fan nameplate data, rated power, and efficiency is also required.

16.2.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL IDs GrocDisp-FEEvapFanMtr and GrocWlklIn-WEvapFanMtr.⁷⁴⁶

16.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- Motor quantity
- Baseline motor type (SP, PSC)
- Motor power rating
- Refrigeration type (cooler, freezer)

Document Revision History

Table 16.2-4: [ECM Motors] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Clarified duty cycle assumptions and references. |
| FY 2026 | Clarified baseline condition and documentation requirements. |

⁷⁴⁶ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

16.3 ELECTRONIC DEFROST CONTROLS

16.3.1 Measure Description

This measure involves the installation of an electronic defrost control that senses whether a refrigerated case requires a defrost cycle in place of a time clock defrost control mechanism.

16.3.1.1 Eligibility Criteria

This measure is eligible to be installed in any commercial retail facility, such as convenience stores, supermarkets, hotels, restaurants, and schools.⁷⁴⁷

The refrigerated case must have a time clock mechanism that controls its defrost cycle.

16.3.1.2 Baseline Condition

The baseline condition is a refrigerated case without defrost controls or with an evaporator fan defrost system that uses a time clock mechanism to initiate electronic resistance defrost.

16.3.1.3 High-Efficiency Condition

The high-efficiency condition is an evaporator fan defrost system with electronic defrost controls.

16.3.2 Energy and Demand Savings Methodology

16.3.2.1 Savings Algorithms and Input Variables

Energy Savings

The energy savings from the installation of electronic defrost controls result from increased operating efficiency and reduced heat from fewer required defrosts. The energy and demand savings are calculated by using the following equations, with the coefficient of performance variable corresponding to low temperature or medium temperature applications:

$$\text{Energy Savings } [\Delta kWh] = \Delta kWh_{\text{defrost}} + \Delta kWh_{\text{heat}}$$

Equation 16.3-1

$$\Delta kWh_{\text{defrost}} = kW_{\text{defrost}} \times CF \times \text{hours}$$

Equation 16.3-2

⁷⁴⁷ Refrigeration and freezers utilized in a school setting typically function year-round. This operating schedule prevents malfunctioning due to periods of prolonged disuse and allows child nutrition meal programs offered to students and the community to operate during school off-seasons. Schools are therefore an applicable building type for this measure, which uses annual operating hours derived from a full-year schedule.

$$\Delta kWh_{heat} = \Delta kWh_{defrost} \times 0.28 \times Eff (kW/ton)$$

Equation 16.3-3

Where:

| | | |
|------------------------|---|--|
| $\Delta kWh_{defrost}$ | = | Energy savings resulting from an increase in operating efficiency attributable to the addition of electronic defrost controls. |
| ΔkWh_{heat} | = | Energy savings attributable to the reduced heat from reduced number of defrosts. |
| $kW_{defrost}$ | = | Load of electric defrost (default = 0.9kW ⁷⁴⁸). |
| hours | = | Number of hours defrost occurs over a year without defrost controls, 487. ⁷⁴⁹ |
| CF | = | Coincidence factor – percent reduction in defrosts required per year, 35%. |
| 0.28 | = | Constant to convert from kW and tons; 3,412 Btuh/kW divided by 12,000 Btuh/ton. |
| COP_{cooler} | = | Coefficient of performance of compressor in the cooler, 12/EER _{MT} . |
| $COP_{freezer}$ | = | Coefficient of performance of compressor in the freezer, 12/EER _{LT} . |
| EER _{MT} | = | See calculations in Section 16.1.2.1. |
| EER _{LT} | = | See calculations in Section 16.1.2.1. |

Demand Savings

Peak demand savings are calculated by the following equation:

$$\text{Demand Savings } [\Delta kW] = \frac{\Delta kWh}{\text{Hours}} \times DF$$

Equation 16.3-4

Where:

| | | |
|----|---|--|
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.3-1. |
|----|---|--|

Table 16.3-1: [Defrost Controls] Demand Factors

| Peak Type | CF |
|-----------|-------|
| NCP | 1.000 |

⁷⁴⁸ Efficiency Vermont TRM, 3/16/2015, p. 170. The total defrost element kW is proportional to the number of evaporator fans blowing over the coil. The typical wattage of the defrost element is 900W per fan. https://www.puc.nh.gov/EERE%20Board/EERS_WG/vt_trm.pdf.

⁷⁴⁹ Demand Defrost Strategies in Supermarket Refrigeration Systems, Oak Ridge National Laboratory, 2011. The refrigeration system is assumed to be in operation every day of the year, while savings from the evaporator coil defrost control will only occur during set defrost cycles. This is assumed to be (4) 20-minute cycles per day, for a total of 487 hours. <https://info.ornl.gov/sites/publications/files/pub31296.pdf>.

| Peak Type | CF |
|-----------|-------|
| CP | 0.981 |
| 4CP | 0.974 |

16.3.2.2 Deemed Energy and Demand Savings Tables

There are no deemed savings tables for this measure.

16.3.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for electronic defrost controls.⁷⁵⁰

16.3.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Hours that defrost occurs over a year without defrost controls
- Load of electric defrost
- Refrigeration temperature (low, medium)

Document Revision History

Table 16.3-2: [Defrost Controls] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Correct peak factor naming convention. |

⁷⁵⁰GDS Associates, Inc. (June 2007). Measure Life Report. Prepared for The New England State Program Working Group (SPWG).

https://library.cee1.org/sites/default/files/library/8842/CEE_Eval_MeasureLifeStudyLights&HVACGDS_1Jun2007.pdf.

Additionally, the Pennsylvania TRM Volume 3 Page 162 cites the Vermont TRM, March 16, 2015. Pg. 171: "This is a conservative estimate is based on a discussion with Heatcraft based on the components expected life. https://www.puc.nh.gov/EESE%20Board/EERS_WG/vt_trm.pdf.

16.4 EVAPORATOR FAN CONTROLS

16.4.1 Measure Description

This measure involves the installation of an evaporator fan controller in a walk-in cooler or freezer so that the evaporator fan only operates when the compressor operates instead of continuously.

16.4.1.1 Eligibility Criteria

This measure is eligible to be installed in any commercial retail facility, such as convenience stores, supermarkets, hotels, restaurants, and schools.⁷⁵¹

The existing walk-in cooler or freezer must not have an evaporator fan controller.

16.4.1.2 Baseline Condition

The baseline condition is an existing shaded pole evaporator fan motor with no temperature controls, running 8,760 annual hours.

16.4.1.3 High-Efficiency Condition

The high-efficiency condition is an energy management system (EMS) or other electronic controls to modulate evaporator fan operation based on temperature of the refrigerated space.

16.4.2 Energy and Demand Savings Methodology

16.4.2.1 Savings Algorithms and Input Variables

Energy Savings

The energy savings from the installation of electronic defrost controls result from increased operating efficiency and reduced heat load produced by fewer numbers of defrosts (i.e., decreased fan operation). The energy and demand savings are calculated using the following equations:

$$\text{Energy Savings } [\Delta kWh] = \left((kW_{evap} \times N_{fans}) - kW_{circ} \right) \times (1 - DC_{comp}) \times DC_{evap} \times BF \times 8,760$$

Equation 16.4-1

⁷⁵¹ Refrigeration and freezers utilized in a school setting typically function year-round. This operating schedule prevents malfunctioning due to periods of prolonged disuse and allows child nutrition meal programs offered to students and the community to operate during school off-seasons. Schools are therefore an applicable building type for this measure, which uses annual operating hours derived from a full-year schedule.

Demand Savings

Peak demand savings are calculated by the following equation:

$$\text{Demand Savings } [\Delta kW] = \left((kW_{\text{evap}} \times N_{\text{fans}}) - kW_{\text{circ}} \right) \times (1 - DC_{\text{comp}}) \times DC_{\text{evap}} \times BF \times DF$$

Equation 16.4-2

Where:

| | | |
|--------------------|---|---|
| kW_{evap} | = | Connected load kW of each evaporator fan. |
| kW_{circ} | = | Connected load kW of the circulating fan. |
| N_{fans} | = | Number of evaporator fans. |
| DC_{comp} | = | Duty cycle of the compressor; see Table 16.4-1. |
| DC_{evap} | = | Duty cycle of the evaporator fan; see Table 16.4-1. |
| BF | = | Bonus factor for reducing cooling load from replacing the evaporator fan with a lower wattage circulating fan when the compressor is not running; see Table 16.4-1. |
| 8,760 | = | Total hours per year. |
| DF | = | Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.4-2. |

Table 16.4-1: [Evap Fan Controls] Deemed Variables for Energy and Demand Savings Calculations⁷⁵²

| Variable | Deemed Values |
|--------------------|--------------------------------|
| kW_{evap} | 0.123 kW |
| kW_{circ} | 0.035 kW |
| DC_{comp} | 50% |
| DC_{evap} | Cooler: 100% Freezer: 94.4% |

⁷⁵² The Maine Technical Reference Manual was utilized to determine all assumed values.

Efficiency Maine, Commercial/Industrial and Multifamily Technical Reference Manual 2020.1, July 1, 2019.

kW_{evap} : Page 78, footnote 366 states this value is determined “based on a weighted average of 80% shaded-pole motors at 132 watts and 20% PSC motors at 88 watts. This weighted average is based on discussions with refrigeration contractors and is considered conservative (market penetration estimated at approximately 10%).”

kW_{circ} : Page 78, footnote 367 states this value is the “wattage of fan used by Freeaire and Cooltrol”

DC_{comp} : Page 78, footnote 368 states the reasoning for this value as follows: “A 50% duty cycle is assumed based on examination of duty cycle assumptions from Richard Traverse (35%-65%), Control (35%-65%), Natural Cool (70%), Pacific Gas and Electric (58%). Also, manufacturers typically size equipment with a built-in 67% duty factor and contractors typically add another 25% safety factor, which results in a 50% overall duty factor.”

DC_{evap} : 94.4% is equivalent to 8,273 / 8,760 annual operating hours. The assumption of 8,273 is the annual total of the assumption that “a[n] evaporator fan in a cooler runs all the time, but a freezer only runs 8273 hours per year due to defrost cycles (4 20-min defrost cycles per day),” an explanation given on page 82, footnote 401.

BF : Page 183, Table 45, footnote A summarizes the Bonus Factor $(-1 + 1/\text{COP})$ as “assum[ing] 2.0 COP for low temp, 3.5 COP for medium temp, and 5.4 COP for high temp, based on the average of standard reciprocating and discus compressor efficiencies with Saturated Suction Temperatures of -20°F, 20°F, and 45°F, respectively, and a condensing temperature of 90°F.”

| Variable | Deemed Values |
|----------|---|
| BF | Low Temp: 1.5 Medium Temp: 1.3 High Temp: 1.2 |

Table 16.4-2: [Evap Fan Controls] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.981 |
| 4CP | 0.974 |

16.4.2.2 Deemed Energy and Demand Savings Tables

There are no deemed savings tables for this measure.

16.4.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 16 years for evaporator fan controls, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GrocWikIn-WEvapFMtrCtrl.⁷⁵³

16.4.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Number of evaporator fans controlled
- Refrigeration type
- Refrigeration temperature

Document Revision History

Table 16.4-3: [Evap Fan Controls] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

⁷⁵³ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

16.5 NIGHT COVERS FOR OPEN REFRIGERATED DISPLAY CASES

16.5.1 Measure Description

This measure involves the installation of Night Covers on open vertical (multi-deck) and horizontal (or coffin-type) low-temperature and medium-temperature display. Night Covers reduce the cooling load borne by the refrigerated display case's compressor due to a combination of factors: 1) a decrease in convective heat transfer from reduced air infiltration, 2) increased insulation reducing conductive heat transfer, and 3) decreased radiation through the blocking of radiated heat.

16.5.1.1 Eligibility Criteria

The existing low or medium temperature open display case must not have night covers.

16.5.1.2 Baseline Condition

The baseline condition is an open low-temperature or medium-temperature refrigerated display case (vertical or horizontal) that is not equipped with a night cover.

16.5.1.3 High-Efficiency Condition

The high-efficiency condition is any suitable low-emissivity material sold as a night cover. It is recommended that these film-type covers have small, perforated holes to decrease the build-up of moisture. The cover must be applied for a period of at least 6 hours⁷⁵⁴ per day (i.e., continuous overnight use).

16.5.2 Energy and Demand Savings Methodology

16.5.2.1 Savings Algorithms and Input Variables

Energy Savings

This section outlines the assumptions and approach used to estimate demand and energy savings attributable to installation of Night Covers on open low and medium temperature, vertical and horizontal, refrigerated display cases. Heat transfer components of the display case include infiltration (convection), transmission (conduction), and radiation.

⁷⁵⁴ Faramarzi, R and Woodworth-Szepler, Michele L. "Modified Effects of Low-E Shields on the Performance and Power Use of a Refrigerated Display Case", Southern California Edison Refrigeration Technology and Test Center, Energy Efficiency Division, August 8, 1997. https://www.econofrost.com/acrobat/sce_report_long.pdf.

$$\text{Energy Savings } [\Delta kWh] = L \times kWh_{base} \times 9\%$$

Equation 16.5-1

Where:

| | | |
|--------------|---|--|
| L | = | Horizontal linear feet of the low- or medium-temperature refrigerated display case. |
| kWh_{base} | = | Baseline average annual unit energy consumption in terms of kWh/horizontal linear foot/year. |
| 9% | = | The reduction in compressor electricity consumption due to the night cover decreasing of convection, conduction, and radiation heat transfer. ⁷⁵⁵ |

Demand Savings

There are no NCP, CP or 4CP demand savings because this measure is implemented outside of the CP and 4CP demand periods.

16.5.2.2 Deemed Energy Savings Tables

The per-linear-foot energy savings of Night Covers are deemed as 9% (the compressor load reduction from Night Covers defined in the previous section) of the “base-case scenario” efficiency level’s average annual unit energy consumption per horizontal linear foot per display case type from the U.S. Department of Energy’s (DOE) Technical Support Document for Commercial Refrigeration Equipment.⁷⁵⁶ Vertical and horizontal open equipment types were selected for inclusion given the nature of this measure.

⁷⁵⁵ Ibid. “Table 1 - Effects of utilizing Heat Reflecting Shields on Refrigeration System Parameters Non-24-hour Supermarket with Shields and Holiday Case versus Base Case”

⁷⁵⁶ In 2013, the U.S. DOE conducted an extensive life-cycle cost (LCC) analysis of the commercial refrigeration equipment classes listed in the current federal standard [10 CFR 431.66](#) to determine average annual unit energy consumption per equipment class. In this analysis, 10,000 separate simulations yielded probability distributions for various parameters associated with each equipment class, among them: the efficiency level in kWh/yr. These efficiency levels were then subject to roll-up calculations to determine market shares of each efficiency level, which were then utilized to compute the average consumption for said efficiency level listed in Table 16.5-1.

Energy Conservation Standards for Commercial Refrigeration Equipment: Technical Support Document, U.S. Department of Energy, September 2013.

https://www1.eere.energy.gov/buildings/appliance_standards/pdfs/cre2_nopr_tsd_2013_08_28.pdf.

LCC Summary Statistics: Section 8B2

Average Annual Unit Energy Consumption per Linear Foot by Efficiency Level: Table 10.2.4

Table 16.5-1: [Night Covers] Deemed Energy Savings

| Temperature ⁷⁵⁷ | Condensing Unit Configuration | Equipment Family | Average Annual Energy Consumption per Horizontal Linear Foot | ΔkWh |
|----------------------------|-------------------------------|------------------|--|--------|
| Medium (≥32±2 °F) | Remote Condensing | Vertical Open | 1,453 | 130.77 |
| | | Horizontal Open | 439 | 39.51 |
| | Self-Contained | Vertical Open | 2,800 | 252.00 |
| | | Horizontal Open | 1,350 | 121.50 |
| Low (<32±2 °F) | Remote Condensing | Vertical Open | 3,292 | 296.28 |
| | | Horizontal Open | 1,007 | 90.63 |
| | Self-Contained | Horizontal Open | 2,748 | 247.32 |

16.5.2.3 Deemed Demand Savings Tables

There are no deemed demand savings tables for this measure.

16.5.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 5 years for night covers, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GrocDisp-DispCvrs.⁷⁵⁸

16.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Display case equipment type
 - Condensing unit configuration (Remote Condensing or Self-Contained)
 - Equipment Family (Vertical or Horizontal)
 - Operating Temperature (Low or Medium as defined in Table 16.5-1)
- Horizontal linear feet of night covers

⁷⁵⁷ Temperature ranges per commercial refrigeration equipment type are detailed in the current federal standard 10 CFR 431.66. https://www.ecfr.gov/cgi-bin/text-idx?SID=ea9937006535237ca30dfd3e03ebaff2&mc=true&node=se10.3.431_166&rgn=div8.

⁷⁵⁸ DEER READI (Remote Ex-Ante Database Interface). <http://www.deerresources.com/index.php/readi>.

Document Revision History

Table 16.5-2: [Night Covers] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

16.6 ENERGY STAR® SOLID AND GLASS DOOR REACH-IN COOLERS

16.6.1 Measure Description

This section presents the deemed savings methodology for the installation of ENERGY STAR or CEE certified vertical or horizontal closed solid and glass (transparent) door reach-in refrigerators and freezers.

- Vertical closed: Equipment with hinged or sliding doors and a door angle less than 45 degrees.
- Horizontal closed: Equipment with hinged or sliding doors and a door angle greater than or equal to 45 degrees.

16.6.1.1 Eligibility Criteria

Solid or glass door reach-in vertical and horizontal refrigerators and freezers must meet ENERGY STAR minimum efficiency requirement; see Table 16.6-2.

The following products are excluded from the ENERGY STAR eligibility criteria:

- Residential refrigerators and freezers. Residential equipment is eligible for installation in commercial applications. In this scenario, refer to the residential savings methodology.
- Prep tables, horizontal open equipment, vertical open equipment, semi-vertical open equipment, remote condensing equipment, convertible temperature equipment, and ice cream freezers

Chef base (or griddle stands) and service over the counter equipment are included in the ENERGY STAR specification, but they are excluded from this measure.

16.6.1.2 Baseline Condition

The baseline condition is a regular vertical refrigerator or freezer with anti-sweat heaters on doors that meets federal standards. The baseline daily kWh for solid door and glass door commercial reach-in refrigerators and freezers are shown in Table 16.6-1.

Table 16.6-1: [Door Reach-Ins] Baseline Energy Consumption^{759, 760}

| Baseline Standards | Refrigerator Daily Consumption (kWh) | Freezer Daily Consumption (kWh) |
|--------------------|--------------------------------------|---------------------------------|
| Solid Door | $0.10 \times V + 2.04$ | $0.40 \times V + 1.38$ |
| Glass Door | $0.12 \times V + 3.34$ | $0.75 \times V + 4.10$ |

16.6.1.3 High-Efficiency Condition

The high-efficiency condition is a solid or glass door reach-in refrigerators and freezers meeting ENERGY STAR minimum efficiency requirements, as shown in Table 16.6-2.

Table 16.6-2: [Door Reach-Ins] Efficient Energy Consumption⁷⁶¹

| Door Type | Product Volume (ft ³) ⁷⁶² | Refrigerator Daily Consumption (kWh) | Freezer Daily Consumption (kWh) |
|---|--|--------------------------------------|---------------------------------|
| Vertical closed solid door | $0 < V < 15$ | $0.0267 \times V + 0.8000$ | $0.2100 \times V + 0.9000$ |
| | $15 \leq V < 30$ | $0.0500 \times V + 0.4500$ | $0.1200 \times V + 2.2480$ |
| | $30 \leq V < 50$ | | $0.2578 \times V - 1.8860$ |
| | $V \geq 50$ | $0.0250 \times V + 1.6991$ | $0.1400 \times V + 4.0000$ |
| Vertical closed glass door | $0 < V < 15$ | $0.0950 \times V + 0.4450$ | $0.2320 \times V + 2.3600$ |
| | $15 \leq V < 30$ | $0.0500 \times V + 1.1200$ | |
| | $30 \leq V < 50$ | $0.0760 \times V + 0.3400$ | |
| | $V \geq 50$ | $0.1050 \times V - 1.1110$ | |
| Horizontal closed door (solid or glass) | All volumes | $0.05 \times V + 0.28$ | $0.0570 \times V + 0.5500$ |

⁷⁵⁹ https://www.ecfr.gov/cgi-bin/text-idx?SID=ea9937006535237ca30dfd3e03ebaff2&mc=true&node=se10.3.431_166&rgn=div8.

⁷⁶⁰ V = Interior volume [ft³] of a refrigerator or freezer (as defined in the Association of Home Appliance Manufacturers Standard HRF1-1979).

⁷⁶¹ ENERGY STAR Program Requirements for Commercial Refrigerators and Freezers Partner Commitments Version 4.0, U.S. Environmental Protection Agency.

https://www.energystar.gov/sites/default/files/Commercial%20Refrigerators%20and%20Freezers%20V4%20Spec%20Final%20Version_0.pdf.

⁷⁶² Based on simple average product volume for volume ranges of vertical solid and glass door refrigerators and freezers. ENERGY STAR Certified Commercial Refrigerators and Freezers qualified product listing. Accessed August 2020.

<https://www.energystar.gov/productfinder/product/certified-commercial-refrigerators-and-freezers/results>.

16.6.2 Energy and Demand Savings Methodology

16.6.2.1 Savings Algorithms and Input Variables

Energy Savings

The energy and demand savings of Solid and Glass Door Reach-In Refrigerators and Freezers are calculated using values in Table 16.6-1 and Table 16.6-2, based on the volume of the units.

The energy savings calculations are found below.

$$\text{Energy Savings } [\Delta kWh] = (kWh_{base} - kWh_{ee}) \times 365$$

Equation 16.6-1

Where:

kWh_{base} = Baseline maximum daily energy consumption in kWh, based on volume (V) of the unit; see Table 16.6-1.

kWh_{ee} = Maximum daily energy consumption in kWh of an efficient door retrofit, based on volume (V) of the unit; see Table 16.6-2.

V = Chilled or frozen compartment volume [ft^3] (as defined in the Association of Home Appliance Manufacturers Standard HFR-1-1979).

365 = Total days per year.

Demand Savings

The demand savings calculations are found below.

$$\text{Demand Savings } [\Delta kW] = \frac{\Delta kWh}{8,760} \times DF$$

Equation 16.6-2

Where:

8,760 = Total hours per year.

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.6-3.

Table 16.6-3: [Door Reach-Ins] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.981 |
| 4CP | 0.974 |

16.6.2.2 Deemed Energy Savings Tables

Calculated for volume ranges specified in Table 16.6-1 and Table 16.6-2, yielding the following energy savings for each unit type:

Table 16.6-4: [Door Reach-Ins] Energy Savings

| Refrigerator or Freezer | Door type | Product volume range (cubic feet) | Average product volume ⁷⁶³ | kWh |
|-------------------------|-------------------------|-----------------------------------|---------------------------------------|-------|
| Refrigerator | Vertical closed solid | $0 < V < 15$ | 9.0 | 693 |
| | | $15 \leq V < 30$ | 20.6 | 956 |
| | | $30 \leq V < 50$ | 41.7 | 1,341 |
| | | $V \geq 50$ | 67.5 | 1,972 |
| | Vertical closed glass | $0 < V < 15$ | 7.9 | 1,129 |
| | | $15 \leq V < 30$ | 21.0 | 1,347 |
| | | $30 \leq V < 50$ | 42.1 | 1,771 |
| | | $V \geq 50$ | 70.7 | 2,012 |
| | Horizontal closed solid | $0 < V < 15$ | 11.4 | 850 |
| | | $15 \leq V < 30$ | 18.6 | 982 |
| | | $30 \leq V < 50$ | 30.0 | 1,190 |
| | | $V \geq 50$ | 50.0 | 1,555 |
| | Horizontal closed glass | $0 < V < 15$ | 3.0 | 1,194 |
| | | $15 \leq V < 30$ | 20.2 | 1,633 |
| | | $30 \leq V < 50$ | 30.0 | 1,883 |
| | | $V \geq 50$ | 50.0 | 2,394 |

⁷⁶³ Average volume ranges for Refrigerator and Freezer Door Types obtained from ENERGY STAR qualified product listing.
<https://www.energystar.gov/productfinder/product/certified-commercial-refrigerators-and-freezers/results>.

| Refrigerator or Freezer | Door type | Product volume range (cubic feet) | Average product volume ⁷⁶³ | kWh |
|-------------------------|-------------------------|-----------------------------------|---------------------------------------|--------|
| Freezer | Vertical closed solid | $0 < V < 15$ | 9.4 | 827 |
| | | $15 \leq V < 30$ | 20.0 | 1,727 |
| | | $30 \leq V < 50$ | 42.3 | 3,388 |
| | | $V \geq 50$ | 68.8 | 5,573 |
| | Vertical closed glass | $0 < V < 15$ | 6.8 | 1,921 |
| | | $15 \leq V < 30$ | 20.7 | 4,549 |
| | | $30 \leq V < 50$ | 41.9 | 8,557 |
| | | $V \geq 50$ | 72.5 | 14,343 |
| | Horizontal closed solid | $0 < V < 15$ | 14.2 | 2,081 |
| | | $15 \leq V < 30$ | 19.1 | 2,694 |
| | | $30 \leq V < 50$ | 30.0 | 4,059 |
| | | $V \geq 50$ | 50.0 | 6,563 |
| | Horizontal closed glass | $0 < V < 15$ | 3.0 | 2,055 |
| | | $15 \leq V < 30$ | 15.0 | 5,090 |
| | | $30 \leq V < 50$ | 30.0 | 8,884 |
| | | $V \geq 50$ | 50.0 | 13,943 |

16.6.2.3 Deemed Demand Savings Tables

Calculated for volume ranges specified in Table 16.6-1 and Table 16.6-2, yielding the following demand savings for each unit type:

Table 16.6-5: [Door Reach-Ins] Demand Savings

| Refrigerator or Freezer | Door type | Product volume range (cubic feet) | Average product volume | NCP kW | CP kW | 4CP kW |
|-------------------------|-----------------------|-----------------------------------|------------------------|--------|-------|--------|
| Refrigerator | Vertical closed solid | $0 < V < 15$ | 9.0 | 0.079 | 0.078 | 0.077 |
| | | $15 \leq V < 30$ | 20.6 | 0.109 | 0.107 | 0.106 |
| | | $30 \leq V < 50$ | 41.7 | 0.153 | 0.150 | 0.149 |
| | | $V \geq 50$ | 67.5 | 0.225 | 0.221 | 0.219 |
| | | $0 < V < 15$ | 7.9 | 0.129 | 0.126 | 0.126 |
| | | $15 \leq V < 30$ | 21.0 | 0.154 | 0.151 | 0.150 |

| Refrigerator or Freezer | Door type | Product volume range (cubic feet) | Average product volume | NCP kW | CP kW | 4CP kW |
|-------------------------|-------------------------|-----------------------------------|------------------------|--------|-------|--------|
| | Vertical closed glass | $30 \leq V < 50$ | 42.1 | 0.202 | 0.198 | 0.197 |
| | | $V \geq 50$ | 70.7 | 0.230 | 0.225 | 0.224 |
| | Horizontal closed solid | $0 < V < 15$ | 11.4 | 0.097 | 0.095 | 0.095 |
| | | $15 \leq V < 30$ | 18.6 | 0.112 | 0.110 | 0.109 |
| | | $30 \leq V < 50$ | 30.0 | 0.136 | 0.133 | 0.132 |
| | | $V \geq 50$ | 50.0 | 0.178 | 0.174 | 0.173 |
| | Horizontal closed glass | $0 < V < 15$ | 3.0 | 0.136 | 0.134 | 0.133 |
| | | $15 \leq V < 30$ | 20.2 | 0.186 | 0.183 | 0.182 |
| | | $30 \leq V < 50$ | 30.0 | 0.215 | 0.211 | 0.209 |
| | | $V \geq 50$ | 50.0 | 0.273 | 0.268 | 0.266 |
| Freezer | Vertical closed solid | $0 < V < 15$ | 9.4 | 0.094 | 0.093 | 0.092 |
| | | $15 \leq V < 30$ | 20.0 | 0.197 | 0.193 | 0.192 |
| | | $30 \leq V < 50$ | 42.3 | 0.387 | 0.379 | 0.377 |
| | | $V \geq 50$ | 68.8 | 0.636 | 0.624 | 0.620 |
| | Vertical closed glass | $0 < V < 15$ | 6.8 | 0.219 | 0.215 | 0.214 |
| | | $15 \leq V < 30$ | 20.7 | 0.519 | 0.509 | 0.506 |
| | | $30 \leq V < 50$ | 41.9 | 0.977 | 0.958 | 0.951 |
| | | $V \geq 50$ | 72.5 | 1.637 | 1.606 | 1.595 |
| | Horizontal closed solid | $0 < V < 15$ | 14.2 | 0.238 | 0.233 | 0.231 |
| | | $15 \leq V < 30$ | 19.1 | 0.308 | 0.302 | 0.300 |
| | | $30 \leq V < 50$ | 30.0 | 0.463 | 0.455 | 0.451 |
| | | $V \geq 50$ | 50.0 | 0.749 | 0.735 | 0.730 |
| | Horizontal closed glass | $0 < V < 15$ | 3.0 | 0.235 | 0.230 | 0.228 |
| | | $15 \leq V < 30$ | 15.0 | 0.581 | 0.570 | 0.566 |
| | | $30 \leq V < 50$ | 30.0 | 1.014 | 0.995 | 0.988 |
| | | $V \geq 50$ | 50.0 | 1.592 | 1.561 | 1.550 |

16.6.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years, as specified in the California Database of Energy Efficiency

Resources (DEER) READI tool for EUL ID GrocDisp-FixtDoors.⁷⁶⁴

16.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Baseline unit volume
- Baseline unit orientation (vertical or horizontal)
- Baseline unit door type (solid, glass)
- Baseline unit temperature (refrigerator, freezer)
- New unit volume
- New unit orientation (vertical or horizontal)
- New unit door type (solid, glass)
- New unit temperature (refrigerator, freezer)
- Copy of ENERGY STAR certification or alternative

Document Revision History

Table 16.6-6: [Door Reach-Ins] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Updated ENERGY STAR efficiency requirements. Clarified that residential refrigerator and freezer equipment can be installed in commercial applications following the methodology in Volume 2 of the TRM. Updated documentation requirements. |
| FY 2026 | No revision. |

⁷⁶⁴ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

16.7 STRIP CURTAINS FOR WALK-IN REFRIGERATED STORAGE

16.7.1 Measure Description

This measure refers to the installation of infiltration barriers (strip curtains or plastic swinging doors) on walk-in coolers or freezers. These units impede heat transfer from adjacent warm and humid spaces into walk-ins when there is an opening or a door is opened, reducing the cooling load. This measure results in a reduced compressor run-time and energy consumption. The measure assumes varying durations for time the walk-in door is open based on facility type and that the strip curtains cover the entire doorframe.

16.7.1.1 Eligibility Criteria

Strip curtains or plastic swinging doors installed on walk-in coolers or freezers.

16.7.1.2 Baseline Condition

The baseline condition is a refrigerated walk-in space with nothing to impede air flow from the refrigerated space to adjacent warm and humid space when the door is opened.

16.7.1.3 High-Efficiency Condition

The high-efficiency condition is a polyethylene strip curtain added to the walk-in cooler or freezer that is at least 0.06 inches thick, or equivalent. Low temperature strip curtains must be used on low temperature applications (e.g., freezers). The strip curtain must cover the entire area of opening and may not leave gaps between strips or along the doorframe.

16.7.2 Energy and Demand Savings Methodology

16.7.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

The algorithms and assumptions detailed in this section are based on the Regional Technical Forum's methodology⁷⁶⁵, which utilizes calculations that determine refrigeration load due to infiltration by air exchange from ASHRAE's Refrigeration Handbook.

Saturation pressure over liquid water, for both the temperature of the refrigerated space which will be treated with strip curtains and the adjacent space, is calculated as follows:

⁷⁶⁵ Regional Technical Forum Strip Curtains UES Measure Workbook (Commercial Grocery Strip Curtain v2.1.xlsx). September 10th, 2019. <https://rtf.nwcouncil.org/measure/strip-curtains>.

$$\ln(P_{ws,adj}) = \frac{C_1}{^{\circ}R_{adj}} + C_2 + (C_3 \times ^{\circ}R_{adj}) + (C_4 \times ^{\circ}R_{adj}^2) + (C_5 \times ^{\circ}R_{adj}^3) + (C_6 \times ^{\circ}R_{adj}^4) + (C_7 \times \ln(^{\circ}R_{adj}))$$

Equation 16.7-1

$$\ln(P_{ws,refrig}) = \frac{C_1}{^{\circ}R_{refrig}} + C_2 + (C_3 \times ^{\circ}R_{refrig}) + (C_4 \times ^{\circ}R_{refrig}^2) + (C_5 \times ^{\circ}R_{refrig}^3) + (C_6 \times ^{\circ}R_{refrig}^4) + (C_7 \times \ln(^{\circ}R_{refrig}))$$

Equation 16.7-2

Where:

| | | |
|----------------------|---|--|
| $P_{ws,adj}$ | = | Saturation pressure over liquid water for the adjacent space. |
| $P_{ws,refrig}$ | = | Saturation pressure over liquid water for the refrigerated space. |
| C_1 | = | -1.0214165E+04. |
| C_2 | = | -4.8932428E+00. |
| C_3 | = | -5.3765794E-03. |
| C_4 | = | 1.9202377E-07. |
| C_5 | = | 3.5575832E-10. |
| C_6 | = | -9.0344688E-14. |
| C_7 | = | 4.1635019E+00. |
| C_8 | = | -1.0440397E+04. |
| C_9 | = | -1.1294650E+01. |
| C_{10} | = | -2.7022355E-02. |
| C_{11} | = | 1.2890360E-05. |
| C_{12} | = | -2.4780681E-09. |
| C_{13} | = | 6.5459673E+00. |
| $^{\circ}R_{adj}$ | = | Adjacent absolute temperature, $t_{DB,Adj} + 459.67$; see Table 16.7-1. |
| $^{\circ}R_{refrig}$ | = | Refrigeration box absolute temperature, $t_{DB,Refrig} + 459.67$; see Table 16.7-1. |

Saturation pressure over liquid water is then utilized to calculate the humidity ratio of both the refrigerated and adjacent space:

$$W_{Adj} = 0.62198 \times \frac{Rh_{Adj} \times P_{ws,Adj}}{14.696 - (Rh_{Adj} \times P_{ws,Adj})}$$

Equation 16.7-3

$$W_{Refrig} = 0.62198 \times \frac{Rh_{Refrig} \times P_{ws,Refrig}}{14.696 - (Rh_{Refrig} \times P_{ws,Refrig})}$$

Equation 16.7-4

Where:

W_{Adj} = Humidity ratio of the adjacent space.

W_{Refrig} = Humidity ratio of the refrigerated space.

Rh_{Adj} = Relative humidity of the adjacent space; see Table 16.7-1.

Rh_{Refrig} = Relative humidity of the refrigerated space; see Table 16.7-1.

The humidity ratio is utilized to compute the air enthalpies for the adjacent and refrigerated space:

$$h_{Adj} = 0.24 \times t_{DB,Adj} + (W_{Adj} \times (1061 + (0.444 \times t_{DB,Adj})))$$

Equation 16.7-5

$$h_{Refrig} = 0.24 \times t_{DB,Refrig} + (W_{Refrig} \times (1061 + (0.444 \times t_{DB,Refrig})))$$

Equation 16.7-6

Where:

h_{Adj} = Air enthalpy of the adjacent space.

h_{Refrig} = Air enthalpy of the refrigerated space.

$t_{DB,Adj}$ = Dry bulb temperature of the adjacent space; see Table 16.7-1.

$t_{DB,Refrig}$ = Dry bulb temperature of the refrigerated space; see Table 16.7-1.

This pair of air enthalpies is then utilized alongside the density factor and the adjacent and refrigerated spaces' air temperature densities and specific volumes to compute the refrigeration load for the fully established flow:

$$v_{Adj} = 0.025210942 \times {}^\circ R_{Adj} \times (1 + (1.6078 \times W_{Adj}))$$

Equation 16.7-7

$$v_{Refrig} = 0.025210942 \times {}^{\circ}R_{Refrig} \times \left(1 + (1.6078 \times W_{Refrig})\right)$$

Equation 16.7-8

$$r_{Adj} = \frac{1}{v_{Adj}}$$

Equation 16.7-9

$$r_{Refrig} = \frac{1}{v_{Refrig}}$$

Equation 16.7-10

$$F_m = \frac{2^{\frac{3}{2}}}{1 + \frac{r_{Refrig}^{\frac{1}{3}}}{r_{Adj}}}$$

Equation 16.7-11

$$q = 795.6 \times Height \times Width \times (h_{Adj} - h_{Refrig}) \times r_{Refrig} \times \left(1 - \frac{r_{Adj}}{r_{Refrig}}\right)^{\frac{1}{2}} \times (32.174 \times Height)^{\frac{1}{2}} \times F_m$$

Equation 16.7-12

v_{Adj} = Specific volume of the adjacent space.

v_{Refrig} = Specific volume of the refrigerated space.

r_{Adj} = Air temperature density of the adjacent space.

r_{Refrig} = Air temperature density of the refrigerated space.

F_m = Density factor.

q = Refrigeration load for fully established flow.

$Height$ = Doorway height; see Table 16.7-1.

$Width$ = Doorway width; see Table 16.7-1.

The infiltration between the adjacent and refrigerated space before and after the installation of the strip curtains is a product of the refrigeration load between the two spaces, the time the doorway is assumed to be open per day, the assumed doorway flow factor, and the assumed effectiveness against infiltration post-retrofit:

$$Q_{baseline} = q \times \frac{m}{60 * 24} \times D_F \times (1 - E_{baseline})$$

Equation 16.7-13

$$Q_{retrofit} = q \times \frac{m}{60 * 24} \times D_F \times (1 - E_{retrofit})$$

Equation 16.7-14

Where:

| | | |
|----------------|---|---|
| $Q_{baseline}$ | = | Baseline total infiltration load. |
| $Q_{retrofit}$ | = | Total infiltration load post-retrofit. |
| m | = | Time the door is open per day; see Table 16.7-1. |
| D_F | = | Doorway flow factor; see Table 16.7-1. |
| $E_{baseline}$ | = | Baseline assumed effectiveness against infiltration, 0. |
| $E_{retrofit}$ | = | Assumed effectiveness against infiltration post-retrofit; see Table 16.7-1. |

The demand and energy consumption of the compressor associated with each infiltration case are calculated as follows:

$$kW_{baseline} = \frac{Q_{baseline}}{EER \times 1,000}$$

Equation 16.7-15

$$kW_{retrofit} = \frac{Q_{retrofit}}{EER \times 1,000}$$

Equation 16.7-16

$$kWh_{baseline} = kW_{baseline} \times EFLH$$

Equation 16.7-17

$$kWh_{retrofit} = kW_{retrofit} \times EFLH$$

Equation 16.7-18

Where:

| | | |
|------------------|---|--|
| $kW_{baseline}$ | = | Baseline demand consumption of the compressor. |
| $kW_{retrofit}$ | = | Demand consumption of the compressor post-retrofit. |
| $kWh_{baseline}$ | = | Baseline energy consumption of the compressor. |
| $kWh_{retrofit}$ | = | Energy consumption of the compressor post-retrofit. |
| EER | = | EER per facility type (see Table 16.7-1), which are averaged or weighted across suction group types; see Table 16.7-2. |
| $EFLH$ | = | Assumed full-load hours per facility type; see Table 16.7-1. |

The difference between the baseline and retrofit demand/energy calculations yields whole-door energy savings, which are divided by the area of the doorway to yield per-square foot savings:

$$kWh_{Door} = kWh_{baseline} - kWh_{retrofit}$$

Equation 16.7-19

$$Energy\ Savings\ [\Delta kWh] = \frac{kWh_{Door}}{h \times w}$$

Equation 16.7-20

$$kW_{Door} = kW_{baseline} - kW_{retrofit}$$

Equation 16.7-21

$$Demand\ Savings\ [\Delta kW] = \frac{kW_{Door} \times DF}{h \times w}$$

Equation 16.7-22

Where:

h = Door height (ft)

w = Door width (ft)

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.7-4

Several assumptions for independent variables are utilized in the prior equations; these are tabulated in Table 16.7-1. EER variables are calculated as either the simple or weighted average of representative EERs for refrigeration suction groups that correspond to medium temperature (cooler) or low temperature (freezer) multiplex or standalone units; these are detailed in Table 16.7-2:

Table 16.7-1: [Strip Curtains] Assumed Independent Variables⁷⁶⁶

| Variable | Notation | Restaurant | | Convenience Store | | Grocery | | Refrigerated Warehouse | |
|--|----------------|------------------|-------------------|-------------------|-------------------|------------------|-------------------|------------------------|-------------------|
| | | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door |
| Adjacent temperature | t_{DB} | 70 | 67 | 68 | 64 | 71 | 67 | 59 | - |
| Refrigeration box temperature | | 39 | 8 | 39 | 5 | 37 | 5 | 28 | - |
| Relative humidity of adjacent surroundings | Rh | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.3 | - |
| Relative humidity of refrigeration box | | 0.65 | 0.4 | 0.4 | 0.6 | 0.5 | 0.45 | 0.86 | - |
| Height | $Height$ | 7 | 7 | 7 | 7 | 7 | 7 | 12 | - |
| Width | $Weight$ | 3 | 3 | 3 | 3 | 3 | 3 | 10 | - |
| Doorway flow factor | D_F | 0.51 | 0.51 | 0.51 | 0.51 | 0.625 | 0.625 | 0.8 | - |
| Post-retrofit effectiveness against infiltration | $E_{retrofit}$ | 0.8 | 0.81 | 0.79 | 0.83 | 0.88 | 0.88 | 0.89 | - |
| Time door open per day | m | 45 | 38 | 38 | 9 | 132 | 102 | 494 | - |
| Equivalent full-load hours of operation | $EFLH$ | 5,509 | 5,509 | 6,887 | 6,887 | 6,482 | 6,482 | 2,525 | - |
| Energy efficiency ratio ⁷⁶⁷ | EER | 9.8 | 4.0 | 9.8 | 4.0 | 11 | 4.1 | 9.8 | - |

⁷⁶⁶ Regional Technical Forum Strip Curtains UES Measure Workbook - Assumptions (Commercial Grocery Strip Curtain v2.1.xlsx). September 10th, 2019. <https://rtf.nwcouncil.org/measure/strip-curtains>.

⁷⁶⁷ EER is not an independent variable but is rather dependent on Table 16.7-2. It is appended here to specify which average corresponds to which facility/refrigeration type.

Table 16.7-2: [Strip Curtains] Default EER by System Configuration⁷⁶⁸

| System Configurations | Representative Suction Group | Annual Average EER Value (Btu/hr-W) | Average EER of System Configuration (Btu/hr-W) | Straight Average EER of Temperature (Btu/hr-W) | Grocery Store Weighted Average EER for Temperature (Btu/hr-W) |
|-------------------------------|------------------------------|-------------------------------------|--|--|---|
| Medium Temperature Multiplex | Suction Group 2075 | 12 | 11 | 9.8 | 11 |
| | Suction Group 2014 | 12 | | | |
| | Suction Group 2185 | 12 | | | |
| | Suction Group 2668 | 9.2 | | | |
| Medium Temperature Standalone | Suction Group 2754 | 7.8 | 8.4 | | |
| | Suction Group 894 | 8.7 | | | |
| | Suction Group 512 | 8.8 | | | |
| | Suction Group 2043 | 8.3 | | | |
| Low Temperature Multiplex | Suction Group 1509 | 3.7 | 4.2 | 4.0 | 4.1 |
| | Suction Group 898 | 4.1 | | | |
| | Suction Group 2152 | 4.7 | | | |
| | Suction Group 1753 | 4.4 | | | |
| Low Temperature Standalone | Suction Group 996 | 3.3 | 3.7 | | |
| | Suction Group 2518 | 3.4 | | | |
| | Suction Group 1950 | 4.6 | | | |
| | Suction Group 2548 | 3.7 | | | |

Table 16.7-3: [Strip Curtains] Energy Consumption and Demand for Coolers and Freezers

| Variable | Notation | Restaurant | | Convenience Store | | Grocery | | Refrigerated Warehouse | |
|-----------------------|-----------------|------------------|-------------------|-------------------|-------------------|------------------|-------------------|------------------------|-------------------|
| | | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door |
| Compressor power (kW) | $kW_{baseline}$ | 0.11 | 0.54 | 0.09 | 0.12 | 0.44 | 1.82 | 8.19 | - |
| | $kW_{retrofit}$ | 0.02 | 0.10 | 0.02 | 0.02 | 0.05 | 0.22 | 0.90 | - |

⁷⁶⁸ Regional Technical Forum Strip Curtains UES Measure Workbook - Assumptions (Commercial Grocery Strip Curtain v2.1.xlsx). September 10th, 2019. <https://rtf.nwcouncil.org/measure/strip-curtains>.

Table 16.7-4: [Strip Curtains] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.981 |
| 4CP | 0.974 |

16.7.2.2 Deemed Energy and Demand Savings Tables

The energy and demand savings for strip curtains are shown below in Table 16.7-5.

Table 16.7-5: [Strip Curtains] Deemed Energy and Demand Savings

| Savings | | Restaurant | | Convenience Store | | Grocery | | Refrigerated Warehouse | |
|---------|-----|------------------|-------------------|-------------------|-------------------|------------------|-------------------|------------------------|-------------------|
| | | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door | Cooler Main Door | Freezer Main Door |
| kWh | | 22.50 | 114.01 | 23.58 | 33.15 | 119.88 | 494.32 | 153.36 | - |
| kW | NCP | 0.0041 | 0.0207 | 0.0034 | 0.0048 | 0.0185 | 0.0763 | - | - |
| | CP | 0.0040 | 0.0203 | 0.0034 | 0.0047 | 0.0181 | 0.0748 | - | - |
| | 4CP | 0.0040 | 0.0202 | 0.0033 | 0.0047 | 0.0180 | 0.0743 | - | - |

16.7.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 4 years for strip curtains, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GrocWIkIn-StripCrtn.⁷⁶⁹

16.7.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Number of treated doors
- Unit temperature (refrigerator or freezer)

⁷⁶⁹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

Document Revision History

Table 16.7-6: [Strip Curtains] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

16.8 ZERO-ENERGY DOORS FOR REFRIGERATED CASES

16.8.1 Measure Description

This measure presents the deemed savings methodology for the installation of zero-energy doors for refrigerated cases. These new zero-energy door designs eliminate the need for anti-sweat heaters to prevent the formation of condensation on the glass surface by incorporating heat reflective coatings on the glass, gas inserted between the panes, non-metallic spacers to separate glass panes, and/or non-metallic frames.

16.8.1.1 Eligibility Criteria

This measure cannot be used in conjunction with anti-sweat heat (ASH) controls. It is not eligible to be installed on cases above 0°F.

16.8.1.2 Baseline Condition

The baseline condition is a standard vertical reach-in refrigerated case with anti-sweat heaters on the glass surface of the doors.⁷⁷⁰

16.8.1.3 High-Efficiency Condition

The high-efficiency condition is the installation of special doors that eliminate the need for anti-sweat heaters, for low-temperature cases only (below 0°F). Doors must have either heat reflective treated glass, be gas-filled, or both.

16.8.2 Energy and Demand Savings Methodology

16.8.2.1 Savings Algorithms and Input Variables

Energy Savings

The energy savings from the installation of zero-energy doors are a result of eliminating the heater (kWh_{ASH}) and the reduction in load on the refrigeration ($\text{kWh}_{\text{refrig}}$). These savings are calculated using the following procedures.

The baseline assumes door heaters are running on an 8,760-hour operation. In the post-retrofit case, it is assumed that the door heaters will all be off (duty cycle of 0%).

⁷⁷⁰ An open refrigerated case is not an eligible baseline for these existing deemed savings. Contact the evaluation team for preliminary approval of any deemed savings methodologies applied to a zero-energy door installed on an open refrigerated case.

The instantaneous door heater power (kW_{ASH}) as a resistive load remains constant per horizontal linear foot of door heater at an assumed 2.5 linear horizontal feet of door:

Medium temperature:

$$kW_{ASH} = 0.109 \text{ per door}^{771}$$

Low temperature:

$$kW_{ASH} = 0.191 \text{ per door}^{772}$$

Door heater energy consumption for each hour of the year is a product of power and run-time:

$$kWh_{ASH-Hourly} = kW_{ASH} \times \text{Door Heater ON\%} \times 1 \text{ hour}$$

Equation 16.8-1

$$kWh_{ASH} = \sum kWh_{ASH-Hourly}$$

Equation 16.8-2

Where:

$$kWh_{ASH-Hourly} = \text{Hourly energy consumption of door heater.}$$

To calculate energy savings from the reduced refrigeration load using average system efficiency and assuming 35% of the anti-sweat heat becomes a load on the refrigeration system,⁷⁷³ the cooling load contribution from door heaters can be determined by:

$$Q_{ASH}(\text{ton} - \text{hrs}) = 0.35 \times kW_{ASH} \times \frac{3,412 \frac{\text{Btu}}{\text{hr}}}{12,000 \frac{\text{Btu}}{\text{ton}}} \times \text{Door Heater ON\%}$$

Equation 16.8-3

Where:

$$Q_{ASH} = \text{Hourly cooling load contribution by door heaters.}$$

$$kWh_{ASH-Hourly} = \text{Hourly energy consumption of door heater.}$$

$$0.35 = \text{Portion of anti-sweat heat that becomes cooling load.}$$

$$3,412 = \text{Constant to convert kWh to Btu.}$$

$$12,000 = \text{Constant to convert tons to Btu/hr.}$$

⁷⁷¹ Here, "medium temperature" is equivalent to the categorization "coolers."

Pennsylvania TRM, "3.5.6 Controls: Anti-Sweat Heater Controls." page 383, June 2016. <http://www.puc.pa.gov/pcdocs/1350348.docx>.

⁷⁷² Ibid. Here, "low temperature" is equivalent to the categorization "freezers."

⁷⁷³ A Study of Energy Efficient Solutions for Anti-Sweat Heaters. Southern California Edison RTTC. December 1999.

The annual energy used by the compressor to remove heat imposed by the door heaters for each hour is determined by calculating the hourly energy used based on calculated cooling load and EER, Equation 16.8-4 then summing the hourly energy for the entire year, Equation 16.8-5.

$$kWh_{refrig-hourly} = Q_{ASH} \times \frac{12}{EER}$$

Equation 16.8-4

$$kWh_{refrig} = \sum kWh_{refrig-hourly}$$

Equation 16.8-5

Where:

EER_{MT} = See calculations in Section 16.1.2.1.

EER_{LT} = See calculations in Section 16.1.2.1.

Total annual energy consumption (direct door heaters and indirect refrigeration) is the sum of all hourly reading values:

$$kWh_{total} = kWh_{refrig} + kWh_{ASH}$$

Equation 16.8-6

Total energy savings is a result of the baseline and post-retrofit case:

$$Energy\ Savings\ [\Delta kWh] = kWh_{total-base} + kWh_{total-post}$$

Equation 16.8-7

Demand Savings

While there might be instantaneous demand savings because of the cycling of the door heaters, peak demand savings will only be attributable to the reduced refrigeration load. NCP, CP, and 4CP peak demand savings are calculated by using Equation 16.8-8 and the appropriate demand factors in Table 16.8-1.

$$Demand\ Savings\ [\Delta kW] = \frac{kWh_{refrig-base} - kWh_{refrig-post}}{8,760} \times DF$$

Equation 16.8-8

Where:

DF = Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.8-1.

Table 16.8-1: [Zero Energy Doors] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.981 |
| 4CP | 0.974 |

1.1.1.1 Deemed Energy and Demand Savings Tables

Table 16.8-2: [Zero Energy Doors] Energy/Demand Savings by Refrigeration Type per Lin. Ft. of Display Case⁷⁷⁴

| Technology Type | Annual Energy Savings [kWh/door] | NCP Savings [kWh/door] | CP Savings [kWh/door] | 4CP Savings [kWh/door] |
|-------------------------|----------------------------------|------------------------|-----------------------|------------------------|
| Medium Temperature Case | 1,141 | 0.130 | 0.128 | 0.127 |
| Low Temperature Case | 2,095 | 0.239 | 0.235 | 0.233 |

16.8.2.2 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 12 years for zero-energy doors, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GrocDisp-ZeroHtDrs.⁷⁷⁵

16.8.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Refrigerator Temperature Range

Document Revision History

Table 16.8-3: [Zero Energy Doors] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

⁷⁷⁴ Ibid.

⁷⁷⁵ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

16.9 DOOR GASKETS FOR WALK-IN AND REACH-IN COOLERS AND FREEZERS

16.9.1 Measure Description

This measure applies to the installation of door gaskets on walk-in coolers and freezers to reduce the refrigeration load associated with the infiltration of non-refrigerated air into the refrigerated space. Additionally, the reduction in moisture entering the refrigerated space also helps prevent frost on the cooling coils. Frost build-up adversely impacts the coil's heat transfer effectiveness, reduces air passage (lowering heat transfer efficiency), and increases energy use during the defrost cycle. Therefore, replacing defective door gaskets reduces compressor run time and improves the overall effectiveness of heat removal from a refrigerated cabinet.

16.9.1.1 Eligibility Criteria

Door gaskets must be installed on walk-in and reach-in coolers and freezers. The most likely applications for this measure are supermarkets, convenience stores, restaurants, and refrigerated warehouses.

16.9.1.2 Baseline Condition

The baseline condition is a walk-in or reach-in cooler or freezer with worn-out, defective door gaskets. An average baseline gasket efficacy of 90 percent is assumed for this measure.⁷⁷⁶

16.9.1.3 High-Efficiency Condition

The high-efficiency condition is a new, better-fitting gasket. Tight fitting gaskets inhibit infiltration of warm, moist air into the cold refrigerated space, reducing the cooling load. A decrease in moisture entering the refrigerated space also prevents frost on cooling coils.

16.9.2 Energy and Demand Savings Methodology

16.9.2.1 Savings Algorithms and Input Variables

Savings for this measure are based on a DEER 2005 analysis performed by Southern California Edison (SCE) and an evaluation of Pacific Gas and Electric (PG&E) direct install refrigeration measures for program year 2006-2008.^{777,778} The results from the PG&E evaluation were used as the foundation for establishing the energy savings for the refrigeration gasket measures. The energy savings achievable for new gaskets replacing baseline gaskets were found during this study to be dependent almost entirely on the leakage through the baseline gaskets. Therefore, the energy savings attributable to door gaskets

⁷⁷⁶ Gasket efficacy is defined as the ratio of the gasket length that was removed by the installers to the gasket length that was replaced. A 90% gasket efficacy equates to an average of 10% missing, badly damaged, or ineffective gasket by length replaced.

⁷⁷⁷ Southern California Edison (SCE). WPSCNRRN0013—Door Gaskets for Glass Doors of Medium and Low Temperature Reach-in Display Cases and Solid Doors of Reach-in Coolers and Freezers. 2007.

⁷⁷⁸ Commercial Facilities Contract Group (ComFac), 2006-2008 Direct Impact Evaluation Study ID: PUC0016.01. February 18, 2010. https://energy.mo.gov/sites/energy/files/comfac_evaluation_v1_final_report_02-18-2010.pdf.

were derived for various scenarios regarding baseline gasket efficacies and are shown in Table 16.9-1 below:

Table 16.9-1: [Door Gaskets] Reference Energy Savings by Refrigeration Type per Lin. Ft. of Door Gasket⁷⁷⁹

| Refrigerator type | Baseline 0% efficacy (kWh/ft) | Baseline 50% efficacy (kWh/ft) | Baseline 90% efficacy (kWh/ft) | Baseline 100% efficacy (kWh/ft) |
|-------------------|-------------------------------|--------------------------------|--------------------------------|---------------------------------|
| Cooler | 30 | 15 | 3 | - |
| Freezer | 228 | 114 | 23 | - |

As the PG&E analysis was performed in California with different climate zones than those in Texas, an analysis was conducted to develop an adjustment factor to associate the savings in Table 16.9-1 to Texas anticipated results. The PG&E study could not be used to determine these effects, as insufficient climate zones were researched. Therefore, the SCE study was utilized as savings in this study were determined for each of the 16 climate zones in California and were similar⁷⁸⁰ to those assessed within the PG&E results at 90 percent efficacy. A comparison was completed between the SCE energy savings and the typical meteorological year 3 (TMY3) data⁷⁸¹ to establish a cooling degree day (CDD) correlation across the 16 California climate zones. Figure 16.9-1 provides a summary comparison for coolers and Figure 16.9-2 does the same for freezers. The resulting correlations are strong, with an R² of 0.85 for coolers and an R² of 0.88 for freezers, respectively.

⁷⁷⁹ Ibid., Table 5-3.

⁷⁸⁰ The SCE ex-ante savings as reported in the PG&E report were 10.2 and 21.7 kWh/linear foot for coolers and freezers respectively. Commercial Facilities Contract Group (ComFac), 2006-2008 Direct Impact Evaluation Study ID: PUC0016.01. February 18, 2010. Table 5-3. http://www.calmac.org/publications/comfac_evaluation_v1_final_report_02-18-2010.pdf.

Modeled savings as reported in the SEC report for climate zone 4 were approximately 6 and 15 kWh/linear foot for coolers and freezers respectively.

⁷⁸¹ Available for download on the Texas Efficiency website: <http://texasefficiency.com/index.php/regulatory-filings/deemed-savings>.

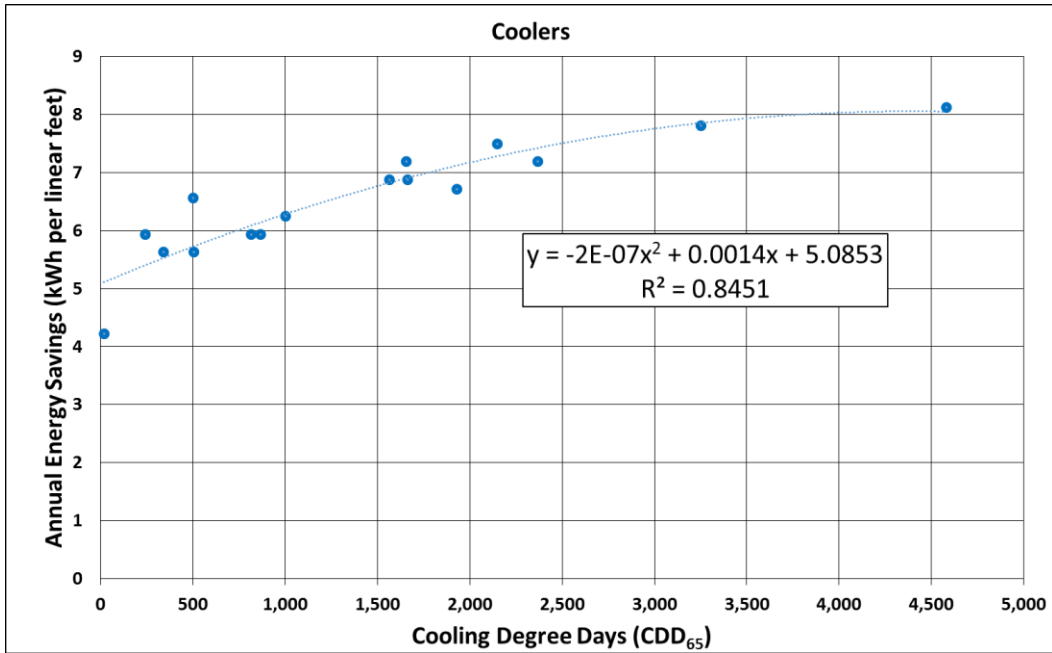


Figure 16.9-1: [Door Gaskets] Comparison of Projected Annual Energy Savings to Cooling Degree Days for All 16 California Climate Zones for Reach-In Display Cases (Coolers)

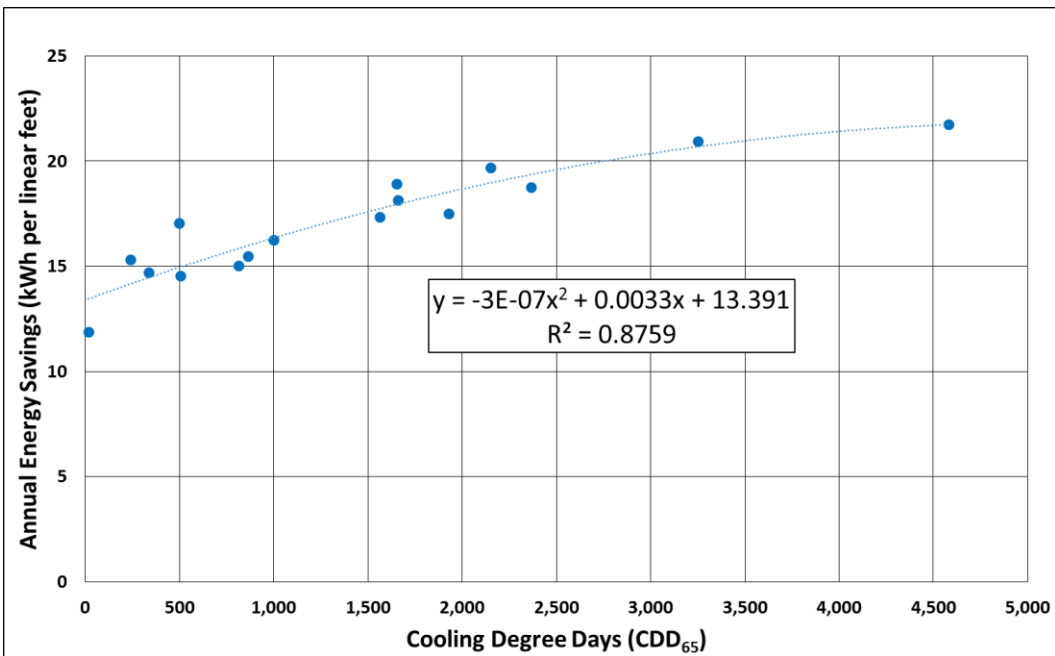


Figure 16.9-2: [Door Gaskets] Comparison of Projected Annual Energy Savings to Cooling Degree Days for All 16 California Climate Zones for Reach-In Display Cases (Freezers)

These correlations were used to adjust the energy savings and TMY3 CDDs in California to TMY3 CDDs in Texas to determine an average energy savings of 7.4 and 20.0 kWh/linear feet for coolers and freezers in Texas. Comparing the average energy savings between California and Texas, the CDD adjustment results in a 113 percent adjustment factor for coolers and a 117 percent adjustment factor for freezers. For simplicity, an average adjustment factor of 115 percent (the midpoint of 113% and 117% TX vs. CA Energy Savings values) was applied to the PG&E results at 90 percent efficacy (as shown in Table 16.9-1 above), resulting in Texas-based annual energy savings values for coolers of 3.5 kWh/linear feet and freezers of 26.5 kWh/linear feet. These results are summarized in Table 16.9-4 below:

Table 16.9-2: [Door Gaskets] Adjusted Energy Savings by Refrigeration Type per Lin. Ft. of Door Gasket

| Refrigerator type | CA CZ1-CZ16 average savings (kWh/ft) | CA average savings normalized to TX by CDD (kWh/ft) | TX vs. CA energy savings | Average CDD adjustment factor | PG&E baseline 90% efficacy (kWh/ft) | TX baseline 90% efficacy (kWh/ft) |
|-------------------|--------------------------------------|---|--------------------------|-------------------------------|-------------------------------------|-----------------------------------|
| Cooler | 6.5 | 7.4 | 113% | 115% | 3 | 3.5 |
| Freezer | 17.1 | 20.0 | 117% | | 23 | 26.5 |

Energy and Demand Savings

The energy and demand algorithms and associated input variables are listed below:

$$\text{Energy Savings } [\Delta kWh] = \frac{\Delta kWh}{ft} \times L \times CAF$$

Equation 16.9-1

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{savings}}{8,760} \times L \times DF$$

Equation 16.9-2

Where:

$$\frac{\Delta kWh}{ft} = \text{Annual CA energy savings per linear foot of gasket } [kWh/ft] = 3 \text{ for coolers and } 23 \text{ for freezers.}$$

$$L = \text{Total gasket length as measured } [ft].$$

$$CAF = \text{California to Texas climate adjustment factor} = 115\%; \text{ see Table 16.6-2.}$$

$$DF = \text{Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.9-3.}$$

Table 16.9-3: [Door Gaskets] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.000 |
| CP | 0.981 |
| 4CP | 0.974 |

16.9.2.2 Deemed Energy Savings Tables

Table 16.9-4: [Door Gaskets] Deemed Energy Savings (per Lin. Ft. of Gasket)

| Refrigerator Type | Walk-In or Reach-In Deemed Savings ($\Delta kWh/ft$) |
|-------------------|--|
| Cooler | 3.5 |
| Freezer | 26.5 |

16.9.2.3 Deemed Demand Savings Tables

Because the walk-in or reach-in cooler or freezer is kept at a constant temperature, the demand savings are estimated as the total energy savings divided evenly over the full year (8,760 hours).

Table 16.9-5: [Door Gaskets] Deemed Demand Savings (per Lin. Ft. of Gasket)

| Refrigerator Type | Walk-In or Reach-In Deemed Savings ($\Delta kW/ft$) | | |
|-------------------|---|----------|----------|
| | NCP | CP | 4CP |
| Cooler | 0.000394 | 0.000386 | 0.000384 |
| Freezer | 0.003019 | 0.002962 | 0.002941 |

16.9.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 4 years for refrigerated door gaskets, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID GrocDisp-FixtDrGask.⁷⁸²

16.9.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type (convenience store, supermarket, restaurant, refrigerated warehouse)
- Refrigerator type (walk-in or reach-in cooler or freezer)

⁷⁸² DEER READI (Remote Ex-Ante Database Interface). <http://www.deerresources.com/index.php/readi>.

- Presence of existing gasket (yes, no)
- Optional (if applicable): length of ineffective baseline gasket (ft), general description of baseline gasket condition (e.g., good, moderate, poor, non-existent), and primary reason for baseline gasket ineffectiveness (partial tear, torn and dislocated, rotted/dry, poor fit/shrink, missing, or other)
- Total gasket length in cooler (ft)
- Total gasket length in freezer (ft)

Document Revision History

Table 16.9-6: [Door Gaskets] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

16.10 HIGH SPEED DOORS FOR COLD STORAGE

16.10.1 Measure Description

This measure presents deemed savings for installation of high-speed doors for cold storage facilities. High speed automatic doors differ from regular automatic doors by increasing their closing speed. High speed doors can save energy over regular automatic and manual doors by shortening the duration that the door to the cold storage area is open.

16.10.1.1 Eligibility Criteria

Eligible equipment includes high speed doors with a minimum opening rate of 32 inches per second, a minimum closing rate of 24 inches per second, and a means to automatically reclose the door, as defined by the Door and Access Systems Manufacturers' Association, International (DASMA).⁷⁸³ The high speed doors must be installed for access to a cold storage area either from exterior conditions, such as a loading dock, or from a conditioned area, such as a non-refrigerated warehouse.

16.10.1.2 Baseline Condition

The baseline condition is a manual or non-high speed automatic door installed for access to a cold storage area.

16.10.1.3 High-Efficiency Condition

The high-efficiency condition is a high speed door installed for access to a cold storage area.

16.10.2 Energy and Demand Savings Methodology

16.10.2.1 Savings Algorithms and Input Variables

Energy and Demand Savings

Savings are calculated based on a reduction in heat gain from airflow across the door opening area. The algorithms below are modeled after equations 14 and 16 in Chapter 24: Refrigerated-Facility Loads of the 2018 ASHRAE Handbook—Refrigeration to calculate heat load associated with infiltration air exchange. This measure does not account for associated motor load or efficiencies; if the new high-speed door includes an efficient motor, reference the motor measure for savings.

⁷⁸³ DASMA Standard Specification for High Speed Doors and Grilles, definition 2.6 for High Speed Door. <https://www.dasma.com/wp-content/uploads/pubs/Standards/DASMA403.pdf>.

$$\text{Energy Savings } [\Delta kWh] = \frac{w \times h^{1.5} \times EC}{COP \times 3,412}$$

Equation 16.10-1

$$EC = \text{hours} \times 3,790 \times \frac{q_s}{A} \times \frac{1}{R_s} \times \Delta D_t \times D_f \times \Delta E$$

Equation 16.10-2

$$\text{Demand Savings } [\Delta kW] = \frac{w \times h^{1.5} \times DC}{COP \times 3,412} \times DF$$

Equation 16.10-3

$$DC = 3,790 \times \frac{q_s}{A} \times \frac{1}{R_s} \times \Delta D_t \times D_f \times \Delta E$$

Equation 16.10-4

Where:

| | | |
|-----------------|---|--|
| w | = | Width of the door opening [ft]. |
| h | = | Height of the door opening [ft]. |
| EC | = | Energy coefficient, the outcome of Equation 16.10-2 based on climate zone and cold storage application; see Table 16.10-1. |
| DC | = | Demand coefficient, the outcome of Equation 16.10-4 based on climate zone and cold storage application; see Table 16.10-1. |
| hours | = | Operating hours, 3,798. ⁷⁸⁴ |
| $3,790$ | = | Constant. ⁷⁸⁵ |
| $\frac{q_s}{A}$ | = | Sensible heat load of infiltration air per square foot of door opening [ton/ft ²]; see Table 16.10-2. |
| R_s | = | Sensible heat ratio of the infiltration air heat gain; see Table 16.10-3. |
| ΔD_t | = | Change in percent of time the doorway is open, 0.33. ⁷⁸⁶ |
| D_f | = | Doorway flow factor, varies based on Temperature delta between cold room and infiltration air, 0.8 for delta $T \geq 20^\circ\text{F}$, 1.1 for delta $T < 20^\circ\text{F}$. ⁷⁸⁷ |
| ΔE | = | Change in door effectiveness, 0.2. ⁷⁸⁸ |

⁷⁸⁴ Operating hours taken from the Texas TRM Volume 3, Table 8, hours for refrigerated warehouse.

⁷⁸⁵ From ASHRAE 2018 Refrigeration Handbook, Chapter 24-4, equation 16.

⁷⁸⁶ From ASHRAE 2018 Refrigeration Handbook, Chapter 24-4, simplification of equation 17 notes; assume baseline door open-close time is 15 seconds, and high speed door open-close time is 10 seconds, for a difference in percent of time the door is open of (15-10)/15 = 0.33.

⁷⁸⁷ ASHRAE 2018 Refrigeration Handbook, Chapter 24-4, equation 17 notes.

⁷⁸⁸ ASHRAE 2018 Refrigeration Handbook, Chapter 24-4, simplification of equation 17 notes. ASHRAE provides a range of doorway effectiveness, stating 0.95 for newly installed doors though that may quickly decrease to 0.8 or 0.85 depending on door use frequency and maintenance. Air

| | | |
|------------|---|---|
| <i>COP</i> | = | <i>Coefficient of performance, assume 2.8 COP.⁷⁸⁹</i> |
| 3,412 | = | <i>Constant to convert from Btu to kWh.</i> |
| <i>DF</i> | = | <i>Demand Factor for NCP, CP, or 4CP peak demand; see Table 16.10-4</i> |

Table 16.10-1: [High Speed Doors] Energy and Demand Factors

| Door-to Space Type | Factor | Cold room temperature | | | |
|--------------------|--------|-----------------------|---------|---------|---------|
| | | -20°F | 0°F | 20°F | 40°F |
| Unconditioned | Energy | 1,098,620 | 764,564 | 506,518 | 251,996 |
| | Demand | 293.09 | 216.28 | 151.60 | 109.15 |
| Conditioned | Energy | 783,056 | 518,199 | 322,435 | 230,311 |
| | Demand | 1.0 | 1.0 | 1.0 | 1.0 |

Table 16.10-2: [High Speed Doors] Sensible Heat Load of Infiltration Air⁷⁹⁰

| Cold Room Temperature | Infiltration Air Temperature | | |
|-----------------------|------------------------------|--------|-------|
| | Conditioned | Annual | Peak |
| | 75°F | 76°F | 104°F |
| -20°F | 1.02 | 1.03 | 1.45 |
| 0°F | 0.68 | 0.68 | 1.07 |
| 20°F | 0.42 | 0.43 | 0.75 |
| 40°F | 0.3 | 0.22 | 0.54 |

curtain effectiveness ranges from very poor to more than 0.7. The input assumptions for this measure are conservatively estimated for baseline door effectiveness of 0.7 and high speed door effectiveness of 0.9.

⁷⁸⁹ Air cooled chiller efficiency from IECC 2009.

⁷⁹⁰ From ASHRAE 2018 Refrigeration Handbook, Chapter 24-4, figure 9. Values in table are summarized to reflect average annual and summer and winter peak infiltration air Temperatures. Where infiltration air Temperatures are not shown on ASHRAE figure 9, $\frac{q_s}{A}$ is estimated by extrapolation. Values for infiltration air temperature of 75°F are used to calculate energy and demand factors for doorways between cold room and conditioned space.

Table 16.10-3: [High Speed Doors] Sensible Heat Ratio of Infiltration Air⁷⁹¹

| For energy factor, unconditioned space | | | | For energy factor, conditioned space | For demand factor, conditioned and unconditioned space |
|---|------|------|------|---|--|
| Cold Room Temperature | | | | | |
| 20°F | 0°F | 20°F | 40°F | All temps | Summer, all temps |
| 0.72 | 0.68 | 0.65 | 0.67 | 1.0 | 1.0 |

Table 16.10-4: [High Speed Doors] Demand Factors

| Peak Type | DF |
|-----------|-------|
| NCP | 1.050 |
| CP | 0.920 |
| 4CP | 0.710 |

16.10.2.2 Deemed Energy and Demand Savings Tables

There are no deemed savings tables for this measure. Please refer to the savings algorithms above.

16.10.2.3 Measure Life and Lifetime Savings

16.10.2.4 The estimated useful life (EUL) for this measure is 16 years based on Navigant's 2018 ComEd Effective Useful Life Research Report.⁷⁹² Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Climate zone
- Cold room temperature
- Doorway opening location – conditioned or unconditioned

⁷⁹¹ Sensible heat ratio determined from psychrometric chart, using values for the air properties of dry bulb Temperature and relative humidity. Relative humidity of the cold room is estimated at 90% based on ASHRAE 2018 Refrigeration Handbook, Chapter 24-4, Table 9. Energy factor values for unconditioned space are the average annual values between the expected operating hours of 8am – 6pm using TMY3 data. Demand factor values for unconditioned space are taken using the highest probability Temperatures from TRM Volume 1 and their associated relative humidity from TMY3 data. Energy and demand factor values for conditioned space assume conditioned air temperature of 75°F and 45% RH.

⁷⁹² "ComEd Effective Useful Life Research Report". Navigant. May 14, 2018. Table A-4. <https://www.icc.illinois.gov/docket/P2017-0312/documents/287811/files/501915.pdf>.

- Width and height of door

Document Revision History

Table 16.10-5: [High Speed Doors] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

17. COMMERCIAL: MISCELLANEOUS

17.1 PREMIUM EFFICIENCY MOTORS

17.1.1 Measure Description

Currently a wide variety of National Electrical Manufacturers Association (NEMA) premium efficiency motors from 1 to 500 horsepower (hp) are available. Deemed saving values for demand and energy savings associated with this measure must be for electric motors with an equivalent operating period (hours x load factor) over 1,000 hours.

17.1.1.1 Eligibility Criteria

To qualify for early retirement, the premium efficiency unit must replace an existing, full-size unit with a maximum age of 16 years. To determine the remaining useful life of an existing unit; see Table 17.1-5. To receive early retirement savings, the unit to be replaced must be functioning at the time of removal.

17.1.1.2 Baseline Condition and High Efficiency Conditions

New Construction or Replace-on-Burnout

The EISA 2007 Sec 313 adopted the new federal standard and required that electric motors that are manufactured and sold in the United States on or after December 19, 2010, to before June 1, 2016, shall have a nominal full-load efficiency that is not less than the values found in Table 17.1-4 with increased efficiency requirements for 250-500 hp motors as of June 1, 2016. These standards replace legislation commonly referred to as EP Act 1992 (the Federal Energy Policy Act of 1992). The standards can also be found in section 431.25 of the Code of Federal Regulations (10 CFR Part 431).⁷⁹³

With these changes, any 1-500 hp motor bearing the "NEMA Premium" trademark will align with national energy efficiency standards and legislation. The Federal Energy Management Program (FEMP) adopted NEMA MG 1-2006 Revision 1 2007 in its Designated Product List for federal customers.

Additionally, NEMA Premium standards include general purpose electric motors, subtype II (i.e., motors ranging from 1-200 hp and 200-500hp) including:

- U-Frame Motors
- Design C Motors
- Close-coupled pump motors

⁷⁹³ Federal Standards for Electric Motors, Table 1: Nominal Full-Load Efficiencies of General Purpose Electric Motors (Subtype I), Except Fire Pump Electric Motors, <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.431#sp10.3.431.b>.

- Footless motors
- Vertical solid shaft normal thrust (tested in a horizontal configuration)
- 8-pole motors
- All poly-phase motors with voltages up to 600 volts other than 230/460 volts (230/460-volt motors are covered by EAct-92)

Under these legislative changes, 200-500 hp and Subtype II motors baselines are to be based on the minimum efficiency allowed under the EAct⁷⁹⁴ (Table 17.1-4) and are thus no longer equivalent to pre-1992/pre-EAct defaults.

Early Retirement

The baseline for early retirement projects is the nameplate efficiency of the existing motor to be replaced, if known. If the nameplate is illegible and the in-situ efficiency cannot be determined, then the baseline should be based on the minimum efficiency allowed under the EAct,⁷⁹⁵ as listed in Table 17.1-6.

NEMA Premium Efficiency motor levels continue to be industry standard for minimum-efficiency levels. The savings calculations assume that the minimum motor efficiency for replacement motors for both replace-on-burnout and early retirement projects exceeds that listed in Table 17.1-4.

For early retirement, the maximum age of an eligible piece of equipment is capped at the point at which it is expected that 75 percent of the equipment has failed (17 years). In situations where the age of the unit exceeds the 75 percent failure age, ROB savings should be applied. This cap prevents early retirement savings from being applied to projects where the age of the equipment greatly exceeds the estimated useful life of the measure. 1-200 hp motors manufactured as of December 19, 2020 and 250-500 hp motors manufactured as of June 1, 2016 are not eligible for early retirement.

17.1.2 Energy and Demand Savings Methodology

Actual motor operating hours are expected to be used to calculate savings. Every effort should be made to capture the estimated operating hours. Short and/or long-term metering can be used to verify estimates. If metering is not possible, interviews with facility operators and review of operations logs should be conducted to obtain an estimate of actual operating hours. If there is not sufficient information to accurately estimate operating hours, then the annual operating hours in Table 17.1-1 or Table 17.1-2 can be used.

⁷⁹⁴ Federal Standards for Electric Motors, Table 4: Nominal Full-Load Efficiencies of NEMA Design B General Purpose Electric Motors (Subtype I and II), Except Fire Pump Electric Motors, <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.431#sp10.3.431.b>.

⁷⁹⁵ Federal Standards for Electric Motors, Tables 3 (≤ 200 hp), and 4 (> 200hp), <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.431#sp10.3.431.b>.

17.1.2.1 Savings Algorithms and Input Variables

New Construction or Replace-on-Burnout

$$\text{Energy Savings } [\Delta kWh] = hp \times 0.746 \times LF \times \left(\frac{1}{\eta_{base,ROB}} - \frac{1}{\eta_{post}} \right) \times \text{hours}$$

Equation 17.1-1

HVAC Applications:

$$\text{Demand Savings } [\Delta kW] = \left(\frac{\Delta kWh}{\text{hours}} \right) \times DF$$

Equation 17.1-2

Industrial Applications⁷⁹⁶:

$$\text{Demand Savings } [\Delta kW] = \left(\frac{\Delta kWh}{8,760} \right)$$

Equation 17.1-3

Where:

| | | |
|-------------------------------------|---|--|
| <i>hp</i> | = | <i>Nameplate horsepower data of the motor.</i> |
| <i>0.746</i> | = | <i>Constant to convert from hp to kWh.⁷⁹⁷</i> |
| <i>LF</i> | = | <i>Estimated load factor; if unknown, see Table 17.1-1 or Table 17.1-2.</i> |
| <i>$\eta_{base,ROB}$</i> | = | <i>Assumed original motor efficiency [%]; see Table 17.1-4.⁷⁹⁸</i> |
| <i>η_{post}</i> | = | <i>Efficiency of the newly installed motor [%].</i> |
| <i>hours</i> | = | <i>Estimated annual operating hours; if unknown, see Table 17.1-1 or Table 17.1-2.</i> |
| <i>DF</i> | = | <i>Demand Factor for NCP, CP, or 4CP peak demand; see Table 17.1-1.</i> |
| <i>kWh_{savings,ROB}</i> | = | <i>Total energy savings for a new construction or ROB project.</i> |
| <i>kW_{savings,ROB}</i> | = | <i>Total demand savings for a new construction or ROB project.</i> |
| <i>8,760</i> | = | <i>Total hours per year.</i> |

⁷⁹⁶ Assumes 3-shift operating schedule.

⁷⁹⁷ U.S. DOE, Technical Support Document, "Energy Efficiency Program for Commercial Equipment: Energy Conservation Standards for Electric Motors, 10.2.2.1 Motor Capacity." Download TSD at: <https://www.mercatus.org/system/files/1904-AC28-TSD-Electric-Motors.pdf>.

⁷⁹⁸ In the case of rewind motors, in-situ efficiency may be reduced by a percentage as found in Table 17.1-3.

Table 17.1-1: [Premium Motors] HVAC Assumptions by Building Type

| Building Type | Load Factor ⁷⁹⁹ | DF ⁸⁰⁰ | HVAC Fan Hours ⁸⁰¹ |
|--|----------------------------|-------------------|-------------------------------|
| Education: K-12 school | 0.75 | 1.00 | 4,173 |
| Education: College/university | | | 4,590 |
| Food service: Full-service restaurant | | | 5,256 |
| Food service: Quick-service restaurant | | | 6,716 |
| Healthcare: Inpatient | | | 8,760 |
| Mercantile: All retail | | | 5,548 |
| Office: Large (>30k SqFt) | | | 4,424 |
| Office: Small (≤30k SqFt) | | | 4,006 |

Table 17.1-2: [Premium Motors] Industrial Assumptions by Building Type

| Industrial Processing (hp) | Load Factor ⁸⁰² | Hours ⁸⁰³ | | | | | |
|----------------------------|----------------------------|----------------------|-------|--------|--------------------|-----------------|-------|
| | | Chem | Paper | Metals | Petroleum Refinery | Food Production | Other |
| 1-5 | 0.54 | 4,082 | 3,997 | 4,377 | 1,582 | 3,829 | 2,283 |
| 6-20 | 0.51 | 4,910 | 4,634 | 4,140 | 1,944 | 3,949 | 3,043 |
| 21-50 | 0.60 | 4,873 | 5,481 | 4,854 | 3,025 | 4,927 | 3,530 |
| 51-100 | 0.54 | 5,853 | 6,741 | 6,698 | 3,763 | 5,524 | 4,732 |
| 101-200 | 0.75 | 5,868 | 6,669 | 7,362 | 4,170 | 5,055 | 4,174 |
| 201-500 | 0.58 | 5,474 | 6,975 | 7,114 | 5,311 | 3,711 | 5,396 |
| 501-1,000 | 0.58 | 7,495 | 7,255 | 7,750 | 5,934 | 5,260 | 8,157 |
| > 1,000 | 0.58 | 7,693 | 8,294 | 7,198 | 6,859 | 6,240 | 2,601 |

⁷⁹⁹ Itron 2004-2005 DEER Update Study, Dec 2005; Table 3-25.

http://deeresources.com/files/deer2005/downloads/DEER2005UpdateFinalReport_ItronVersion.pdf.

⁸⁰⁰ Commercial Prototype Building Models HVAC operating schedules for hours ending 15-18. U.S. Department of Energy.

https://www.energycodes.gov/development/commercial/prototype_models.

⁸⁰¹ Assumed equivalent to 13.5 HVAC Variable Frequency Drive Hours per Building Type

⁸⁰² United States Industrial Electric Motor Systems Market Opportunities Assessment, Dec 2002; Table 1-19.

https://www1.eere.energy.gov/manufacturing/tech_assistance/pdfs/mtrmkt.pdf.

⁸⁰³ United States Industrial Electric Motor Systems Market Opportunities Assessment, Dec 2002; Table 1-15.

https://www1.eere.energy.gov/manufacturing/tech_assistance/pdfs/mtrmkt.pdf.

Table 17.1-3: [Premium Motors] Rewound Motor Efficiency Reduction Factors⁸⁰⁴

| Motor Horsepower | Efficiency Reduction Factor |
|------------------|-----------------------------|
| < 40 | 0.010 |
| ≥ 40 | 0.005 |

Table 17.1-4: [Premium Motors] NC/ROB Baseline Efficiencies by Motor Size (%)^{805,806,807}

| hp | Open Motors: $\eta_{\text{baseline, ROB}}$ | | | Closed Motors: $\eta_{\text{baseline, ROB}}$ | | |
|-----|--|--------|--------|--|--------|--------|
| | 6-Pole | 4-Pole | 2-Pole | 6-Pole | 4-Pole | 2-Pole |
| 1 | 82.5 | 85.5 | 77.0 | 82.5 | 85.5 | 77.0 |
| 1.5 | 86.5 | 86.5 | 84.0 | 87.5 | 86.5 | 84.0 |
| 2 | 87.5 | 86.5 | 85.5 | 88.5 | 86.5 | 85.5 |
| 3 | 88.5 | 89.5 | 85.5 | 89.5 | 89.5 | 86.5 |
| 5 | 89.5 | 89.5 | 86.5 | 89.5 | 89.5 | 88.5 |
| 7.5 | 90.2 | 91.0 | 88.5 | 91.0 | 91.7 | 89.5 |
| 10 | 91.7 | 91.7 | 89.5 | 91.0 | 91.7 | 90.2 |
| 15 | 91.7 | 93.0 | 90.2 | 91.7 | 92.4 | 91.0 |
| 20 | 92.4 | 93.0 | 91.0 | 91.7 | 93.0 | 91.0 |
| 25 | 93.0 | 93.6 | 91.7 | 93.0 | 93.6 | 91.7 |
| 30 | 93.6 | 94.1 | 91.7 | 93.0 | 93.6 | 91.7 |
| 40 | 94.1 | 94.1 | 92.4 | 94.1 | 94.1 | 92.4 |
| 50 | 94.1 | 94.5 | 93.0 | 94.1 | 94.5 | 93.0 |
| 60 | 94.5 | 95.0 | 93.6 | 94.5 | 95.0 | 93.6 |
| 75 | 94.5 | 95.0 | 93.6 | 94.5 | 95.4 | 93.6 |
| 100 | 95.0 | 95.4 | 93.6 | 95.0 | 95.4 | 94.1 |
| 125 | 95.0 | 95.4 | 94.1 | 95.0 | 95.4 | 95.0 |
| 150 | 95.4 | 95.8 | 94.1 | 95.8 | 95.8 | 95.0 |
| 200 | 95.4 | 95.8 | 95.0 | 95.8 | 96.2 | 95.4 |
| 250 | 95.8 | 95.8 | 95.0 | 95.8 | 96.2 | 95.8 |
| 300 | 95.8 | 95.8 | 95.4 | 95.8 | 96.2 | 95.8 |
| 350 | 95.8 | 95.8 | 95.4 | 95.8 | 96.2 | 95.8 |

⁸⁰⁴ U.S. DOE, Technical Support Document, “Energy Efficiency Program for Commercial Equipment: Energy Conservation Standards for Electric Motors, 8.2.2.1 Annual Energy Consumption.” Download TSD at: <https://www.mercatus.org/system/files/1904-AC28-TSD-Electric-Motors.pdf>.

⁸⁰⁵ Ibid.

⁸⁰⁶ Federal Standards for Electric Motors, Tables 1 and 5, <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.431#sp10.3.431.b>.

⁸⁰⁷ For unlisted motor horsepower values, round down to the next lowest horsepower value.

| hp | Open Motors: $\eta_{\text{baseline, ROB}}$ | | | Closed Motors: $\eta_{\text{baseline, ROB}}$ | | |
|-----|--|--------|--------|--|--------|--------|
| | 6-Pole | 4-Pole | 2-Pole | 6-Pole | 4-Pole | 2-Pole |
| 400 | - | 95.8 | 95.8 | - | 96.2 | 95.8 |
| 450 | - | 96.2 | 96.2 | - | 96.2 | 95.8 |
| 500 | - | 96.2 | 96.2 | - | 96.2 | 95.8 |

Early Retirement

Annual energy (kWh) and peak demand (kW) savings must be calculated separately for two time periods:

1. The estimated remaining life of the equipment that is being removed, designated the remaining useful life (RUL), and
2. The remaining time in the EUL period (EUL – RUL)

Annual energy and peak demand savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

Where:

RUL = Remaining Useful Life; see Table 17.1-5. If unknown, assume the age of the replaced unit is equal to the EUL resulting in a default RUL of 2.0 years.

EUL = Estimated Useful Life = 15 years.

Table 17.1-5: [Premium Motors] Remaining Useful Life (RUL) of Replaced Motor⁸⁰⁸

| Age of Replaced Motor (years) | RUL (years) | Age of Replaced Motor (years) | RUL (years) | Age of Replaced Motor (years) | RUL (years) |
|-------------------------------|-------------|-------------------------------|-------------|-------------------------------|-------------|
| 1 | 13.9 | 7 | 7.9 | 13 | 3.0 |
| 2 | 12.9 | 8 | 6.9 | 14 | 2.5 |
| 3 | 11.9 | 9 | 5.9 | 15 | 2.0 |
| 4 | 10.9 | 10 | 5.0 | 16 | 1.0 |
| 5 | 9.9 | 11 | 4.2 | 17 ⁸⁰⁹ | 0.0 |
| 6 | 8.9 | 12 | 3.6 | | |

⁸⁰⁸ Current federal standard effective date is 12/19/2010. Existing systems manufactured after this date are not eligible to use the early retirement baseline.

⁸⁰⁹ RULs are capped at the 75th percentile of equipment age, 17 years, as determined based on DOE survival curves. Systems older than 17 years should use the ROB baseline. See the January 2015 memo, "Considerations for early replacement of residential equipment," for further detail.

Derivation of RULs

Premium Efficiency Motors have an estimated useful life of 15 years. This estimate is consistent with the age at which approximately 50 percent of the motors installed in a given year will no longer be in service, as described by the survival function for a general fan or air compressor application in Figure 17.1-1.

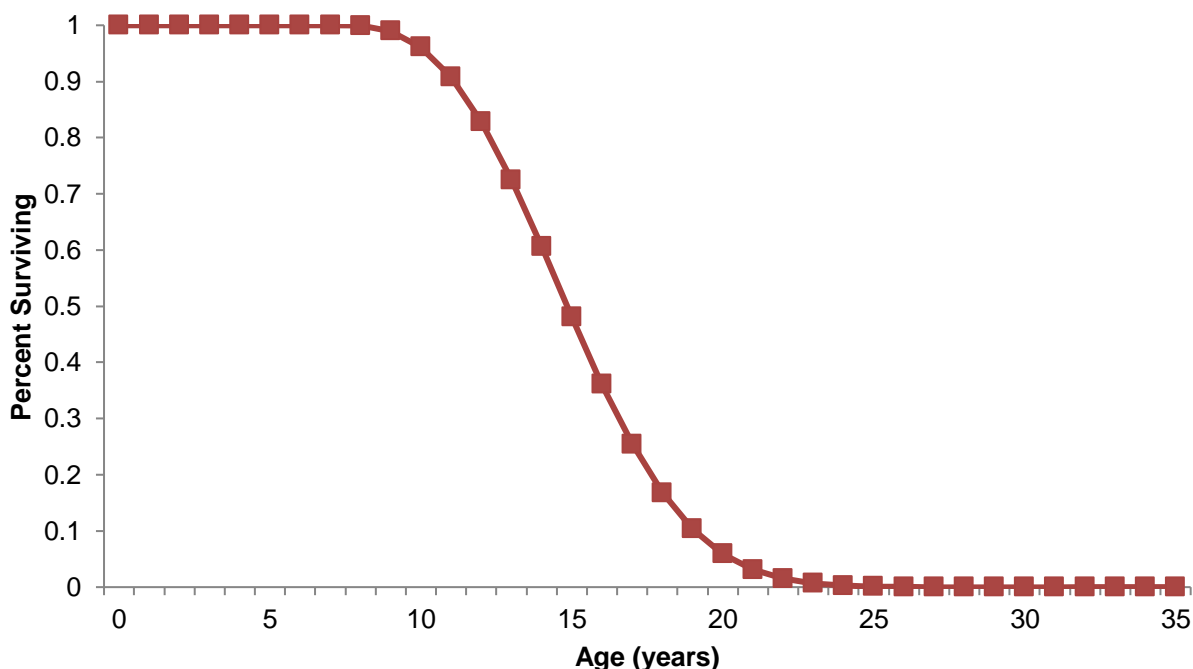


Figure 17.1-1: [Premium Motors] Survival Function⁸¹⁰

The method for estimating the remaining useful life (RUL) of a replaced system uses the age of the existing system to re-estimate the projected unit lifetime based on the survival function shown in Figure 17.1-1. The age of the motor being replaced is found on the horizontal axis, and the corresponding percentage of surviving motors is determined from the chart. The surviving percentage value is then divided in half, creating a new estimated useful lifetime applicable to the current unit age. Then, the age (year) that corresponds to this new percentage is read from the chart. RUL is estimated as the difference between that age and the current age of the system being replaced.

For example, assume a motor being replaced is 15 years old (the estimated useful life). The corresponding percent surviving value is approximately 50 percent. Half of 50 percent is 25 percent. The age corresponding to 25 percent on the chart is approximately 17 years. Therefore, the RUL of the motor being replaced is $(17 - 15) = 2$ years.

⁸¹⁰ Department of Energy, Federal Register, 76 Final Rule 57516, Technical Support Document: 8.2.3.1 Estimated Survival Function. September 15, 2011. http://www1.eere.energy.gov/buildings/appliance_standards/pdfs/refrig_finalrule_tsd.pdf.

Energy Savings Algorithms

For the RUL period:

$$kWh_{savings,RUL} = hp \times 0.746 \times LF \times \left(\frac{1}{\eta_{base,ER}} - \frac{1}{\eta_{post}} \right) \times hours$$

Equation 17.1-4

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project.

$$kWh_{savings,EUL} = hp \times 0.746 \times LF \times \left(\frac{1}{\eta_{base,ROB}} - \frac{1}{\eta_{post}} \right) \times hours$$

Equation 17.1-5

It follows that total lifetime energy savings for early retirement projects are then determined by adding the savings calculated under the two preceding equations:

$$kWh_{savings,ER} = kWh_{savings,RUL} \times RUL + kWh_{savings,EUL} \times (EUL - RUL)$$

Equation 17.1-6

Demand Savings Algorithms

To calculate demand savings for the early retirement of a motor, a similar methodology is used as for replace-on-burnout installations, with separate savings calculated for the remaining useful life of the unit, and the remainder of the EUL as outlined in the section above.

For the RUL period:

HVAC Applications:

$$kW_{savings,RUL} = \frac{kWh_{savings,RUL}}{hours} \times DF$$

Equation 17.1-7

Industrial Applications:

$$kW_{savings,RUL} = \frac{kWh_{savings,RUL}}{8,760}$$

Equation 17.1-8

For the remaining time in the EUL period, calculate annual savings as you would for a replace-on-burnout project:

HVAC Applications:

$$kW_{savings,EUL} = \frac{kWh_{savings,EUL}}{hours} \times DF$$

Industrial Applications:

$$kW_{savings,EUL} = \frac{kWh_{savings,EUL}}{8,760}$$

Equation 17.1-10

Annual deemed peak demand savings are calculated by weighting the early retirement and replace-on-burnout savings by the RUL of the unit and the remainder of the EUL period, as outlined in Section 22.1.

$$kW_{savings,ER} = kW_{savings,RUL} \times RUL + kW_{savings,EUL} \times (EUL - RUL)$$

Equation 17.1-11

Where:

$\eta_{base,ER}$ = Assumed original motor efficiency for RUL period; if unknown, see Table 17.1-6 or Table 17.1-7,⁸¹¹

$kWh_{savings,RUL}$ = Energy savings for RUL period in an ER project.

$kWh_{savings,EUL}$ = Energy savings for remaining EUL period in an ER project.

$kW_{savings,RUL}$ = Demand savings for RUL period in an ER project.

$kW_{savings,EUL}$ = Demand savings for remaining EUL period in an ER project.

$kWh_{savings,ER}$ = Total energy savings for an ER project.

$kW_{savings,ER}$ = Total demand savings for an ER project.

Table 17.1-6: [Premium Motors] Early Retirement Baseline Efficiencies by Motor Size for 1-200 hp Motors Manufactured Prior to December 19, 2010 (%)^{812,813}

| hp | Open Motors: $\eta_{baseline, ER}$ | | | Closed Motors: $\eta_{baseline, ER}$ | | |
|-----|------------------------------------|--------|--------|--------------------------------------|--------|--------|
| | 6-Pole | 4-Pole | 2-Pole | 6-Pole | 4-Pole | 2-Pole |
| 1 | 80.0 | 82.5 | 75.5 | 80.0 | 82.5 | 75.5 |
| 1.5 | 84.0 | 84.0 | 82.5 | 85.5 | 84.0 | 82.5 |
| 2 | 85.5 | 84.0 | 84.0 | 86.5 | 84.0 | 84.0 |
| 3 | 86.5 | 86.5 | 84.0 | 87.5 | 87.5 | 85.5 |
| 5 | 87.5 | 87.5 | 85.5 | 87.5 | 87.5 | 87.5 |
| 7.5 | 88.5 | 88.5 | 87.5 | 89.5 | 89.5 | 88.5 |
| 10 | 90.2 | 89.5 | 88.5 | 89.5 | 89.5 | 89.5 |
| 15 | 90.2 | 91.0 | 89.5 | 90.2 | 91.0 | 90.2 |

⁸¹¹ Ibid.

⁸¹² Federal Standards for Electric Motors, Table 3, <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.431#sp10.3.431.b>.

⁸¹³ For unlisted motor horsepower values, round down to the next lowest horsepower value.

| hp | Open Motors: $\eta_{\text{baseline, ER}}$ | | | Closed Motors: $\eta_{\text{baseline, ER}}$ | | |
|-----|---|--------|--------|---|--------|--------|
| | 6-Pole | 4-Pole | 2-Pole | 6-Pole | 4-Pole | 2-Pole |
| 20 | 91.0 | 91.0 | 90.2 | 90.2 | 91.0 | 90.2 |
| 25 | 91.7 | 91.7 | 91.0 | 91.7 | 92.4 | 91.0 |
| 30 | 92.4 | 92.4 | 91.0 | 91.7 | 92.4 | 91.0 |
| 40 | 93.0 | 93.0 | 91.7 | 93.0 | 93.0 | 91.7 |
| 50 | 93.0 | 93.0 | 92.4 | 93.0 | 93.0 | 92.4 |
| 60 | 93.6 | 93.6 | 93.0 | 93.6 | 93.6 | 93.0 |
| 75 | 93.6 | 94.1 | 93.0 | 93.6 | 94.1 | 93.0 |
| 100 | 94.1 | 94.1 | 93.0 | 94.1 | 94.5 | 93.6 |
| 125 | 94.1 | 94.5 | 93.6 | 94.1 | 94.5 | 94.5 |
| 150 | 94.5 | 95.0 | 93.6 | 95.0 | 95.0 | 94.5 |
| 200 | 94.5 | 95.0 | 94.5 | 95.0 | 95.0 | 95.0 |

Table 17.1-7: [Premium Motors] Early Retirement Baseline Efficiencies by Motor Size for 250-500 hp Motors Manufactured Prior to June 1, 2016 (%)^{814,815}

| hp | Open Motors: $\eta_{\text{baseline, ER}}$ | | | Closed Motors: $\eta_{\text{baseline, ER}}$ | | |
|-----|---|--------|--------|---|--------|--------|
| | 6-Pole | 4-Pole | 2-Pole | 6-Pole | 4-Pole | 2-Pole |
| 250 | 95.4 | 95.4 | 94.5 | 95.0 | 95.0 | 95.4 |
| 300 | 95.4 | 95.4 | 95.0 | 95.0 | 95.4 | 95.4 |
| 350 | 95.4 | 95.4 | 95.0 | 95.0 | 95.4 | 95.4 |
| 400 | - | 95.4 | 95.4 | - | 95.4 | 95.4 |
| 450 | - | 95.8 | 95.8 | - | 95.4 | 95.4 |
| 500 | - | 95.8 | 95.8 | - | 95.8 | 95.4 |

17.1.2.2 Deemed Energy and Demand Savings Tables

There are no deemed savings tables for this measure.

17.1.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years for premium efficiency motors.⁸¹⁶

⁸¹⁴ Federal Standards for Electric Motors, Table 4, <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.431#sp10.3.431.b>.

⁸¹⁵ For unlisted motor horsepower values, round down to the next lowest horsepower value.

⁸¹⁶ U.S. DOE, Technical Support Document, "Energy Efficiency Program for Commercial Equipment: Energy Conservation Standards for Electric Motors," Median of "Table 8.2.23 Average Application Lifetime." Download TSD at: <https://www.mercatus.org/system/files/1904-AC28-TSD-Electric-Motors.pdf>.

17.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- The project type of the installation (new construction, replace-on-burnout, or early retirement)
- Motor quantity
- Estimated annual operating hours and estimated load factor
- Horsepower
- Number of poles in and horsepower of original motor
- Newly installed motor efficiency (%)
- Description of motor service application
- Photograph demonstrating functionality of existing equipment and/or customer responses to survey questionnaire documenting the condition of the replaced unit and their motivation for measure replacement for early retirement eligibility determination (early retirement only)

Document Revision History

Table 17.1-8: [Premium Motors] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | Aligned building type names across all commercial measures. Incremented RUL table for code compliance. |
| FY 2026 | No revision. |

17.2 PUMP-OFF CONTROLLERS

17.2.1 Measure Description

Pump-off Controllers (POC) are micro-processor-based devices that continuously monitor pump down conditions, which is the condition when the fluid in the well bore is insufficient to warrant continued pumping. These controllers are used to shut down the pump when the fluid falls below a certain level and “fluid pounding”⁸¹⁷ occurs. POCs save energy by optimizing the pump run-times to match the flow conditions of the well.

17.2.1.1 Eligibility Criteria

The POC measure is only available as a retrofit measure for existing wells (wells with an existing API number⁸¹⁸ prior to September 11th, 2014) with rod pumps using 15 hp or larger motors operating on time clock controls or less efficient devices. These cannot be integrated with a variable frequency drive, and only apply to POCs using load cells, which measure the weight on the rod string for greater precision. Additionally, the POC must control a conventional well (above ground, vertical, with a standard induction motor of 480V or less).

17.2.1.2 Baseline Condition

The baseline condition is an existing conventional well (with an API number prior to September 11th, 2014) with rod pumps operating on time clock controls or less efficient control devices.

17.2.1.3 High-Efficiency Condition

The efficient condition is the same well, retrofitted with a pump-off controller.

17.2.2 Energy and Demand Savings Methodology

17.2.2.1 Savings Algorithms and Input Variables

Two main sources were referenced to develop the savings methods for the POC measure: Electrical Savings in Oil Production (SPE 16363),⁸¹⁹ which identified a relationship between volumetric efficiency and pump run times, and the 2006-2008 Evaluation Report for PG&E Fabrication, Process, and Manufacturing Contract Group,⁸²⁰ which showed a reduction in savings from the SPE 16363 paper. These

⁸¹⁷ Fluid pounding occurs when the downhole pump rate exceeds the production rate of the formation. The pump strikes the top of the fluid column on the downstroke causing extreme shock loading of the components which can result in premature equipment failure.

⁸¹⁸ The API number is a unique, permanent identifier assigned by the American Petroleum Institute. The API number should correspond to a well that was in existence prior to the date of PUCT Docket 42551.

⁸¹⁹ Bullock, J.E. “SPE 16363 Electrical Savings in Oil Production,” (paper presented at the Society of Petroleum Engineers California Regional Meeting held in Ventura, California, April 8-10, 1987).

⁸²⁰ 2006-2008 Evaluation Report for PG&E Fabrication, Process and Manufacturing Contract Group. Calmac Study ID: CPU0017.01. Itron, Inc. Submitted to California Public Utilities Commission. February 3, 2010.

two methods were the basis of the current savings calculations and deemed inputs listed below.

Energy Savings

Deemed savings are calculated based on the following algorithms:

$$\text{Energy Savings } [\Delta kWh] = kW_{avg} * (\text{TimeClock}\%On - \text{POC}\%On) * 8,760$$

Equation 17.2-1

The inputs for the energy and peak coincident demand savings are listed below:

$$kW_{avg} = HP \times 0.746 \times \frac{LF/ME}{SRME}$$

Equation 17.2-2

$$\text{POC}\%On = \frac{\text{Run}_{constant} + \text{Run}_{coefficient} \times VE \times \text{TC}\%On \times 100}{100}$$

Equation 17.2-3 ⁸²¹

Where:

| | | |
|----------------------------|---|--|
| kW_{avg} | = | The demand used by each rod pump. |
| HP | = | Rated pump motor horsepower. |
| 0.746 | = | Constant to convert from HP to kW. |
| LF | = | Motor load factor – ratio of average demand to maximum demand; see Table 17.2-1. |
| ME | = | Motor efficiency, based on NEMA Standard Efficiency Motor; see Table 17.2-2. |
| $SRME$ | = | Mechanical efficiency of sucker rod pump; see Table 17.2-1. |
| $\text{TC}\%On$ | = | Stipulated baseline timeclock setting; see Table 17.2-1. |
| $\text{Run}_{constant}$ | = | 8.336, derived from SPE 16363. ⁸²² |
| $\text{Run}_{coefficient}$ | = | 0.956, derived from SPE 16363. ⁸²³ |
| VE | = | Volumetric efficiency, or average well gross production divided by theoretical production. |

⁸²¹ This equation from the petition deviates from that in SPE 16363 but will provide conservative savings estimates. The equation will be updated and made consistent when this measure is updated with field data. The correct equation term is $(\text{Run}_{constant} + \text{Run}_{coefficient} \times \text{VolumetricEfficiency}\%)$ with the volumetric efficiency expressed as percent value not a fraction (i.e., 25 not 0.25 for 25%).

⁸²² Bullock, J.E. "SPE 16363 Electrical Savings in Oil Production," (paper presented at the Society of Petroleum Engineers California Regional Meeting held in Ventura, California, April 8-10, 1987).

⁸²³ Ibid.

Table 17.2-1: [Pump-Off Controllers] Deemed Variables for Energy and Demand Savings Calculations

| Variable | Deemed Values |
|----------------------------------|--------------------|
| LF (Load Factor) | 25% ⁸²⁴ |
| ME (motor efficiency) | See Table 17.2-2 |
| SME (pump mechanical efficiency) | 95% ⁸²⁵ |
| Timeclock%On | 65% ⁸²⁶ |

Table 17.2-2: [Pump-Off Controllers] NEMA Premium Efficiency Motor Efficiencies⁸²⁷

| Motor Horsepower | Nominal Full Load Efficiency | | | | | |
|---------------------|------------------------------|----------|----------|------------------------|----------|----------|
| | Open Motors (ODP) | | | Enclosed Motors (TEFC) | | |
| | 6 poles | 4 poles | 2 poles | 6 poles | 4 poles | 2 poles |
| | 1200 rpm | 1800 rpm | 3600 rpm | 1200 rpm | 1800 rpm | 3600 rpm |
| 15 | 91.7% | 93.0% | 90.2% | 91.7% | 92.4% | 91.0% |
| 20 | 92.4% | 93.0% | 91.0% | 91.7% | 93.0% | 91.0% |
| 25 | 93.0% | 93.6% | 91.7% | 93.0% | 93.6% | 91.7% |
| 30 | 93.6% | 94.1% | 91.7% | 93.0% | 93.6% | 91.7% |
| 40 | 94.1% | 94.1% | 92.4% | 94.1% | 94.1% | 92.4% |
| 50 | 94.1% | 94.5% | 93.0% | 94.1% | 94.5% | 93.0% |
| 60 | 94.5% | 95.0% | 93.6% | 94.5% | 95.0% | 93.6% |
| 75 | 94.5% | 95.0% | 93.6% | 94.5% | 95.4% | 93.6% |
| 100 | 95.0% | 95.4% | 93.6% | 95.0% | 95.4% | 94.1% |
| 125 | 95.0% | 95.4% | 94.1% | 95.0% | 95.4% | 95.0% |
| 150 | 95.4% | 95.8% | 94.1% | 95.8% | 95.8% | 95.0% |
| 200 | 95.4% | 95.8% | 95.0% | 95.8% | 96.2% | 95.4% |

⁸²⁴ Comprehensive Process and Impact Evaluation of the (Xcel Energy) Colorado Motor and Drive Efficiency Program, FINAL. TetraTech. March 28, 2011. Adjusted based on Field Measurements provided by ADM Associates, based on 2010 custom projects.

⁸²⁵ Engineering estimate for standard gearbox efficiency.

⁸²⁶ A TimeClock%On of 80% is typical from observations in other jurisdictions, but that was adjusted to 65% for a conservative estimate.

⁸²⁷ DOE Final Rule regarding energy conservation standards for electric motors. 79 FR 30933. Full-Load Efficiencies for General Purpose Electric Motors [Subtype I] https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=6&action=viewlive.

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{\Delta kWh}{8,760}$$

Equation 17.2-5⁸²⁸

Where:

$$8,760 = \text{Total hours per year.}$$

17.2.2.2 Deemed Energy Savings Tables

There are no deemed savings tables for this measure.

17.2.2.3 Deemed Demand Savings Tables

There are no deemed savings tables for this measure.

17.2.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 15 years for pump-off controllers.⁸²⁹

17.2.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Motor manufacturer
- Motor model number
- Rated motor horsepower
- Motor type (TEFC or ODP)
- Rated motor RPM
- Baseline control type and timeclock % on time (or actual on-time schedule)
- Volumetric efficiency
- Field data on actual energy use and post-run times if available

⁸²⁸ The equations in the petition for peak demand simplify to the equation shown.

⁸²⁹ CPUC 2006-2008 Industrial Impact Evaluation "SCIA_06-08_Final_Report_Appendix_D-5": An EUL of 15 years was used for the ex-post savings, consistent with the SPC – Custom Measures and System Controls categories in the CPUC Energy Efficiency Policy Manual (Version 2) and with DEER values for an energy management control system.

Document Revision History

Table 17.2-3: [Pump-Off Controllers] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

17.3 ENERGY STAR® POOL PUMPS

17.3.1 Measure Description

This measure involves the replacement of a single-speed pool pump with an ENERGY STAR-certified variable speed pool pump.

17.3.1.1 Eligibility Criteria

This measure applies to all commercial applications, indoor or outdoor, with a pump size up to 3 hp; larger sizes should be implemented through a custom program. Motor-only retrofits are not eligible. Ineligible pump products include waterfall, integral cartridge filter, integral sand filter, storable electric spa, and rigid electric spa.⁸³⁰

Multi-speed pool pumps are not permitted. The multi-speed pump uses an induction motor that functions as two motors in one, with full-speed and half-speed options. Multi-speed pumps may enable significant energy savings. However, if the half-speed motor is unable to complete the required water circulation task, the larger motor will operate exclusively. Having only two speed-choices limits the ability of the pump motor to fine-tune the flow rates required for maximum energy savings.⁸³¹ The default pump curves provided in the ENERGY STAR Pool Pump Savings Calculator indicate that the motor operating at half-speed will be unable to meet the minimum turnover requirements for commercial pool operation as mandated by Texas Administrative Code.

17.3.1.2 Baseline Condition

The baseline is assumed to be a new pool pump that is compliant with the current federal standard, effective July 19, 2021.⁸³² Weighted Energy Factor (WEF) requirements are based on rated hydraulic horsepower (hhp).

Table 17.3-1: [Pool Pumps] Baseline Condition – Federal Standard Effective July 19, 2021

| Pump Sub-Type | Size Class | WEF |
|------------------------------------|-------------------------------|------------------------------|
| Self-priming (inground) pool pumps | Extra Small (hhp ≤ 0.13) | WEF = 5.55 |
| | Small (hhp > 0.13 to < 0.711) | WEF = -1.30 x ln(hhp) + 2.90 |
| | Standard (hhp ≥ 0.711) | WEF = -2.30 x ln(hhp) + 6.59 |

⁸³⁰ These pump products are ineligible for ENERGY STAR v3.0

certification: <https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.1%20Pool%20Pumps%20Final%20Specification%200.pdf>.

⁸³¹ Hunt, A. & Easley, S., 2012, "Measure Guideline: Replacing Single-Speed Pool Pumps with Variable Speed Pumps for Energy Savings." Building America Retrofit Alliance (BARA), U.S. U.S. DOE. May/. <http://www.nrel.gov/docs/fy12osti/54242.pdf>.

⁸³² Federal standard for dedicated purpose pool pumps.

<https://www.ecfr.gov/current/title-10/section-431.465>.

17.3.1.3 High Efficiency Condition

The high efficiency condition is a 1 to 5 hp variable speed pool pump that is compliant with the current ENERGY STAR specification v3.1, effective July 19, 2021.⁸³³

Table 17.3-2: [Pool Pumps] ENERGY STAR Pool Pumps – Energy Efficiency Level

| Pump Subtype | Size class | ENERGY STAR |
|------------------------------------|-------------------------------|------------------------------|
| Self-priming (inground) pool pumps | Extra small (hhp ≤ 0.13) | WEF ≥ 13.40 |
| | Small (hhp > 0.13 to < 0.711) | WEF ≥ -2.45 x ln(hhp) + 8.40 |
| | Standard (hhp ≥ 0.711) | |

Energy and Demand Savings Methodology

Savings for this measure are based on methods and input assumptions from the ENERGY STAR Pool Pump Savings Calculator. ENERGY STAR has not published updates to the calculator for version 2.0 and therefore the deemed input assumptions that follow are based on certification version 1.0. This measure will be updated when the ENERGY STAR Pool Pump Savings Calculator is updated to version 2.0.

17.3.1.4 Savings Algorithms and Input Variables

Energy Savings

Energy savings for this measure were derived using the ENERGY STAR Pool Pump Savings Calculator.⁸³⁴

$$\text{Energy Savings } [\Delta kWh] = kWh_{conv} - kWh_{ES}$$

Equation 17.3-1

Where:

kWh_{conv} = Conventional single-speed pool pump energy (kWh).

kWh_{ES} = ENERGY STAR variable speed pool pump energy (kWh).

Algorithms to calculate the above parameters are defined as:

⁸³³ ENERGY STAR Program Requirements Product Specification for Pool Pumps

<https://www.energystar.gov/sites/default/files/asset/document/ENERGY%20STAR%20Version%203.1%20Pool%20Pumps%20Final%20Specification.pdf>

⁸³⁴ The ENERGY STAR Pool Pump Savings Calculator, updated May 2020, can be found on the ENERGY STAR website at: <https://www.energystar.gov/productfinder/product/certified-pool-pumps/results>.

$$kWh_{conv} = \frac{PFR_{conv} \times 60 \times \text{hours} \times \text{days}}{WEF_{conv} \times 1,000}$$

Equation 17.3-2

$$kWh_{ES} = \frac{V \times TO \times \text{days}}{WEF_{ES} \times 1,000}$$

Equation 17.3-3

Where:

| | | |
|--------------|---|--|
| PFR_{conv} | = | Conventional single-speed pump flow rate [gal/min]; see Table 17.3-3. |
| WEF_{conv} | = | Conventional single-speed pump weighted energy factor [gal/W·hr]; see Table 17.3-3. |
| WEF_{ES} | = | ENERGY STAR weighted energy factor [gal/W·hr]; see Table 17.3-4. |
| hours | = | Pump daily operating hours; see Table 17.3-3. |
| days | = | Operating days per year = Year-round operation: 365 days; Seasonal operation: 7 months x 30.4 days/month = 212.8 days (default). |
| V | = | Pool volume; (use actual or see Table 17.3-4). |
| TO | = | Turnovers per day, or number of times the volume of the pool is run through the pump per day; see Table 17.3-4. |
| 60 | = | Constant to convert between minutes and hours. |
| 1,000 | = | Constant to convert from watts to kilowatts. |

Table 17.3-3: [Pool Pumps] Conventional Pool Pump Assumptions⁸³⁵

| New Pump HP | Reference HP | Reference HHP ⁸³⁶ | Limited Hours ⁸³⁷ | 24/7 Operation | PFR _{conv} (gal/min) |
|------------------|--------------|------------------------------|------------------------------|----------------|-------------------------------|
| ≤ 1.25 | 1.0 | 0.533 | 12 | 24 | 75.5000 |
| 1.25 < hp ≤ 1.75 | 1.5 | 0.800 | | | 78.1429 |
| 1.75 < hp ≤ 2.25 | 2.0 | 1.066 | | | 88.6667 |
| 2.25 < hp ≤ 2.75 | 2.5 | 1.333 | | | 93.0910 |
| 2.75 < hp ≤ 5 | 3.0 | 1.599 | | | 101.6667 |

⁸³⁵ Conventional pump PFR and EF values are taken from pump curves found in the ENERGY STAR Pool Pump Savings Calculator. Note: input assumptions will be updated once calculator has been updated for compliance with the current specification.

⁸³⁶

⁸³⁷ Limited Hours assumes that pump operating hours are 12 hours per day, based on 2016 commercial pool pump program data reviewed by the Texas Evaluation Contractor.

Table 17.3-4: [Pool Pumps] ENERGY STAR Pool Pump Assumptions^{838,839}

| New Pump HP | V (gal) | TO | |
|------------------|---------|---------------|----------------|
| | | Limited Hours | 24/7 Operation |
| ≤ 1.25 | 20,000 | 2.7 | 5.4 |
| 1.25 < hp ≤ 1.75 | 20,000 | 2.8 | 5.6 |
| 1.75 < hp ≤ 2.25 | 22,000 | 2.9 | 5.8 |
| 2.25 < hp ≤ 2.75 | 25,000 | 2.7 | 5.4 |
| 2.75 < hp ≤ 5 | 28,000 | 2.6 | 5.2 |

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{kWh_{conv} - kWh_{ES}}{\text{hours}} \times \frac{DF}{\text{days}}$$

Equation 17.3-4

Where:

DF = Demand Factor from Table 17.3-5.

Table 17.3-5: [Pool Pumps] Demand Factors

| Operation | DF |
|--------------------|-----|
| 24/7 Operation | 1.0 |
| Limited Hours | 1.0 |
| Seasonal Operation | 1.0 |

⁸³⁸ ENERGY STAR PFR and EF values are taken from pump curves found in the ENERGY STAR Pool Pump Savings Calculator. Note: input assumptions will be updated once calculator has been updated for compliance with the current specification.

⁸³⁹ Turnovers calculated as TO = hours x 60 x PFR_{conv} ÷ V.

17.3.1.5 Deemed Energy Savings Tables

Table 17.3-6: [Pool Pumps] Deemed Energy Savings⁸⁴⁰

| New Rated Pump HP | Year-Round Operation | | Seasonal Operation (7 months) |
|-------------------|----------------------|---------------|-------------------------------|
| | 24/7 Operation | Limited Hours | |
| | kWh Savings | kWh Savings | kWh Savings |
| ≤ 1.25 | 6,682 | 3,341 | 1,948 |
| 1.25 < hp ≤ 1.75 | 1,191 | 596 | 347 |
| 1.75 < hp ≤ 2.25 | 1,580 | 790 | 461 |
| 2.25 < hp ≤ 2.75 | 1,895 | 947 | 552 |
| 2.75 < hp ≤ 5 | 2,327 | 1,163 | 678 |

17.3.1.6 Deemed Demand Savings Tables

Table 17.3-7: [Pool Pumps] Deemed Demand Savings for All Operating Profiles

| New Rated Pump (HP) | Demand Savings (kW) |
|---------------------|---------------------|
| ≤ 1.25 | 0.763 |
| 1.25 < hp ≤ 1.75 | 0.136 |
| 1.75 < hp ≤ 2.25 | 0.180 |
| 2.25 < hp ≤ 2.75 | 0.216 |
| 2.75 < hp ≤ 5 | 0.266 |

17.3.1.7 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years for pool pumps, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID OutD-PoolPump.⁸⁴¹

17.3.2 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- For all projects collect:
 - Manufacturer and model number of new pool pump

⁸⁴⁰ The results in this table may vary slightly from results produced by the ENERGY STAR calculator because of rounding of default savings coefficients throughout the measure and pool volume.

⁸⁴¹ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

- Rated pool pump horsepower
- Proof of purchase – with date of purchase, quantity, and model
- ENERGY STAR certificate matching new unit model number
- Facility operation schedule (24/7, year-round limited hours, seasonal)
- Pool volume in gallons (only required when calculating site-specific savings in lieu of deemed savings)
- For a significant sample of projects where attainable (e.g., those projects that are selected for inspection, not midstream or retail programs)
 - Baseline type: ER, ROB, NC
 - Items listed above for all projects
 - Rated horsepower of existing pool pump
 - Existing and new pump operating hours

Document Revision History

Table 17.3-8: [Pool Pumps] Revision History

| Guidebook version | Description of change |
|-------------------|--|
| FY 2025 | No revision. |
| FY 2026 | Updated baseline condition and deemed savings to reflect current federal standard. |

17.5 VENDING MACHINE CONTROLS

17.5.1 Measure Description

This measure is for the installation of Vending Machine Controls to reduce energy usage during periods of inactivity. These controls reduce energy usage by powering down the refrigeration and lighting systems when the control device signals that there is no human activity near the machine. If no activity or sale is detected over the manufacturer's programmed time duration, the device safely de-energizes the compressor, condenser fan, evaporator fan, and any lighting. For refrigerated machines, it will power up occasionally to maintain cooling to meet the machine's thermostat set point. When activity is detected, the system returns to full power. The energy and demand savings are determined on a per-vending machine basis.

17.5.1.1 Eligibility Criteria

This measure applies to refrigerated beverage vending machines manufactured and purchased prior to August 31, 2012. Refrigerated beverage vending machines manufactured after this date must already comply with federal standard maximum daily energy consumption requirements. The current federal standard further reduced these maximum consumption values, effective January 8, 2019.⁸⁴⁴

All non-refrigerated snack machines are eligible if controls are installed on equipment consistent with the Baseline Condition below. Display lighting must not have been permanently disabled.

17.5.1.2 Baseline Condition

The baseline condition is a 120-volt single phase refrigerated beverage or non-refrigerated snack vending machine without any controls.

17.5.1.3 High-Efficiency Condition

The high-efficiency condition is a 120-volt single phase refrigerated beverage or non-refrigerated snack vending machine with occupancy controls and compliant with the current federal standard, effective January 8, 2019.⁸⁴⁵

⁸⁴⁴ Appliance Standards for Refrigerated Beverage Vending Machines.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=29#current_standards.

⁸⁴⁵ Appliance Standards for Refrigerated Beverage Vending Machines.

https://www1.eere.energy.gov/buildings/appliance_standards/standards.aspx?productid=29#current_standards.

17.5.2 Energy and Demand Savings Methodology

17.5.2.1 Savings Algorithms and Input Variables

Energy Savings

Energy savings are deemed based on a metering study completed by Pacific Gas & Electric (PG&E). Delta load shapes for this measure are taken from a Sacramento Municipal Utility District (SMUD) metering study. Demand savings for refrigerated cold drink units are calculated based on a probability weighted analysis of hourly consumption impacts, and demand savings for other unit types are adjusted proportionally based on differences in rated product wattage.

17.5.2.2 Deemed Energy Savings Tables

Table 17.5-1: [Vending Controls] Deemed Energy Savings by Equipment Type

| Vending Machine Controls | Annual Energy Savings [kWh] |
|--|-----------------------------|
| Control for Refrigerated Cold Drink Unit cans or bottles ⁸⁴⁶ | 1,612 |
| Control for Refrigerated Reach-in Unit any sealed beverage ⁸⁴⁷ | 1,086 |
| Control for Non-Refrigerated Snack Unit with lighting (including warm beverage) ⁸⁴⁸ | 387 |

17.5.2.3 Deemed Demand Savings Tables

Load shapes for this measure are taken from a Sacramento Municipal Utility District (SMUD) study on vending machine controls and their verified savings performance.⁸⁴⁹

Table 17.5-2: [Vending Controls] Deemed Demand Savings by Unit Type

| Unit Type | Peak Type | Demand Savings [kW] |
|------------------------------|-----------|---------------------|
| Refrigerated Cold Drink Unit | NCP | 0.165 |
| | CP | 0.022 |
| | 4CP | 0.030 |
| Refrigerated Reach-in Unit | NCP | 0.190 |
| | CP | 0.026 |
| | 4CP | 0.035 |

⁸⁴⁶ Pacific Gas and Electric, Work Paper VMCold, Revision 3, August 2009, Measure Code R97.

⁸⁴⁷ Pacific Gas and Electric, Work Paper VMReach, Revision 3, August 2009, Measure Code R143.

⁸⁴⁸ Pacific Gas and Electric, Work Paper VMSnack, Revision 3, August 2009, Measure Code R98.

⁸⁴⁹ Chappell, C., Hanzawi, E., Bos, W., Brost, M., and Peet, R. (2002). "Does It Keep the Drinks Cold and Reduce Peak Demand? An Evaluation of a Vending Machine Control Program," 2002 ACEEE Summer Study on Energy Efficiency in Buildings Proceedings, pp. 10.47-10.56.

| Unit Type | Peak Type | Demand Savings [kW] |
|-----------------------------|-----------|---------------------|
| Non-Refrigerated Snack Unit | NCP | 0.035 |
| | CP | 0.005 |
| | 4CP | 0.006 |

17.5.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 5 years for vending machine controls, as specified in the California Database of Energy Efficiency Resources (DEER) READI tool for EUL ID Plug-VendCtrlr.⁸⁵⁰

17.5.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Vending machine type (refrigerated cold drink unit, refrigerated reach-in unit, non-refrigerated snack unit with lighting)
- Vending machine manufacture date

Document Revision History

Table 17.5-3: [Vending Controls] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

⁸⁵⁰ DEER READI (Remote Ex-Ante Database Interface). <http://www.deeresources.com/index.php/readi>.

17.6 COMPUTER POWER MANAGEMENT

17.6.1 Measure Description

This measure presents deemed savings for implementation of computer power management strategies. Computer power management includes the use of operational settings that automate the power management features of computer equipment, including automatically placing equipment into a low power mode during periods of inactivity. This may be done either with built-in features integral to the computer operating system or through an add-on software program. Typically, this measure is implemented across an entire network of computers.

17.6.1.1 Eligibility Criteria

To be eligible for this measure, computers must not have any automatic sleep or other low power setting in place. Both conventional and ENERGY STAR computer equipment is eligible for this measure. Applicable building types include offices and schools.

17.6.1.2 Baseline Condition

The baseline conditions are the estimated number of hours that the computer spends in active, sleep, and off modes before the power settings are actively managed. Operating hours may be estimated from metering, or the default hours provided in the calculation of deemed savings may be used. The default baseline hours are taken from the ENERGY STAR modeling study assumptions contained in the Low Carbon IT Savings Calculator,⁸⁵¹ and assume baseline computer settings never enter sleep mode, and 60% of computers are turned off each night.⁸⁵²

17.6.1.3 High Efficiency Condition

The efficient conditions are the estimated number of hours that the computer spends in active, sleep, and off modes after the power settings are actively managed. Operating hours may be estimated from metering, or the default hours provided in the calculation of deemed savings may be used. The default efficient hours are taken from the ENERGY STAR modeling study assumptions contained in the Low Carbon IT Savings Calculator and assume managed computer settings enter sleep mode after 15 minutes of inactivity, and 80% of computers are turned off each night.⁸⁵³

⁸⁵¹ ENERGY STAR Low Carbon IT Calculator available for download at:
https://www.energystar.gov/products/low_carbon_it_campaign/put_your_computers_sleep.

⁸⁵² Based on 2015 custom project metering from El Paso Electric.

⁸⁵³ Based on 2015 custom project metering from El Paso Electric.

17.6.2 Energy and Demand Savings Methodology

17.6.2.1 Savings Algorithms and Input Variables

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = \frac{W_a(\text{hours}_{a,pre} - \text{hours}_{a,post}) + W_s(\text{hours}_{s,pre} - \text{hours}_{s,post}) + W_o(\text{hours}_{o,pre} - \text{hours}_{o,post})}{1,000}$$

Equation 17.6-1

Demand Savings

$$\text{Demand Savings } [\Delta kW] = \frac{(W_a - W_s) \times DF_{inactive}}{1,000}$$

Equation 17.6-2

Where:

| | | |
|-------------------------|---|--|
| W_a | = | total wattage of the equipment, including computer and monitor, in active/idle mode; see Table 17.6-1. |
| $\text{hours}_{a,pre}$ | = | annual number of hours the computer is in active/idle mode before computer management software is installed; see Table 17.6-2. |
| $\text{hours}_{a,post}$ | = | annual number of hours the computer is in active/idle mode after computer management software is installed; see Table 17.6-2. |
| W_s | = | total wattage of the equipment, including computer and monitor, in sleep mode; see Table 17.6-1. |
| $\text{hours}_{s,pre}$ | = | annual number of hours the computer is in sleep mode before computer management software is installed; see Table 17.6-2. |
| $\text{hours}_{s,post}$ | = | annual number of hours the computer is in sleep mode after computer management software is installed; see Table 17.6-2. |
| W_o | = | total wattage of the equipment, including computer and monitor, in off mode; see Table 17.6-1. |
| $\text{hours}_{o,pre}$ | = | annual number of hours the computer is in off mode before computer management software is installed; see Table 17.6-2. |
| $\text{hours}_{o,post}$ | = | annual number of hours the computer is in off mode after computer management software is installed; see Table 17.6-2. |
| 1,000 | = | Constant to convert from watts to kilowatts. |
| $DF_{inactive}$ | = | Demand factor for inactive hours (sleep and off); see Table 17.6-3. |

Table 17.6-1: [Computer Power Management] Equipment Wattages⁸⁵⁴

| Equipment | W _{active} | W _{sleep} | W _{off} |
|---|---------------------|--------------------|------------------|
| Conventional Monitor ⁸⁵⁵ | 18.30 | 0.30 | 0.30 |
| Conventional Computer | 48.11 | 2.31 | 0.96 |
| Conventional Notebook (including display) | 14.82 | 1.21 | 0.61 |
| ENERGY STAR Monitor | 15.00 | 0.26 | 0.26 |
| ENERGY STAR Computer | 27.11 | 1.80 | 0.81 |
| ENERGY STAR Notebook (including display) | 8.61 | 0.89 | 0.46 |

Table 17.6-2: [Computer Power Management] Operating Hours⁸⁵⁶

| Building Activity Type | hrs _{active,pre} | hrs _{active,post} | hrs _{sleep,pre} | hrs _{sleep,post} | hrs _{off,pre} | hrs _{off,post} |
|---|---------------------------|----------------------------|--------------------------|---------------------------|------------------------|-------------------------|
| Typical office (8 hours/day, 5 days/week, 22 non-workdays/year) | 4,650 | 1,175 | - | 2,105 | 4,110 | 5,480 |
| Typical school (8 hours/day, 5 days/week, 113 non-school days/year) | 4,213 | 727 | - | 1,970 | 4,547 | 6,063 |

The load shapes for this measure were taken from the ENERGY STAR Low Carbon IT calculator modeling profile, with computer settings to enter sleep mode after 15 minutes of inactivity. Office load shapes assume the same daily profile throughout the year.

Table 17.6-3: [Computer Power Management] Demand Factors

| Peak Type | DF _{inactive} |
|-----------|------------------------|
| NCP | 1.00 |
| CP | 0.36 |
| 4CP | 0.75 |

⁸⁵⁴ Equipment wattages taken from the Low Carbon IT Savings Calculator.

https://www.energystar.gov/buildings/save_energy_commercial_buildings/ways_save/energy_efficient_products.

⁸⁵⁵ Average of 17.0-24.9 inches monitor sizes taken from the ENERGY STAR Office Equipment Calculator.

⁸⁵⁶ Hours taken from assumptions in the ENERGY STAR calculator. Hours_{pre} assume baseline computer settings never enter sleep mode, and 60% of computers are turned off each night. Hours_{post} assume managed computer settings enter sleep mode after 15 minutes of inactivity, and 80% of computers are turned off each night.

17.6.2.2 Deemed Energy and Demand Savings Tables

Table 17.6-4: [Computer Power Management] Deemed Energy and Demand Savings: Office and School

| Equipment | kWh | NCP kW | CP kW | 4CP kW |
|---|-------|--------|-------|--------|
| Conventional Monitor | 62.6 | 0.018 | 0.006 | 0.014 |
| Conventional Computer | 161.4 | 0.046 | 0.016 | 0.034 |
| Conventional Notebook (including display) | 48.2 | 0.014 | 0.005 | 0.010 |
| ENERGY STAR Monitor | 51.3 | 0.015 | 0.005 | 0.011 |
| ENERGY STAR Computer | 89.5 | 0.025 | 0.009 | 0.019 |
| ENERGY STAR Notebook (including display) | 27.5 | 0.008 | 0.003 | 0.006 |

17.6.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 3 years for computer power management based on the useful life of the computer equipment being controlled.⁸⁵⁷

17.6.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Equipment type:
 - Conventional or ENERGY STAR
 - Monitor, computer, or notebook
- Application type (office, school)

Document Revision History

Table 17.6-5: [Computer Power Management] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

⁸⁵⁷ Internal Revenue Service, 1.35.6.4 (09-27-2019), Property and Equipment Capitalization, Useful life for Laptop and Desktop Equipment. https://www.irs.gov/irm/part1/irm_01-035-006.

17.7 ENERGY STAR® ELECTRIC VEHICLE SUPPLY EQUIPMENT (EVSE)

17.7.1 Measure Description

This section applies to the installation of electric vehicle supply equipment (EVSE) meeting the specifications of ENERGY STAR Level 2 at a non-residential site. EVSE is the infrastructure that enables plug-in electric vehicles (PEV) to charge onboard batteries. Level 2 EVSE require 240-volt electrical service. This measure provides deemed savings for the energy efficiency improvement of an ENERGY STAR EVSE over a standard or non-ENERGY STAR EVSE.

17.7.1.1 Eligibility Criteria

Eligible equipment includes ENERGY STAR compliant Level 2 EVSE installed in a non-residential application, which includes public, multifamily, workplace, and fleet locations. Public locations are sites where an EVSE is intended to be used by the public or visitors to the site. This includes locations such as retail, education, municipal, hospitality, and other similar locations. For the purposes of this measure, multifamily sites are public locations. Workplace locations include sites where an EVSE is intended to be used by employees to charge their personal vehicles when reporting to the workplace site. Fleet locations include sites where an EVSE is intended to be used to charge a fleet of company vehicles. The EVSE may be installed for use on either an all-battery electric vehicle (BEV) or a plug-in hybrid electric vehicle (PHEV). Savings estimates for this measure are based on studies of light duty vehicles; EVSE for charging heavy duty vehicles should pursue custom M&V.

17.7.1.2 Baseline Condition

The baseline condition is a non-ENERGY STAR compliant Level 2 EVSE.

17.7.1.3 High-Efficiency Condition

The high-efficiency condition is a Level 2 EVSE compliant with ENERGY STAR Version 1.1 Specification, effective March 31, 2021.⁸⁵⁸

17.7.2 Energy and Demand Savings Methodology

Savings for EVSE come from efficiency gains of the ENERGY STAR equipment during operating modes when the vehicle is plugged in but not charging and when not plugged in. Deemed savings are calculated according to the following algorithms.

⁸⁵⁸ ENERGY STAR Program Requirements for Electric Vehicle Supply Equipment Eligibility Criteria v1.1.
https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20V1.1%20DC%20EVSE%20Final%20Specification_0.pdf.

17.7.2.1 Savings Algorithms and Input Variables

Energy Savings

$$ENERGY STAR Idle Consumption [kWh] = \frac{(Hrs_{plug} \times W_{plug} + Hrs_{unplug,C} \times W_{unplug}) \times days_C + Hrs_{unplug,NC} \times W_{unplug} \times days_{NC}}{1,000}$$

Equation 17.7-1

$$Baseline Idle Consumption [kWh] = \frac{ENERGY STAR Idle Consumption}{0.6}$$

Equation 17.7-2

$$Energy Savings [\Delta kWh] = Baseline Idle Consumption - ENERGY STAR Idle Consumption$$

Equation 17.7-3

Demand Savings

$$Demand Savings [\Delta kW] = \frac{\Delta kWh}{Hrs_{unplug,C} \times days_C + Hrs_{unplug,NC} \times days_{NC}} \times DF$$

Equation 17.7-4

Where:

Hrs_{plug} = Time per day the vehicle is plugged into the EVSE and not charging [hours]⁸⁵⁹ = 2.8

W_{plug} = Wattage of the EVSE when the vehicle is plugged into the EVSE but not charging [W]⁸⁶⁰ = 6.9 W

$Hrs_{unplug,C}$ = Time per day the vehicle is not plugged into the EVSE on a charging day [hours]⁸⁶¹ = 19

$Hrs_{unplug,NC}$ = Time per day the vehicle is not plugged into the EVSE on a non-charge day [hours] = 24

W_{unplug} = Wattage of the EVSE when the vehicle is not plugged into the EVSE [W]⁸⁶² = 3.3

$days_C$ = Number of charging days per year [days]⁸⁶³ = 204

⁸⁵⁹ National Renewable Energy Laboratory (NREL), February 2018, "Charging Electric Vehicles in Smart Cities: An EVI-Pro Analysis of Columbus Ohio," page 26, Table 8: Charging Statistics by Location Type and Level, ChargePoint Data. Average across all location types, dwell time minus charging duration.

⁸⁶⁰ Average Idle Mode Input Power from ENERGY STAR certified EVSE product list as of July 13, 2020.

⁸⁶¹ NREL "Charging Electric Vehicles in Smart Cities: An EVI-Pro Analysis of Columbus Ohio," page 26, Table 8; 24 hours per day minus average dwell time.

⁸⁶² Average No Vehicle Mode Input Power from ENERGY STAR certified EVSE product list.

⁸⁶³ NREL "Charging Electric Vehicles in Smart Cities: An EVI-Pro Analysis of Columbus Ohio," page 25; 0.56 charging sessions per day per plug in Austin, Texas. 365 x 0.56 = 204.

| | | |
|-------------|---|---|
| $days_{NC}$ | = | Number of non-charging days per year [days] = 161 |
| 1,000 | = | Constant to convert from W to kW |
| 0.6 | = | Efficiency adjustment factor ⁸⁶⁴ |
| DF | = | Demand factor (see Table 17.7-1) |

Table 17.7-1: [COM EVSE] Demand Factors⁸⁶⁵

| Peak Type ⁸⁶⁶ | Public | Workplace | Fleet |
|--------------------------|---------|-----------|---------|
| NCP | 0.46134 | 0.87173 | 0.26507 |
| CP | | | |
| 4CP | | | |

17.7.2.2 Deemed Energy and Demand Savings Tables

Table 17.7-2: [COM EVSE] Energy and Demand Savings

| Location Type | kWh | NCP kW | CP kW | 4CP kW |
|---------------|------|--------|-------|--------|
| Public | 19.7 | 0.0012 | | |
| Workplace | | 0.0022 | | |
| Fleet | | 0.0007 | | |

1.1.1.2 Measure Life and Lifetime Savings

The estimated useful life (EUL) for an EVSE is assumed to be 10 years.⁸⁶⁷

17.7.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Location type (public, workplace, or fleet) ⁸⁶⁸
- EVSE quantity

⁸⁶⁴ ENERGY STAR Electric Vehicle Chargers Buying Guidance: "ENERGY STAR certified EV charger... on average use 40% less energy than a standard EV charger when the charger is in standby mode (i.e., not actively charging a vehicle)."
<https://www.energystar.gov/products/other/evse>.

⁸⁶⁵ Calculated using data from NREL "Charging Electric Vehicles in Smart Cities: An EVI-Pro Analysis of Columbus Ohio," page 27, Figure 21: Daily distribution of ChargePoint charging events by EVSE type and day of the week.

⁸⁶⁶ Charging load profiles are expected to vary significantly by application. Therefore, NCP and 4CP are assumed to be equal to CP.

⁸⁶⁷ U.S. Department of Energy Vehicle Technologies Office, November 2015, "Costs Associated with Non-Residential Electric Vehicle Supply Equipment" p. 21. https://afdc.energy.gov/files/u/publication/evse_cost_report_2015.pdf.

⁸⁶⁸ Refer to Eligibility Criteria section for location type definitions.

- EVSE manufacturer and model number
- ENERGY STAR certificate matching EVSE model number

Document Revision History

Table 17.7-3: [COM EVSE] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

17.8 HAND DRYERS

17.8.1 Measure Description

This section presents the methodology for calculating the savings realized from installing efficient hand dryers, which save energy by drying with air movement using motion sensors, thus reducing hand-drying time.

17.8.1.1 Eligibility Criteria

Existing hand dryer equipment must be push-button operated and rated at more than 1,500 W. New hand dryers must be motion sensor operated and rated at 1,500 W or less.

17.8.1.2 Baseline Condition

The baseline efficiency case is a push-button activated hand dryer rated at more than 1,500 W.

17.8.1.3 High Efficiency Condition

Eligible high-efficiency equipment is a motion sensor operated hand dryer with a nominal input power of 1,500 W or less.

17.8.2 Energy and Demand Savings Methodology

17.8.2.1 Savings Algorithms and Input Variables

The energy savings from the installation of efficient hand dryers are due to a decrease in power and runtime of the efficient hand dryers over the pre-retrofit equipment. The energy and demand savings are calculated using the following equations:

AOH, CF, IEF_E, and IEF_D match assumptions from the non-residential lighting measure.⁸⁶⁹

Energy Savings

$$\text{Energy Savings } [\Delta kWh] = \frac{UPD \times AOD \times \Delta Wh}{1,000} \times IEF_E$$

Equation 17.8-1

$$\Delta Wh = \frac{(W_{Base} \times CT_{Base}) - (W_{Eff} \times CT_{Eff})}{3,600}$$

Equation 17.8-2

⁸⁶⁹ See Commercial Lighting Efficiency section. It is assumed building occupancy with respect to lighting is an appropriate proxy for occupant utilization of hand dryers.

Demand Savings

$$\text{Peak Demand Savings } [\Delta kW] = \frac{UPD \times AOD \times \Delta Wh}{1,000 \times AOH} \times DF \times IEF_D$$

Equation 17.8-3

Where:

| | | |
|-------------|---|---|
| UPD | = | Number of uses per day ⁸⁷⁰ (see Table 17.8-2) |
| AOD | = | Number of days the facility operates per year ⁸⁷¹ (see Table 17.8-2) |
| IEF_E | = | Interactive effects factor for energy (see Table 17.8-1) |
| W_{Base} | = | Baseline equipment nominal power, 2,155 W ⁸⁷² |
| W_{Eff} | = | Efficient equipment nominal power, 1,329 W ⁸⁷³ |
| CT_{Base} | = | Cycle time of baseline equipment ⁸⁷⁴ , 34 seconds |
| CT_{Eff} | = | Cycle time of efficient equipment ⁸⁷⁵ , 17 seconds |
| AOH | = | Annual building operating hours (see Table 17.8-2) |
| DF | = | Demand factor (see Table 17.8-2) |
| IEF_D | = | Interactive effects factor for demand (see Table 17.8-1) |

Table 17.8-1: [Hand Dryers] Deemed Energy and Demand Interactive Effects Factors⁸⁷⁶

| Space Conditioning Type | IEF_E | IEF_D (NCP) | IEF_D (CP/4CP) |
|-------------------------------|---------|------------------|---------------------|
| Refrigerated air | 1.05 | 1.05 | 1.10 |
| Evaporative cooling | 1.02 | 1.02 | 1.04 |
| None (unconditioned/uncooled) | 1.00 | 1.00 | 1.00 |

⁸⁷⁰ IL TRM 12 Volume 2, 4.8.26

⁸⁷¹ Technology Data Characterizing Water Heating in Commercial Buildings: Application to End-Use Forecasting, Osman Sezgen and Jonathan G. Koomey, Lawrence Berkeley National Laboratory, December 1995. Table 2. <https://eta-publications.lbl.gov/sites/default/files/lbnl-37398e.pdf>.

⁸⁷² Baseline and efficient nominal power and cycle times are averages of surveyed individual hand dryer units by CLEARresult in Arkansas.

⁸⁷³ Ibid.

⁸⁷⁴ Ibid.

⁸⁷⁵ Ibid.

⁸⁷⁶ Texas Technical Reference Manual, Volume 2, Section 2.1, Table 11, Nonresidential Lighting.

Table 17.8-2: [Hand Dryers] Savings Calculation Input Assumptions

| Usage Level | Building Type | DF ⁸⁷⁷ | | | AOH ⁸⁷⁸ | UPD ⁸⁷⁹ | AOD ⁸⁸⁰ |
|--------------------|---|-------------------|------|------|--------------------|--------------------|--------------------|
| | | NCP | CP | 4CP | | | |
| Low | Office | 0.90 | 0.86 | 0.90 | 3,737 | 50 | 250 |
| | Warehouse | 0.85 | 0.79 | 0.75 | 3,501 | | |
| Medium/moderate | Non-24 hour supermarket or convenience store | 0.90 | 0.90 | 0.90 | 4,706 | 125 | 365 |
| | Full-service restaurant | 0.90 | 0.90 | 0.90 | 4,368 | | |
| | Quick-service restaurant | 0.90 | 0.90 | 0.90 | 6,188 | | |
| | Stand-alone retail | 0.90 | 0.90 | 0.90 | 3,668 | | |
| | Strip mall | 0.90 | 0.90 | 0.90 | 3,965 | | |
| High | College, university, vocational, and day care | 0.65 | 0.65 | 0.65 | 3,577 | 250 | 200 |
| | Education: K-12 ⁸⁸¹ | 0.90 | 0.32 | 0.54 | 3,177 | | |
| | 24-hour supermarket or convenience store | 0.65 | 0.65 | 0.65 | 6,900 | | |
| | Enclosed mall | 0.65 | 0.65 | 0.65 | 4,813 | | |
| | Public Assembly | 0.90 | 0.90 | 0.90 | 2,638 | | |
| Heavy duty/extreme | Transportation center | 0.90 | 0.90 | 0.90 | 8,760 | 750 | 365 |

17.8.2.2 Deemed Energy and Demand Savings Tables

The deemed energy and demand savings for hand dryers with unknown number of operating days per year, base/efficient cycles times, and base/efficient unit wattages are as follows:

⁸⁷⁷From the commercial Lighting Efficiency measure..

⁸⁷⁸ From the commercial Lighting Efficiency measure.

⁸⁷⁹IL TRM 12 Volume 2, 4.8.26)

⁸⁸⁰ Technology Data Characterizing Water Heating in Commercial Buildings: Application to End-Use Forecasting, Osman Sezgen and Jonathan G. Koomey, Lawrence Berkeley National Laboratory, December 1995. Table 2. <https://eta-publications.lbl.gov/sites/default/files/lbnl-37398e.pdf>.

⁸⁸¹ Assuming K–12 without summer session.

Table 17.8-3: [Hand Dryers] Deemed Energy and Demand Savings

| Usage Level | Building Type | kWh | NCP | | CP | 4CP |
|--------------------|---|-------|-------|-------|----|-------|
| Low | Office | 185 | 0.047 | 0.045 | | 0.047 |
| | Warehouse | | 0.047 | 0.044 | | 0.041 |
| Medium/moderate | Non-24 hour supermarket or convenience store | 674 | 0.135 | 0.135 | | 0.135 |
| | Full-service restaurant | | 0.145 | 0.145 | | 0.145 |
| | Quick-service restaurant | | 0.103 | 0.103 | | 0.103 |
| | Stand-alone retail | | 0.173 | 0.173 | | 0.173 |
| | Strip mall | | 0.160 | 0.160 | | 0.160 |
| High | College, university, vocational, and day care | 739 | 0.141 | 0.141 | | 0.141 |
| | Education: K-12 | | 0.219 | 0.078 | | 0.132 |
| | 24-hour supermarket or convenience store | 2,022 | 0.200 | 0.200 | | 0.200 |
| | Enclosed mall | | 0.286 | 0.286 | | 0.286 |
| | Public Assembly | 923 | 0.330 | 0.330 | | 0.330 |
| Heavy duty/extreme | Transportation center | 4,044 | 0.484 | 0.484 | | 0.484 |

17.8.2.3 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 10 years⁸⁸² for efficient hand dryers.

17.8.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Building type
- Installed quantity

⁸⁸² Based on studies conducted by two separate parties; Comparative Environmental Life Cycle Assessment of Hand Drying Systems by Quantis (pg. 2) and Guidelines to Reduce/Eliminate Paper Towel Use by Installing Electric Hand Dryers by Partners in Pollution Prevention P3 (pg. 17).

- Efficient hand dryer make and model
- Efficient hand dryer nominal input power (W)
- Proof of purchase

17.8.4 Document Revision History

Table 17.8-4: [Hand Dryers] Revision History

| Guidebook version | Description of change |
|-------------------|---|
| FY 2025 | Measure origin. |
| FY 2026 | Updated building type naming convention. Updated peak demand calculation, savings calculation input assumptions and deemed savings. |

18. COMMERCIAL: CUSTOM

18.1 COMMERCIAL CUSTOM

18.1.1 Measure Description

Measures that do not fit into existing prescriptive programs will require measure-specific energy and demand savings calculations to be done, sometimes requiring development of new and unique savings calculation methods. These measures are referred to as custom measures and the measurement and verification (M&V) procedures as outlined in this section should be followed to facilitate impact evaluation.

18.1.1.1 Eligibility Criteria

Projects whose measures fall into the custom category are required to submit a qualifying M&V plan prior to beginning work. The proposed M&V plan should adhere to industry best practices such as the options put forth in the International Performance Measurement & Verification Protocol (IPMVP).⁸⁸³ M&V plan contents may include the following sections, as suggested by the IPMVP.

- Energy Conservation Measure (ECM) intent
- Measurement boundary
- Baseline & reporting period, energy, and conditions
- Basis for adjustment
- Analysis procedures
- Energy prices
- Meter specifications
- Monitoring responsibilities
- Expected accuracy
- Justification of estimates
- Quality assurance

⁸⁸³ International Performance Measurement & Verification Protocol (IPMVP). Available at: <http://evo-world.org/en/>.

18.1.1.2 Baseline Condition

Baseline conditions will be determined on a per-project basis and should be declared in the M&V plan.

18.1.1.3 High-Efficiency Condition

High Efficiency conditions will be determined on a per-project basis and should be declared in the M&V plan.

18.1.2 Energy and Demand Savings Methodology

18.1.2.1 Savings Algorithms and Input Variables

The savings methodology will be determined on a per-project basis and declared in the M&V plan.

18.1.2.2 Deemed Energy Savings Tables

There are no deemed savings tables for this measure.

18.1.2.3 Deemed Demand Savings Tables

There are no lookup tables available for this measure.

18.1.2.4 Measure Life and Lifetime Savings

The estimated useful life (EUL) will be determined on a per-project basis.

18.1.3 Program Tracking Data & Evaluation Requirements

Tracking data should be designed to fit the custom methodology.

19. COMMERCIAL: NEW CONSTRUCTION

19.1 COMMERCIAL NEW CONSTRUCTION

19.1.1 Measure Description

New construction projects are projects that take a whole-building approach to incorporating energy efficient technologies during the design and construction of new facilities.

19.1.1.1 Eligibility Criteria

New construction projects are required to submit a qualifying measurement and verification (M&V) plan prior to beginning work. The M&V plan should adhere to the International Performance Measurement & Verification Protocol (IPMVP) Option D: Calibrated Simulation method.⁸⁸⁴

Project implementers are required to conduct a simulation analysis using a method that is appropriate for the complexity of the project site. A whole-building simulation program that uses hourly calculation techniques may be required to estimate project savings on most sites, but simplified models may be accepted on a per-project basis. Evaluation of new construction projects requires review of simulation models and design documents by the Evaluation, Measurement & Verification (EM&V) contractor.

A visual site inspection will be conducted by the EM&V contractor post construction and before occupancy to confirm that as built conditions match design documents.

Model calibration is required to be conducted using metered site data over a reporting period long enough to capture a period of stable operation. The reporting period will be declared in the M&V plan. To implement this recommendation, it is necessary to ensure that whole-building energy models are obtained and retained at the time of application submittal.

19.1.1.2 Baseline Condition

The applicable baseline condition shall be based on the building code in effect for the City of San Antonio at the time of project permitting, which is IECC 2018 as of October 2018. For projects that were permitted outside of the City of San Antonio's jurisdiction, the applicable baseline will be the statewide code adopted for Texas, IECC 2015.

19.1.1.3 High-Efficiency Condition

The high efficiency condition is the facility as built.

⁸⁸⁴ International Performance Measurement & Verification Protocol (IPMVP). Available at: <http://evo-world.org/en/>.

19.1.2 Energy and Demand Savings Methodology

19.1.2.1 Energy Savings

Energy savings will be determined on a per-project basis according to the M&V plan.

19.1.2.2 Demand Savings

Demand savings will be determined on a per-project basis according to the M&V plan.

19.1.2.3 Deemed Energy Savings Tables

There are no lookup tables available for this measure.

19.1.2.4 Deemed Demand Savings Tables

There are no lookup tables available for this measure.

19.1.2.5 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 18 years for commercial new construction when reporting whole building savings based on a mix of energy efficient design features (envelope, mechanical/plumbing, lighting). Prescriptive savings reported for individual energy efficiency measures should refer to the EUL for each respective measure.

19.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Approved contractor product submittals for HVAC and lighting equipment, or product sheets from operations and maintenance (O&M) manual
- Simulation summary reports
- Hourly energy output files
- Demand and energy savings calculation file (spreadsheet)
- Commissioning Report and HVAC TAB (test, adjust & balance) Report - review of these reports will confirm initial building control settings are in accordance with design

20. COMMERCIAL: RENEWABLE ENERGY

20.1 COMMERCIAL AND SCHOOLS SOLAR PHOTOVOLTAIC

20.1.1 Measure Description

This measure involves the installation of a new or expanded commercial grid-connected solar photovoltaic (PV) system.

20.1.1.1 Eligibility Criteria

Only PV systems that result in reductions of the customer's purchased energy and/or peak demand qualify for savings. Off-grid systems are not eligible. CPS Energy maintains additional eligibility criteria for participating in the incentive program.

20.1.1.2 Baseline Condition

PV system not currently installed (typical), or an existing system is present but additional generating capacity is added.

20.1.1.3 High-Efficiency Condition

PV system (or additional capacity on an existing system) is installed and operational.

20.1.2 Energy and Demand Savings Methodology

20.1.2.1 Savings Algorithms and Input Variables

Energy and demand savings are derived from meter-based savings validation of CPS Energy's commercial fleet of solar energy systems conducted by Frontier Energy in 2021.

Energy Savings

Based on Frontier's 2021 analysis of CPS Energy's residential solar fleet, CPS Energy uses an average annual performance factor of 1,206 kWh per kW_{DC} per year for commercial and school solar energy systems.⁸⁸⁵ Thus,

$$\text{Energy Savings } [\Delta kWh] = 1,206 \times kW_{DC} \text{ installed}$$

Equation 20.1-1

⁸⁸⁵ Evaluation, Measurement and Verification of CPS Energy's FY 2015 DSM Programs, June 11, 2015, Frontier Associates.

Where:

kW_{DC} = Sum of the DC capacity at standard test conditions (STC) of all PV modules installed (or additional capacity installed on existing system). This factor may be reassessed periodically and updated if the composition of installed projects is determined to vary substantially from the assumed fleet-wide average.

The annual energy savings performance factor above results from the analysis of solar AMI data for commercial systems installed from 2017 through 2020. The table below lists the percentage of annual kWh applied to each costing period.

Table 20.1-1 [COM Solar PV] Solar Initiative Allocation of Annual kWh Savings into CPS Energy Costing Periods

| Load Shape Category | Summer On Peak | Summer Mid Peak | Summer Off Peak | Non-Summer Mid Peak | Non-Summer Off Peak |
|------------------------------|----------------|-----------------|-----------------|---------------------|---------------------|
| Commercial/ Schools Solar | 12.60% | 26.36% | 0.25% | 42.18% | 18.61% |

20.1.2.2 Deemed Energy Savings Tables

This section is not applicable for this measure.

20.1.2.3 Deemed Demand Savings Tables

Frontier’s 2021 analysis of CPS Energy’s commercial and schools solar fleet estimated average performance factors for coincident peak (CP), non-coincident peak (NCP), and ERCOT TCOS 4CP demand savings. These performance factors were determined by subjecting the commercial fleet-wide 8,760 hourly load shape to methods for determining each demand metric:

- **Non-Coincident Peak (NCP):** CPS Energy uses a non-coincident peak factor of 91.5% (or 0.915) of the total array DC capacity at standard test conditions (STC). This factor represents the maximum hourly kW_{AC} value over the 8,760-hour period, regardless of when it occurred.

$$\text{Non-Coincident Peak (NCP) savings} = 0.915 \times kW_{DC}$$

Equation 20.1-2

- **Coincident Peak (CP):** CPS Energy uses a coincident peak factor of 41.1% (or 0.411) of the total array DC capacity at standard test conditions (STC). This factor is calculated as the probability-weighted average kW_{AC} output of a one (1) kW_{DC} “fleet average” commercial/schools array over the top 20 hours in a blended TMY weather file determined to be the most likely to coincide with CPS Energy’s peak.

$$\text{Coincident Peak (CP) savings} = 0.411 \times kW_{DC}$$

Equation 20.1-3

- **ERCOT TCOS 4CP:** CPS Energy uses an ERCOT TCOS 4CP factor of 34.5% (or 0.345) of the total array DC capacity at standard test conditions (STC). This factor is calculated as the average demand savings of a one (1) kW_{DC} “fleet average” commercial and schools array during the most recent 20 historical 4CP intervals.

$$ERCOT\ TCOS\ 4CP\ savings = 0.345 \times kW_{DC}$$

Equation 20.1-4

20.1.2.4 Deemed Winter Demand Savings Tables

This section is not applicable for this measure.

20.1.2.5 Claimed Peak Demand Savings

This section is not applicable for this measure.

20.1.2.6 Measure Life and Lifetime Savings

The estimated useful life (EUL) is 30 years for solar PV. This value is consistent with engineering estimates based on manufacturers' warranties and historical data, and with the EUL reported in the Texas Technical Reference Manual (TRM).

20.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- Project location (city) and zip code
- Module type: Standard, premium, or thin film
- Array Type: Fixed (open rack), fixed (roof mount), 1-axis tracking, 1-axis backtracking, 2-axis tracking, etc.
- Tilt, azimuth, and DC system size rating at standard test conditions for each array
- Date of PVWatts® run, and PVWatts® report (retained with project documentation) for each array

20.1.4 Document Revision History

Table 20.1-2 [COM Solar PV] Revision History

| Guidebook version | Description of change |
|-------------------|-----------------------|
| FY 2025 | No revision. |
| FY 2026 | No revision. |

21. COMMERCIAL: DEMAND RESPONSE/LOAD CONTROL

21.1 COMMERCIAL DEMAND RESPONSE

21.1.1 Measure Description

Commercial demand response (DR) measures include technologies that enable CPS Energy to reduce aggregate commercial customer demand to respond to an electric system need. These technologies include a variety of control mechanisms affecting production processes, large appliances, and other controllable loads.

CPS Energy plans to deploy commercial demand response through customers enrolled in one of the C&I DR program options (there are currently four), and the Automatic Demand Response (ADR) program.

21.1.1.1 Eligibility Criteria

Any commercial or industrial customer with an eligible control technology who is actively enrolled in one of CPS Energy's commercial and industrial demand response programs.

21.1.1.2 Baseline Condition

Customer did not participate in a demand response event.

21.1.1.3 High-Efficiency Condition

Customer participated in a commercial/industrial demand response event.

21.1.2 Energy and Demand Savings Methodology

21.1.2.1 Savings Algorithms and Input Variables

Demand and Energy Savings

CPS Energy estimates demand and energy savings from C&I DR events using a multiple baselining method. This approach calculates savings using 4 different methods first and then selects the savings generated by the most appropriate method by evaluating some statistical criteria. To be more specific, the general calculation process of "multiple-baselining method" is as follows:

Step 1: data selection. For each event and each customer, the previous 10 eligible days and the event day are selected. These 11 days of data will be used for the analysis in the following steps.

Step 2: calculation. For each customer on each event, kW savings are calculated using 4 different methods, described as follows.

- Regression: Load is modeled as a function of cdh (cooling degree hours), notifying-period dummy variable indicating whether a period is a notifying period, event dummy variable indicating whether a period is an event period, 10 day-dummy variables indicating date and 3 time-of-day dummy variables indicating time of day – 0:00-6:00, 6:00-12:00, 12:00-18:00 or 18:00-24:00. The model equation can be expressed as follows:

$$kWt = \beta_0 + \beta_1 \times scdht + \beta_2 \times eventt + \beta_3 \times notify - periodt + \sum_{i=4}^6 \beta_i \times time - of - dayt + \sum_{j=7}^{16} \beta_j \times datet$$

$-\beta_2$ is the estimated load reduction for a certain customer during a certain event.

- CPS “High 3 of 10 baseline” analysis
- Previous X hours: X = event duration + notifying period. For example, if an event duration is 2 hours, and CPS notify customers 2 hours in advance, then X = 4. So, if an event is 3:30-5:30pm, then the baseline would be the average of 11:30am – 1:30pm)
- Average everything: this method calculates the average of all the load for the previous 10 eligible days and serve as baseline and is designed for customers with rather amorphous and irregular load.

Step 3: evaluation. For the testing data period,⁸⁸⁶ three measures including accuracy (RMSE), bias (difference) and variability (standard deviation) are calculated. This step measures how fit the model results are when compared with actual results for a similar period.

Step 4: final selection. For the three measures described in Step 3, a pairwise comparison is conducted using ranking method.⁸⁸⁷ The method with top ranking is selected.

After kW savings are generated by the automatic ranking selection process, manual inspections and potential manual adjustments may be needed for certain events or account IDs with unusual load profiles.

Demand savings are converted to energy savings by multiplying by the event duration. Per-customer kW and kWh savings are summed to yield program-wide demand and energy savings.

Under typical operations, for commercial demand response programs, 100 percent of energy and demand savings is allocated to the peak period, because the programs primarily reduce peak demand. However, it is possible that some commercial DR programs could be deployed in response to other, off-

⁸⁸⁶ Here “testing data period” refers to the same period as event period on top 3 of the previous 10 eligible days, plus 09:00am – 1:00pm on event day.

⁸⁸⁷ General rule for “pairwise comparison using ranking”: if the difference for a pair of baselines > 2% then the baseline with the higher one gets one point; otherwise, both baselines get 0.5 point. In the end, for each method respectively, RMSE, Error and standard deviation score are added together.

peak emergencies; in these cases, savings would be allocated as appropriate.

21.1.2.2 Measure Life and Lifetime Savings

Because commercial customers must re-enroll annually, the estimated useful life (EUL) is one year for commercial DR options 1, 2, 3, and 4. For the ADR program, in which CPS Energy makes significant investments in control technologies at the participating customers' premises, the EUL is assumed to be 10 years to better reflect the expected useful life of the installed equipment.

21.1.3 Program Tracking Data & Evaluation Requirements

The following list includes primary inputs and contextual data that should be specified and tracked in the program database to inform the evaluation and apply the savings properly.

- For each event, the starting and ending time, ambient temperature, and reason for deployment
- Program enrollment at the beginning and end of the program year, and during each demand response event, by participant class
- Fifteen-minute interval meter data should be available for all program participants

22. APPENDICES

22.1 MEASURE LIFE CALCULATIONS FOR EARLY RETIREMENT PROGRAMS

This section describes the method of calculating savings for early retirement programs. While this methodology addresses early retirement installations, it is also applicable to scenarios in which the baseline changes over the lifetime of the measure. This methodology tracks the early retirement calculations approved by the Public Utility Commission of Texas for use by other utilities in Texas.⁸⁸⁸

Step 1: Determine the measure life for ER and ROB components of the calculated savings:

$$\text{Early Retirement (ER) Period} = ML_{ER} = RUL$$

Equation 22.1-1

$$\text{Replace on Burnout (ROB) Period} = ML_{ROB} = EUL - RUL$$

Equation 22.1-2

Where:

RUL = Remaining useful life determined from lookup tables based on the age of the replaced unit (or default age when actual age is unknown).

EUL = Estimated useful life as specified in applicable energy efficiency measure.

Step 2: Calculate the ER demand and energy savings and the ROB demand and energy savings:

$$\Delta kW_{ER} = kW_{replaced} - kW_{installed}$$

Equation 22.1-3

$$\Delta kW_{ROB} = kW_{baseline} - kW_{installed}$$

Equation 22.1-4

$$\Delta kWh_{ER} = kWh_{replaced} - kWh_{installed}$$

Equation 22.1-5

$$\Delta kWh_{ROB} = kWh_{baseline} - kWh_{installed}$$

Equation 22.1-6

Where:

ΔkW_{ER} = Early retirement demand savings.

ΔkW_{ROB} = Replace-on-burnout demand savings.

⁸⁸⁸ Petition of AEP Texas Central Company, AEP Texas North Company, CenterPoint Energy Houston Electric, LLC, El Paso Electric Company, Entergy Texas, Inc., Oncor Electric Delivery Company LLC, Sharyland Utilities, L.P., Southwestern Electric Power Company, Southwestern Public Service Company, And Texas-New Mexico Power Company to Approve Revisions to Residential and Nonresidential Deemed Savings Incorporated in Texas TRM 2.0 (February 18, 2015).

| | | |
|--------------------|---|---|
| $kW_{replaced}$ | = | Demand of the retired system. ⁸⁸⁹ |
| $kW_{baseline}$ | = | Demand of the baseline ROB system. ⁸⁹⁰ |
| $kW_{installed}$ | = | Demand of the replacement system. ⁸⁹¹ |
| ΔkWh_{ER} | = | Early retirement energy savings. |
| ΔkWh_{ROB} | = | Replace-on-burnout energy savings. |
| $kWh_{replaced}$ | = | Energy Usage of the retired system. ⁸⁹² |
| $kWh_{baseline}$ | = | Energy Usage of the baseline ROB system. ⁸⁹³ |
| $kWh_{installed}$ | = | Energy Usage of the replacement system. ⁸⁹⁴ |

Step 3: Calculate the avoided capacity and energy cost contributions of the total NPV for both the ER and ROB components:

$$NPV_{ER,kW} = AC_{kW} \times \frac{1+e}{d-e} \times \left\{ 1 - \left[\frac{1+e}{1+d} \right]^{ML_{ER}} \right\} \times \Delta kW_{ER}$$

Equation 22.1-7

$$NPV_{ROB,kW} = AC_{kW} \times \frac{1+e}{d-e} \times \left\{ 1 - \left[\frac{1+e}{1+d} \right]^{ML_{ROB}} \right\} \times \frac{(1+e)^{ML_{ER}}}{(1+d)^{ML_{ER}}} \times \Delta kW_{ROB}$$

Equation 22.1-8

$$NPV_{ER,kWh} = AC_{kWh} \times \frac{1+e}{d-e} \times \left\{ 1 - \left[\frac{1+e}{1+d} \right]^{ML_{ER}} \right\} \times \Delta kWh_{ER}$$

Equation 22.1-9

$$NPV_{ROB,kWh} = AC_{kWh} \times \frac{1+e}{d-e} \times \left\{ 1 - \left[\frac{1+e}{1+d} \right]^{ML_{ROB}} \right\} \times \frac{(1+e)^{ML_{ER}}}{(1+d)^{ML_{ER}}} \times \Delta kWh_{ROB}$$

Equation 22.1-10

Where:

| | | |
|----------------|---|---|
| $NPV_{ER,kW}$ | = | Net Present Value (kW) of ER projects. |
| $NPV_{ROB,kW}$ | = | Net Present Value (kW) of ROB projects. |
| $NPV_{ER,kWh}$ | = | Net Present Value (kWh) of ER projects. |

⁸⁸⁹ Retired system refers to the existing equipment that was in use before the retrofit has occurred.

⁸⁹⁰ Baseline used for a replace-on-burnout project of the same type and capacity as the system being installed in the early retirement project (as specified in the applicable measure).

⁸⁹¹ Replacement system refers to the installed equipment that is in place after the retrofit has occurred.

⁸⁹² Retired system refers to the existing equipment that was in use before the retrofit has occurred.

⁸⁹³ Baseline used for a replace-on-burnout project of the same type and capacity as the system being installed in the early retirement project (as specified in the applicable measure).

⁸⁹⁴ Replacement system refers to the installed equipment that is in place after the retrofit has occurred.

| | | |
|------------------|---|---|
| $NPV_{ROB, kWh}$ | = | Net Present Value (kWh) of ROB projects. |
| e | = | Escalation Rate, provided by CPS Energy. |
| d | = | Discount rate weighted average cost of capital, provided by CPS Energy. |
| AC_{kW} | = | Avoided cost per kW, provided by CPS Energy. |
| AC_{kWh} | = | Avoided cost per kWh, provided by CPS Energy. |
| ML_{ER} | = | ER Measure Life (calculated in Equation 22.1-1). |
| ML_{ROB} | = | ROB measure life (calculated in Equation 22.1-2). |

Note: (1) the Early Retirement savings, earned for the RUL of the replaced system, are estimated by using the difference between the efficiency of the replaced system and that of the installed system; (2) the replace-on-burnout savings, earned over the measure EUL minus the project's RUL, are estimated by using the difference between the replace-on-burnout baseline efficiency and the efficiency of the installed system.

Step 4: Calculate the total capacity and energy cost contributions to the total NPV:

$$NPV_{Total, kW} = NPV_{ER, kW} + NPV_{ROB, kW}$$

Equation 22.1-11

$$NPV_{Total, kWh} = NPV_{ER, kWh} + NPV_{ROB, kWh}$$

Equation 22.1-12

Where:

$$NPV_{Total, kW} = \text{Total capacity contributions to NPV of both ER and ROB component.}$$

$$NPV_{Total, kWh} = \text{Total energy contributions to NPV of both ER and ROB component.}$$

Step 5: Calculate the capacity and energy cost contributions to the NPV without weighting by demand and energy savings for a scenario using the original EUL:

$$NPV_{EUL, kW} = AC_{kW} \times \frac{1+e}{d-e} \times \left\{ 1 - \left[\frac{1+e}{1+d} \right]^{EUL} \right\}$$

Equation 22.1-13

$$NPV_{EUL, kWh} = AC_{kWh} \times \frac{1+e}{d-e} \times \left\{ 1 - \left[\frac{1+e}{1+d} \right]^{EUL} \right\}$$

Equation 22.1-14

Where:

$$NPV_{EUL, kW} = \text{Capacity contributions to NPV without weighting, using original EUL.}$$

$$NPV_{EUL, kWh} = \text{Energy contributions to NPV without weighting, using original EUL.}$$

Step 6: Calculate the weighted demand and energy savings by dividing the combined capacity and energy cost contributions from the ER and ROB scenarios by the non-savings weighted capacity and energy cost contributions from the single EUL scenario. These weighted savings are claimed over the original measure EUL:

$$\text{Weighted } kW = \frac{NPV_{Total.kW}}{NPV_{EUL,kW}}$$

Equation 22.1-15

$$\text{Weighted } kWh = \frac{NPV_{Total.kWh}}{NPV_{EUL,kWh}}$$

Equation 22.1-16

Where:

| | | |
|---------------------------------|---|---|
| <i>Weighted kW</i> | = | <i>Weighted lifetime demand savings.</i> |
| <i>Weighted kWh</i> | = | <i>Weighted lifetime energy savings.</i> |
| <i>NPV_{Total, kW}</i> | = | <i>Total capacity contributions to NPV of both ER and ROB component, calculated in Equation 22.1-11.</i> |
| <i>NPV_{Total, kWh}</i> | = | <i>Total energy contributions to NPV of both ER and ROB component, calculated in Equation 22.1-12.</i> |
| <i>NPV_{EUL, kW}</i> | = | <i>Capacity contributions to NPV without weighting, using original EUL, calculated in Equation 22.1-13.</i> |
| <i>NPV_{EUL, kWh}</i> | = | <i>Energy contributions to NPV without weighting, using original EUL, calculated in Equation 22.1-14.</i> |



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